



MEMO

ТО	Katie Daugherty, Oregon Department of Environmental Quality
FROM	Brendan Robinson, PE, Environmental Resources Management, Inc.
DATE	16 September 2024
REFERENCE	0732445 Phase 204
SUBJECT	July 2024 GW SCM Monthly Performance Monitoring Report

1. INTRODUCTION

Environmental Resources Management, Inc. (ERM) prepared this Monthly Performance Monitoring Report (MPR) on behalf of Legacy Site Services LLC (LSS), agent for Arkema Inc. (Arkema), for the former Arkema Portland Plant (the Site) at 6400 NW Front Avenue in Portland, Oregon. The Oregon Department of Environmental Quality (ODEQ), in its letter dated 31 May 2019 and in the subsequent meeting with LSS and ERM on 2 July 2019, requested that LSS initiate monthly status reports associated with the onsite groundwater source control measure (GW SCM) consistent with the Performance Monitoring Plan (PMP; ERM 2014) beginning July 2019. The 2014 PMP was prepared pursuant to the Order on Consent issued by ODEQ, signed on 31 October 2008 (ODEQ No. LQVC-NWR-08-04; Consent Order). The purpose of the PMP was to present the monitoring, reporting, and adaptive management processes used during implementation of the GW SCM. On 30 November 2021, ODEQ directed LSS that following the October 2021 MPR, subsequent MPRs would be suspended pending the implementation of the Groundwater Extraction Enhancement (GEE) project in 2022. During that time, ODEQ requested monthly schedule updates in lieu of MPRs. The trench wells installed as part of the GEE project were started on 27 November 2022, and MPR writing restarted in December 2022. The purpose of the GEE project was to install new extraction capacity to achieve the Capture Zone Objectives.

This July 2024 MPR summarizes the GW SCM performance monitoring data collected in July 2024. This report assesses the current gradient status and proposes system improvements to meet the Capture Zone Objectives set in the PMP.

GROUNDWATER SOURCE CONTROL IMPLEMENTATION

A detailed description of the design and implementation of the GW SCM is provided in the *Revised Upland Feasibility Study Work Plan* (ERM 2017); however, a brief description of the GW SCM is provided here. In February 2009, ODEQ and the United



States Environmental Protection Agency (USEPA) approved the general approach for the GW SCM. This approach included installation of a groundwater barrier wall (GWBW), groundwater recovery wells (RW), and a Groundwater Extraction and Treatment (GWET) system, with treated water discharged to the Willamette River. ODEQ and USEPA approved the *Groundwater Barrier Wall Final Design* (ERM 2012) on 7 August 2012. Construction of the GWBW began in May 2012 and was completed in December 2012. ODEQ approved the *Groundwater Extraction and Treatment System Final Design* (ERM 2013) on 2 April 2013. Construction of the GWET system began in December 2012 and was completed in December 2013.

GWET startup and optimization commenced in May 2014. The GW SCM at the Site consists of the following primary components (Figure 1):

- 1. A GWBW to physically separate the affected upland portions and in-water portions of the Site.
- Hydraulic control to minimize flow of groundwater containing unacceptable concentrations of constituents of potential concern around, over, and under the GWBW.
- 3. Management of extracted groundwater through the GWET system, with treated effluent discharged to the Willamette River under a National Pollutant Discharge Elimination System (NPDES) Permit.

On 1 September 2018, ERM submitted the *Draft GWET System Effectiveness Evaluation* (Draft SEE Report; ERM 2018). The Draft SEE Report provided an update on the corrective actions implemented to improve the performance of the GWET system, evaluate the extent of capture, and propose actions to improve hydraulic capture. Additional data requested by ODEQ were submitted on 26 October 2018.

The key objective of the GW SCM is to achieve hydraulic containment of the alluvial sequence within the Target Capture Zone at the Site to prevent the flow of constituents of potential concern to the Willamette River. The Site alluvial aquifer sequence within the Target Capture Zone consists of the Shallow Zone, Intermediate Zone, and the Deep Zone. Site hydraulic conditions are variable and subject to both seasonal and daily tidal fluctuations.

The hydraulic control component formerly consisted of 22 RWs prior to the implementation of the GEE. Of the 22 pre-existing RWs, four were retained for active pumping. The remaining 18 former RWs had pumps removed, but retained their pressure transducers so that they can continuously collect high-resolution groundwater elevation data. The hydraulic control system now consists of the four-remaining active RWs, as well as seven groundwater extraction trenches that each contain two extraction wells (EW). Each trench is approximately 50 feet deep, 50 feet long, and 3 feet wide and is filled with an engineered backfill. More information about the groundwater extraction trenches is provided in the *Final Design Report* (ERM 2022). The gradient control-monitoring network consists of six gradient control clusters (GCC)



with each cluster containing six monitoring points. Within each RW, EW, and GCC location, pressure transducers are continuously collecting high-resolution groundwater elevation data. Each GCC contains three transducers interior to the wall and three transducers exterior to the wall screened in the Shallow, Intermediate, and Deep Aguifers at the Site.

3. RECOVERY WELL AND EXTRACTION WELL PERFORMANCE

The average system influent flow rate was 38.02 gallons per minute (gpm) for the entire month of July 2024, including non-operational periods. The average operational influent flow during operational periods was 49.56 gpm, a decrease from June 2024.

Extraction pumps become fouled with accumulated solids over time. A proactive pump removal and maintenance program is in place to address fouling and maximize flow rates. Trench 1 was off during June 2024 due to low pH from chemical redevelopment and was restarted in July 2024. Pressure jetting was completed at EW-11 and EW-12 during July 2024 to clean the well screen at Trench 6. Ongoing redevelopment is anticipated in August and September 2024 to maintain the productivity of the groundwater extraction trenches, and conveyance line cleaning will be conducted as needed based on analysis of backpressure. The reduction in groundwater extraction rate in July 2024 compared to June 2024 is believed to be a result of a significant decline in river elevation and average groundwater elevation as shown in Figures 1-1 and 1-2.

LSS is continuing to optimize extraction rates within the system to increase flow rates at each operational well until either the extraction rates specified in the *Final Design Report* (ERM 2022) are achieved, the wells are producing the maximum quantity of water possible, or until the Capture Zone Objectives are met.

TABLE 1-1 RECOVERY WELL PUMPING RATES

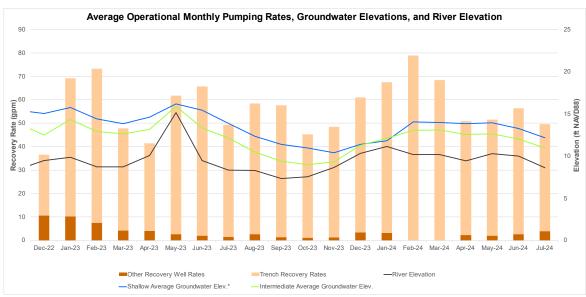
Recovery Well	July 2024 Average Operational Pumping Rate (gpm)	July 2024 Average Monthly Pumping Rate (gpm)
RW-14	2.17	2.10
RW-22*	0.00	0.00
RW-23	0.43	0.36
RW-25	1.42	1.42
EW-01	1.05	0.88
EW-02*	0.00	0.00
EW-03	12.51	12.51



Recovery Well	July 2024 Average Operational Pumping Rate (gpm)	July 2024 Average Monthly Pumping Rate (gpm)			
EW-04	2.59	0.83			
EW-05	7.18	7.18			
EW-06*	0.00	0.00			
EW-07	1.53	0.99			
EW-08	1.78	0.80			
EW-09	1.15	0.04			
EW-10	2.37	1.68			
EW-11	1.84	1.54			
EW-12*	0.00	0.00			
EW-13	7.39	6.68			
EW-14	6.13	0.99			
Total	49.56	38.02			

^{* =} Recovery well not in service during reporting period. gpm = gallon per minute

FIGURE 1-1 OPERATIONAL PUMPING RATE



^{* =} The shallow average groundwater elevation is calculated without PA-04 due to its groundwater elevations being unrepresentative of the whole aquifer. ft NAVD88 = feet North American Vertical Datum of 1988



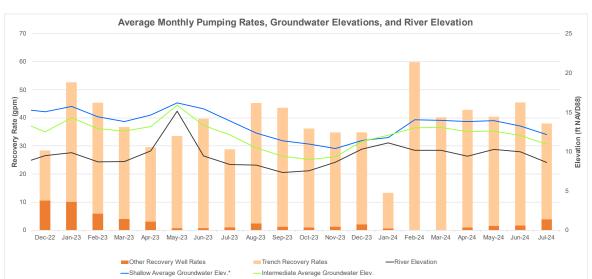


FIGURE 1-2 AVERAGE MONTHLY PUMPING RATE

* = The shallow average groundwater elevation is calculated without PA-04 due to its groundwater elevations being unrepresentative of the whole aquifer. ft NAVD88 = feet North American Vertical Datum of 1988

3.1 GWET SYSTEM PERFORMANCE

The GWET system operated within permit conditions during the reporting period. There was one shutdown:

 5 July 2024: The GWET system was shut down for 1.5 hours to clean the plate separator (PS-1).

4. HYDRAULIC CONTAINMENT MONITORING PROGRAM

As described in the PMP, the purpose of hydraulic monitoring (i.e., groundwater elevation data) is to provide sufficient data to demonstrate an inward hydraulic gradient across the GWBW and to evaluate the effective hydraulic capture produced by the GW SCM.

Monitoring requirements were established in the PMP to demonstrate GWET effectiveness. The Site monitoring program includes groundwater elevation data (manual and transducer measurements) collected from the 36 monitoring points located within six GCCs spaced across the GWBW, with piezometers interior and exterior to the wall, throughout the alluvial sequence; and groundwater elevation and flow rate data from the four-remaining active RWs and 14 EWs. High-resolution groundwater elevation data are also collected from the 18 inactive RWs. Additionally, one new monitoring well was installed in each of the seven extraction trenches for manual water level measurement. These data were used to prepare horizontal and vertical potentiometric surface maps representing potentiometric differences between the alluvial sequences, and to generate spatial and temporal hydrographs to evaluate hydraulic capture.



4.1 GROUNDWATER ELEVATION MONITORING

Groundwater elevation monitoring was completed on 12 July 2024. Manual groundwater elevations were measured at wells that were experiencing transducer mechanical issues or that were offline during the groundwater elevation measurement event. Additionally, all transducers in inactive RWs were down until upgrades were completed and transducers were sequentially turned on. Specific issues are addressed in Attachment A-1.

As detailed in Attachments A-1 and A-2, during July 2024, the following transducers were:

Fully out of service pending repairs:

None

Out of service for a period, but returned to full operation:

None

As described above, GCC locations collect high-resolution groundwater elevation data using transducers. Transducer data are filtered to remove anomalous data from monitoring points due to potential equipment failures, such as transducer malfunctions, power outages, or updates to the GWET programmable logic controller (PLC) system, which controls and houses all the operational data. These specific issues and time periods are summarized in Table A-1 in Attachment A-1. The following flags are applied to filter anomalous data:

- Groundwater elevations had a change greater than 1.5 feet within 1 hour
- Water column depth measurements that were found to be greater than 50 feet, or less than 1 foot
- Calculated groundwater elevation slope indicates no change between consecutive measurements indicating a transducer malfunction
- Manually flagging data that are inconsistent with the typical nature of the well
- Periods where transducer power supply was deactivated for work on interconnected electrical systems

After July 2024 flagged data were removed, the Serfes (1991) method was used to account for tidal variations as described in the PMP. Using Serfes-corrected data, both horizontal and vertical gradients were calculated and plotted over time (Attachment B). Groundwater elevations, horizontal gradients, and vertical gradients from 12 July 2024 are shown below at each GCC (Tables 1-2 and Table 1-3).



TABLE 1-2 JULY HORIZONTAL GRADIENTS

Gradient Cluster	Well Pair Zone	Exterior Well	Water Elevation (ft NAVD88)	Interior Well	Water Elevation (ft NAVD88)	Horizontal Gradient (ft/ft)
GCC1	Shallow	PA-03	25.29	PA-04	25.80	-0.005
	Intermediate	Intermediate PA-17iR		PA-10i	12.43	-0.016
	Deep	PA-27d	10.19	PA-18d	10.17	0.000
GCC2	Shallow	MWA-2	9.18	PA-05 ^M	7.42	0.026
	Intermediate	MWA-8i	8.79	PA-11i	9.80	-0.014
	Deep	PA-19d	7.81	PA-30d	8.72	-0.017
GCC3	Shallow	MWA-69	9.16	PA-06	12.09	-0.028
	Intermediate	MWA-66i	8.62	PA-12i	11.83	-0.018
	Deep	PA-21d ^M	8.99	PA-20d	8.79	0.002
GCC4	Shallow	MWA-19	9.70	PA-28 [™]	14.60	-0.049
	Intermediate	MWA-34iR ^M	9.44	PA-13i	10.81	-0.015
	Deep	MWA-58d	8.15	PA-22d	9.82	-0.019
GCC5	Shallow	MWA-47	9.18	PA-07	14.37	-0.050
	Intermediate	PA-29i	8.88	PA-14i	10.85	-0.036
	Deep	PA-24d ^M	8.37	PA-23d	8.77	-0.008
GCC6	Shallow	PA-09 ^M	11.61	PA-08 [™]	12.84	-0.022
	Intermediate	PA-16i	10.24	PA-15i	10.33	-0.002
	Deep	PA-26d	10.59	PA-25d ^M	10.24	0.006

Positive horizontal gradient indicates an inward hydraulic gradient across the GWBW. Horizontal gradient calculated as (Exterior Elevation – Interior Elevation) / Horizontal distance. * = anomalous groundwater elevation; ** = horizontal gradient cannot be calculated due to anomalous elevation reading; ft NAVD88 = feet North American Vertical Datum of 1988; $^{\text{M}}$ = manual groundwater elevation measurement



TABLE 1-3 JULY VERTICAL GRADIENTS

Region	Pair	Gradient Cluster	Upper Well	Water Elevation (ft NAVD88)	Lower Well	Water Elevation (ft NAVD88)	Vertical Gradient (ft/ft)
		GCC1	PA-04	25.80	PA-10i ^M	12.43	1.35
		GCC2	PA-05 [™]	7.42	PA-11i	9.80	-0.22
	ZI·	GCC3	PA-06	12.09	PA-12i	11.83	0.02
	ZI-ZS	GCC4	PA-28 ^M	14.60	PA-13i	10.81	0.59
		GCC5	PA-07	14.37	PA-14i	10.85	0.37
rior		GCC6	PA-08 ^M	12.84	PA-15i	10.33	0.19
Interior		GCC1	PA-10i ^M	12.43	PA-18d	10.17	0.30
		GCC2	PA-11i	9.80	PA-30d	8.72	0.16
	DZ	GCC3	PA-12i ^M	11.83	PA-20d	8.79	0.15
	ZQ-ZI	GCC4	PA-13i	10.81	PA-22d	9.82	0.05
		GCC5	PA-14i	10.85	PA-23d	8.77	0.05
		GCC6	PA-15i	10.33	PA-25d ^M	10.24	0.00
		GCC1	PA-03	25.29	PA-17iR	10.75	0.93
		GCC2	MWA-2	9.18	MWA-8i	8.79	0.03
	ZI·	GCC3	MWA-69 ^M	9.16	MWA-66i	8.62	0.04
	ZI-ZS	GCC4	MWA-19	9.70	MWA-34iR ^M	9.44	0.04
		GCC5	MWA-47	9.18	PA-29i	8.88	0.03
rior		GCC6	PA-09 [™]	11.61	PA-16i ^M	10.24	0.10
Exterior		GCC1	PA-17iR	10.75	PA-27d	10.19	0.09
		GCC2	MWA-8i	8.79	PA-19d ^M	7.81	0.63
	ZQ	GCC3	MWA-66i	8.62	PA-21d ^M	8.99	-0.03
	ZQ-ZI	GCC4	MWA-34iR ^M	9.44	MWA-58d	8.15	0.06
		GCC5	PA-29i	8.88	PA-24d ^M	8.37	0.01
		GCC6	PA-16i	10.24	PA-26d	10.59	-0.01

Positive vertical gradient indicates a downward hydraulic gradient.

Vertical gradient calculated as (Upper Elevation – Lower Elevation) / Screen Midpoint distance.

^{* =} anomalous groundwater elevation; ** = vertical gradient cannot be calculated due to anomalous elevation reading; DZ = Deep Zone; ft NAVD88 = feet North American Vertical Datum of 1988; IZ = Intermediate Zone; $^{\text{M}}$ = manual groundwater elevation measurement; SZ = Shallow Zone



4.2 POTENTIOMETRIC SURFACE, GROUNDWATER ELEVATION DIFFERENCE MAPS, AND GROUNDWATER FLOW DIRECTIONS

As described in the PMP, potentiometric surface maps are used to evaluate flow paths. Vertical gradients are also used as an additional line of evidence to evaluate hydraulic containment. Groundwater elevation data collected on 12 July 2024 were used to prepare potentiometric surface maps based on manual measurements and averaged transducer groundwater elevations (Figures 2 through 4) and vertical difference maps (Figures 5 and 6).

The generalized flow direction indicated by the potentiometric surface maps shows overall groundwater flow from upgradient toward the GWBW. Potentiometric maps (Figures 2, 3, and 4) indicate generalized groundwater movement to the extraction trenches in the Shallow, Intermediate, and Deep Zones due to GW SCM pumping, and cones of depression are apparent around each groundwater extraction trench. Inward gradient was observed in the Shallow Zone at GCC2 and in the Deep Zone at GCC3 and GCC6. Horizontal gradients at GCCs across the Site mixed, with some areas trending toward an inward gradient, and some areas losing improvements made in June in all three hydrogeological zones.

River elevations are shown over time on Figures 1-1 and 1-2, and in an inset on the potentiometric surface maps (Figures 2 through 4). The river elevation in July 2024 had an average elevation of 8.61 feet NAVD88 with a minimum elevation of 6.25 NAVD88 and a maximum elevation of 11.87 NAVD88, a decrease compared to June 2024. However, the average Shallow and Intermediate groundwater elevation decreased from June by 1.1 feet each, and the river elevation has largely been trending downward since January 2024. The river did not experience a seasonal rise this year as typically occurs during most years.

Vertical gradients were calculated for each vertical well pair and are plotted on Figures 5 and 6. Vertical groundwater gradients interior to the GWBW between the Shallow and Intermediate Zones were generally downward with exception to GCC2 being upward (Figure 5). Vertical groundwater gradient trend lines are shown in Attachment B-3. The magnitude of the gradient is much greater at GCC1 than other monitoring locations due to the influence from a localized high-pressure zone near GCC1 where vertical groundwater flow is impeded by a localized confining unit (Figure 2). Exterior of the GWBW, vertical gradients between the Shallow and Intermediate Zones were overall downward as shown on Figure 5 and in Attachment B-2.

Interior of the GWBW vertical gradients between the Intermediate and Deep Zones were overall downward. The direction of vertical gradients exterior to the GWBW were primarily downward with exception to GCC6 and GCC3 being upward, as shown on Figure 6 and Attachment B-3.



4.2.1 RECOMMENDATIONS FOR EXTRACTION SYSTEM OPTIMIZATION

Recovery rates indicate that the active RWs and EWs are operating as designed, except for the troubleshooting discussed above. The extraction rates throughout the GWET system will continue to be optimized to meet Target Capture Objectives.

ANALYTICAL PROGRAM

Quarterly groundwater monitoring was implemented in accordance with the ODEQ-approved *Arkema Quarterly Groundwater Monitoring Work Plan* dated October 2019 and the ODEQ-approved reduced scope described in the 2021 monitoring program modification request memorandum dated 9 September 2021. The table below outlines sampling dates and submittal dates related to groundwater monitoring since the implementation of the reduced scope. The Quarterly Monitoring Reports present results from these sampling events.

Report	Sampling Dates	Report Submittal Date	
2021 Quarter 3	9/21/2021-9/24/2021	1/14/2022	
2021 Quarter 4	12/13/2021-12/16/2021	4/20/2022	
2022 Quarter 1	3/14/2022-3/17/2022	6/15/2022	
2022 Quarter 2	6/6/2022-6/9/2022	9/12/2022	
2022 Quarter 4	11/7/2022-11/10/2022	2/17/2023	
2023 Quarter 1	3/6/2023-3/10/2023	6/12/2023	
2023 Quarter 2	6/12/2023-6/16/2023	9/22/2023	
2023 Quarter 3	8/21/2023-8/24/2023	12/1/2023	
2023 Quarter 4	12/11/2023-12/14/2023	3/15/2024	
2024 Quarter 1	2/26/2024-2/29/2024	6/7/2024	
2024 Quarter 2	6/10/2024-6/13/2024	9/13/2024*	
2024 Quarter 3	9/9/2024-9/12/2024*	12/12/2024*	

^{*} Dates are tentative.

SUMMARY AND CONCLUSIONS

This report presents a summary of the GW SCM operation, maintenance, and monitoring activities conducted at the Site in July 2024 and documents results from system monitoring. The following summarizes ERM's observations and conclusions drawn from collected data.

6.1 GROUNDWATER FLOW

 Horizontal groundwater gradients in the Shallow and Intermediate Zones were all outward and the magnitude of the gradients has increased somewhat since June as



a result of a decrease in the elevation of the river and average groundwater elevation outside the GWBW compared to inside the GWBW. Horizontal gradients in the Deep Zone were inward GCC3 and GCC6 and are trending toward inward gradients except for GCC2 and GCC4. Additional improvements in gradients are anticipated as higher flow rates and uptime are achieved relative the flow rate of water toward the Target Capture Zone.

- Vertical groundwater gradients interior of the GWBW between the Shallow and
 Intermediate Zones were generally downward with exception to GCC2 being
 upward (Figure 5), and the magnitude of downward gradients has increased since
 June due to the decrease in river elevation and the average groundwater elevation
 outside the GWBW compared to inside the GWBW. Exterior of the GWBW, vertical
 gradients between the Shallow and Intermediate Zones were all downward and the
 magnitude of the gradients has generally increased since June.
- Interior of the GWBW vertical gradients between the Intermediate and Deep Zones were all downward and the magnitude of gradients has increased since June. The direction of vertical gradients exterior to the GWBW were generally downward with GCC6 and GCC3 being upward, as shown on Figure 6.
- The average river elevation in July 2024 was 8.61 feet NAVD88 with a minimum elevation of 6.25 feet NAVD88 and a maximum elevation of 11.87 feet NAVD88, a decrease compared to June, and has largely been trending downward since January 2024.

6.2 GROUNDWATER EXTRACTION

Based on July 2024 groundwater extraction and relevant hydrograph analysis, the trenches are achieving increased groundwater extraction rates compared to the legacy system. The groundwater mound around Trenches 1, 2, 3, and 4 is largely gone, and the mound around Trenches 5, 6, and 7 is being reduced with increased average extraction rates compared to prior years. Average monthly pumping rates in July 2024 were lower than June 2024 due to lower groundwater elevation.

Within the Site alluvial sequence, potentiometric maps indicate the GW SCM is producing generalized hydraulic capture throughout the Target Capture Zone. More operational time at elevated extraction rates will be required to evaluate whether GWET objectives are being met system wide.

Due to work conducted throughout 2024, issues that have historically limited groundwater extraction rates including fouling of pumps, back pressure in the conveyance line, and a pause on pump maintenance, have been addressed resulting in improved average pumping rates. As of July 2024, the main limitations to groundwater extraction are groundwater elevation, and the accumulation of silt within the EW trenches filter pack. Efforts to successfully redevelop the trenches and remove silt are ongoing.



6.3 RECOMMENDATIONS AND FUTURE WORK

Redevelopment of the trenches is planned for September 2024 to mitigate accumulation of silt in the filter pack in both the vertical and horizontal sections using impulse redevelopment techniques. LSS will continue to optimize new EWs, including pump maintenance and upgrades. Additional modifications to the system, if needed to meet capture objectives, will be included in subsequent MPRs. The project schedule provided as Attachment C summarizes planned activities.

Regards,

Brendan Robinson, PE Partner



7. References



Affected by Tidal Fluctuations." Groundwater, Vol. 29. No 4. July-August 1991.



FIGURES

FIGURE 1: SITE LAYOUT

FIGURE 2: JULY 2024 SHALLOW ZONE GROUNDWATER CONTOURS

FIGURE 3: JULY 2024 INTERMEDIATE ZONE GROUNDWATER CONTOURS

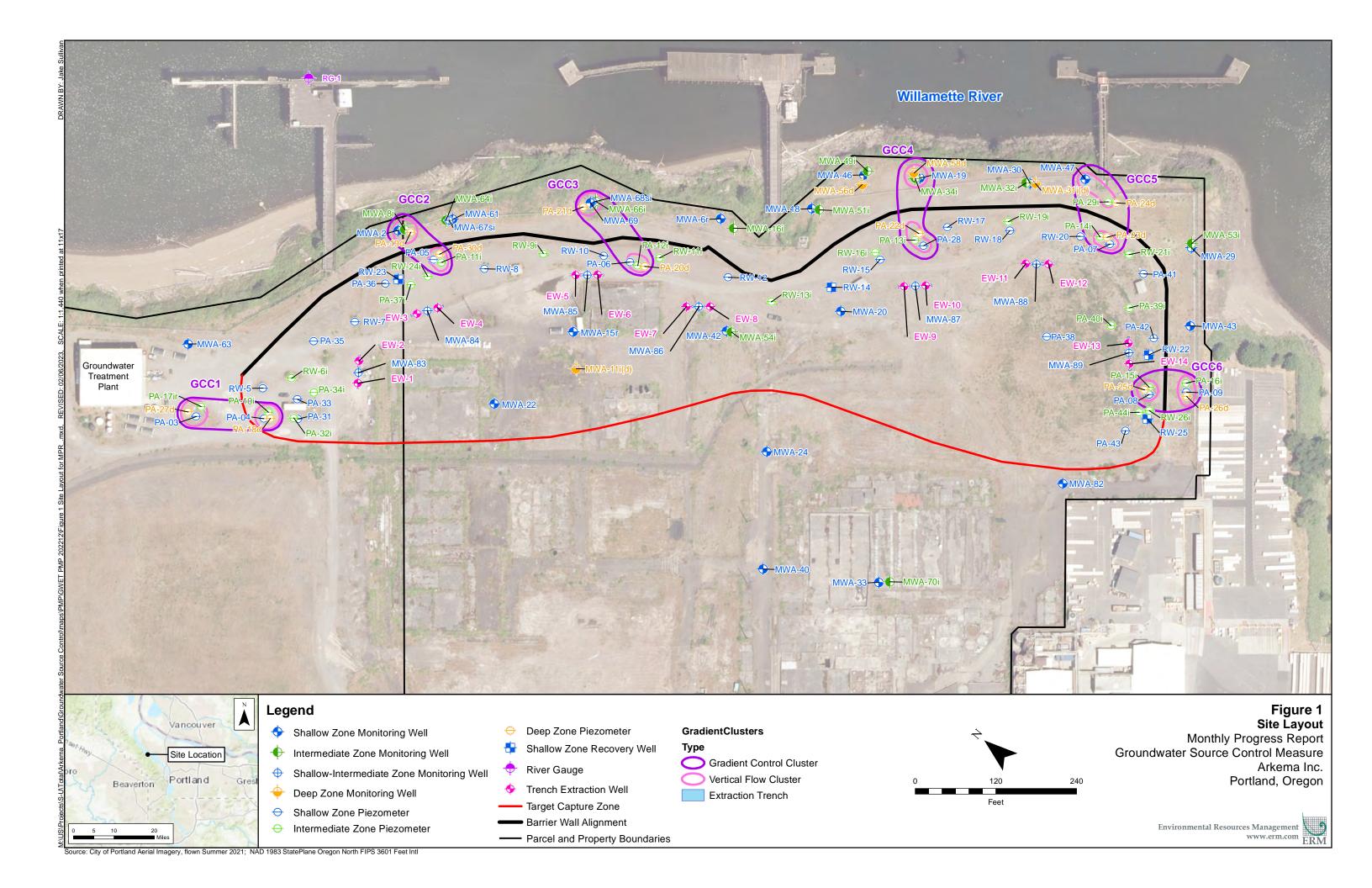
FIGURE 4: JULY 2024 DEEP ZONE GROUNDWATER CONTOURS

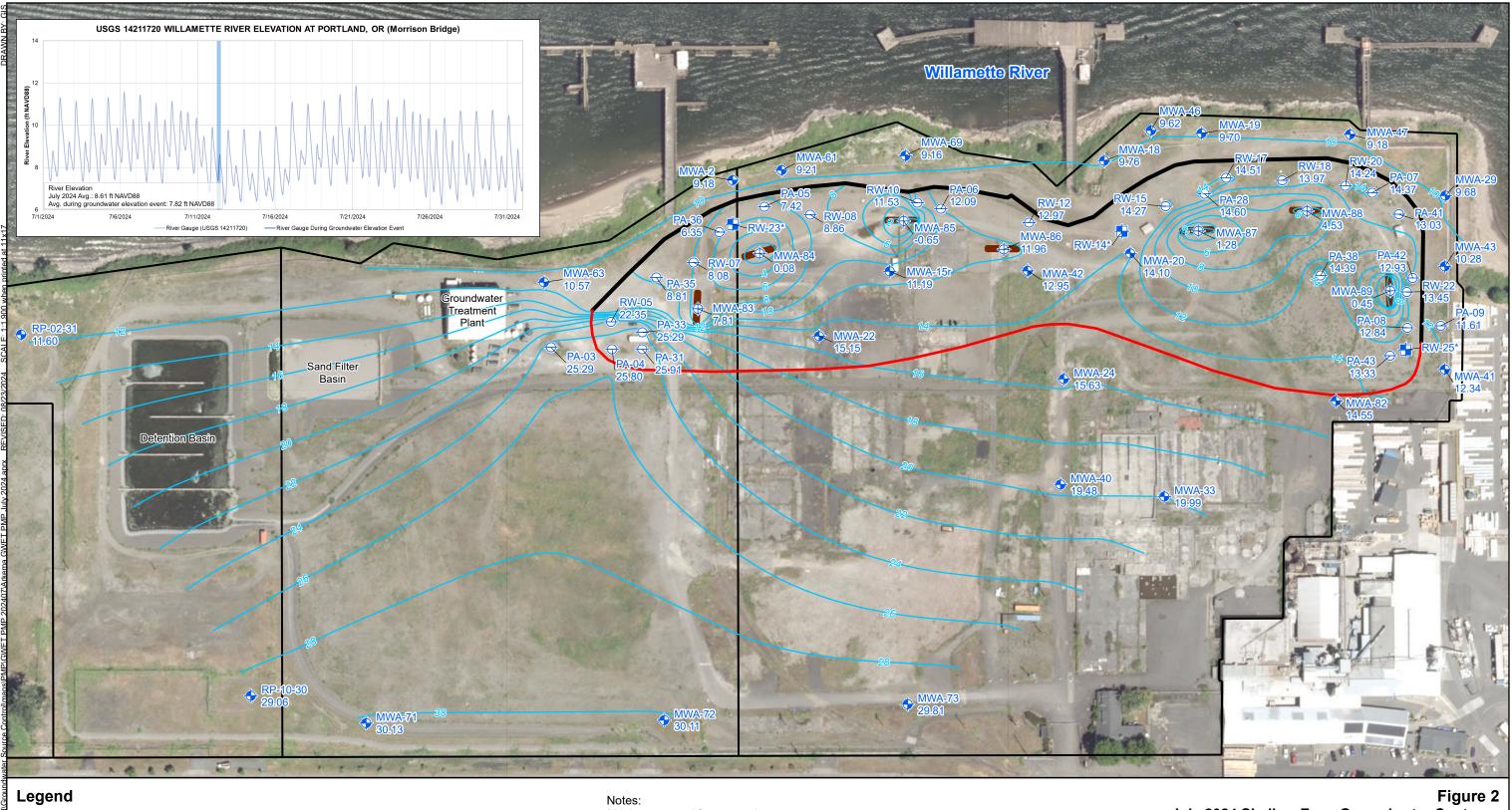
FIGURE 5: JULY 2024 SHALLOW TO INTERMEDIATE ZONE VERTICAL HEAD

DIFFERENCE

FIGURE 6: JULY 2024 INTERMEDIATE TO DEEP ZONE VERTICAL HEAD

DIFFERENCE





→ Shallow Zone Piezometer

Shallow Zone Monitoring Well

Active Recovery Well;
Not Used During Contouring

◆ Shallow-Intermediate Zone Monitoring Well Extraction Trench (Not To Scale)

27.70 Groundwater Elevation (ft NAVD88)

* Value not used for contouring.

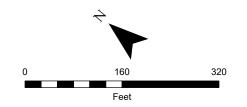
Water levels collected July 12, 2024.
ft NAVD88: feet North American Vertical Datum of 1988.

Aerial Photo: City of Portland, Summer 2017.

Shallow Zone Groundwater Contours (ft NAVD88) Dashed where Inferred

Target Capture Zone

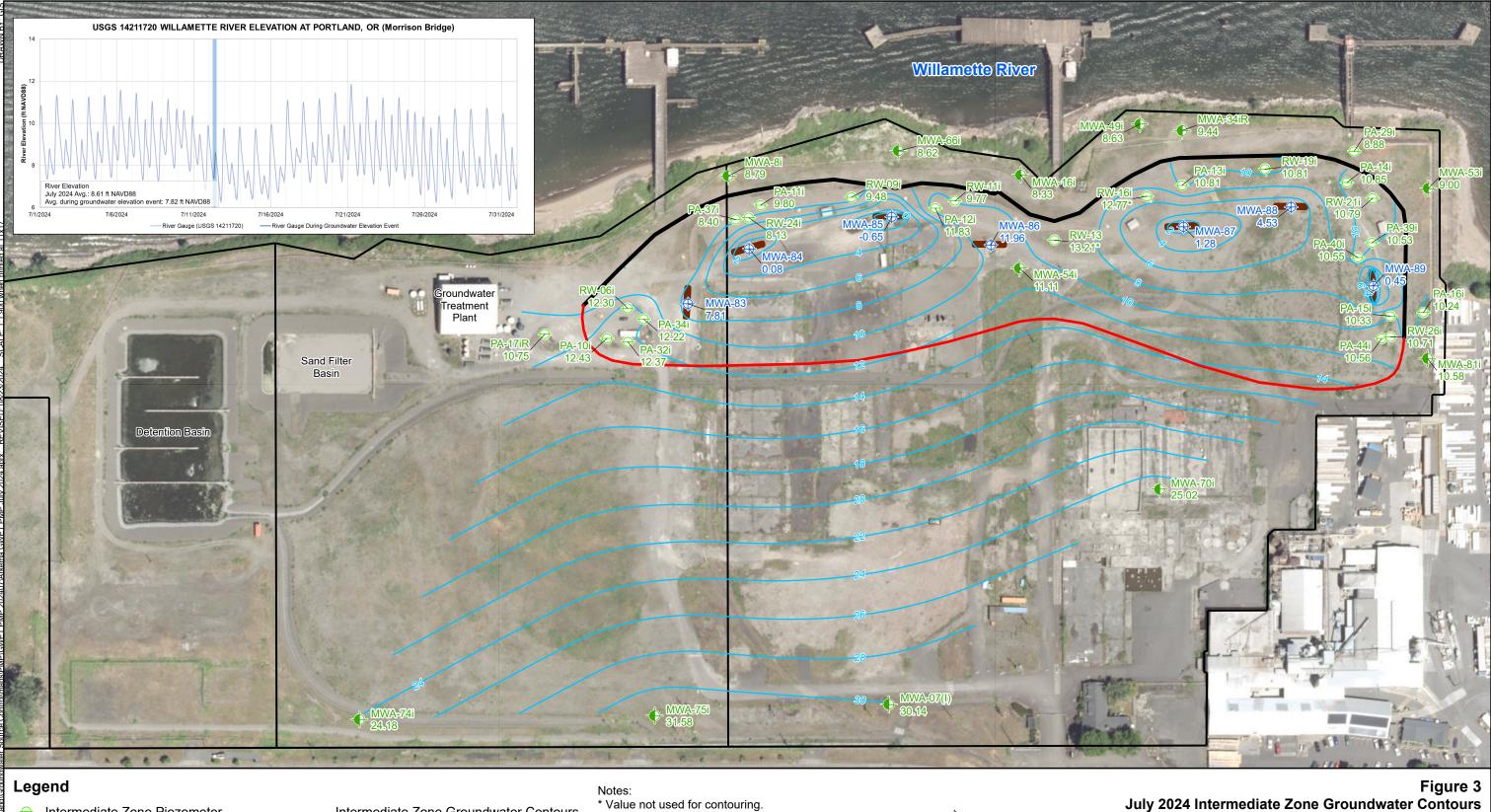
Barrier Wall Alignment



July 2024 Shallow Zone Groundwater Contours

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Environmental Resources Management www.erm.com



→ Intermediate Zone Piezometer

Intermediate Zone Monitoring Well

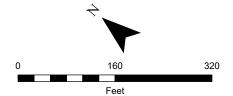
Shallow-Intermediate Zone Monitoring Well

27.70 Groundwater Elevation (ft NAVD88)

Intermediate Zone Groundwater Contours (ft NAVD88) Dashed where Inferred

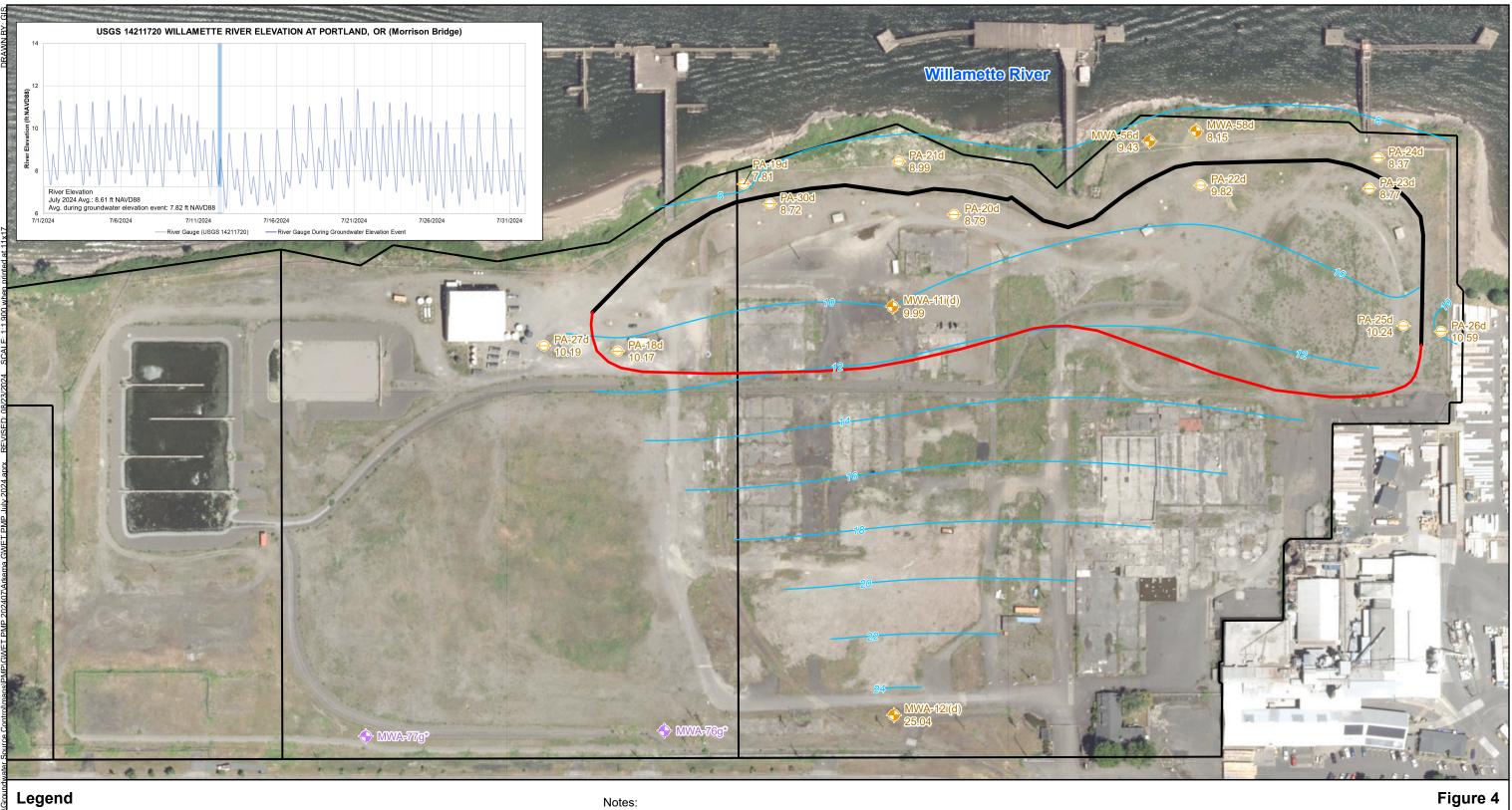
Target Capture Zone

 Barrier Wall Alignment Extraction Trench (Not To Scale) * Value not used for contouring.
Water levels collected July 12, 2024.
ft NAVD88: feet North American Vertical Datum of 1988. Aerial Photo: City of Portland, Summer 2017.



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Oeep Zone Piezometer

Deep Zone Monitoring Well

Gravel Zone Monitoring Well

27.70 Groundwater Elevation (ft NAVD88)

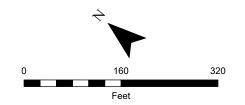
Deep Zone Groundwater Contours (ft NAVD88)

Dashed where Inferred

Target Capture Zone

Barrier Wall Alignment

* Value not used for contouring.
Gravel zone wells not used in contouring.
Water levels collected July 12, 2024.
ft NAVD88: feet North American Vertical Datum of 1988.
Aerial Photo: City of Portland, Summer 2017.



July 2024 Deep Zone Groundwater Contours

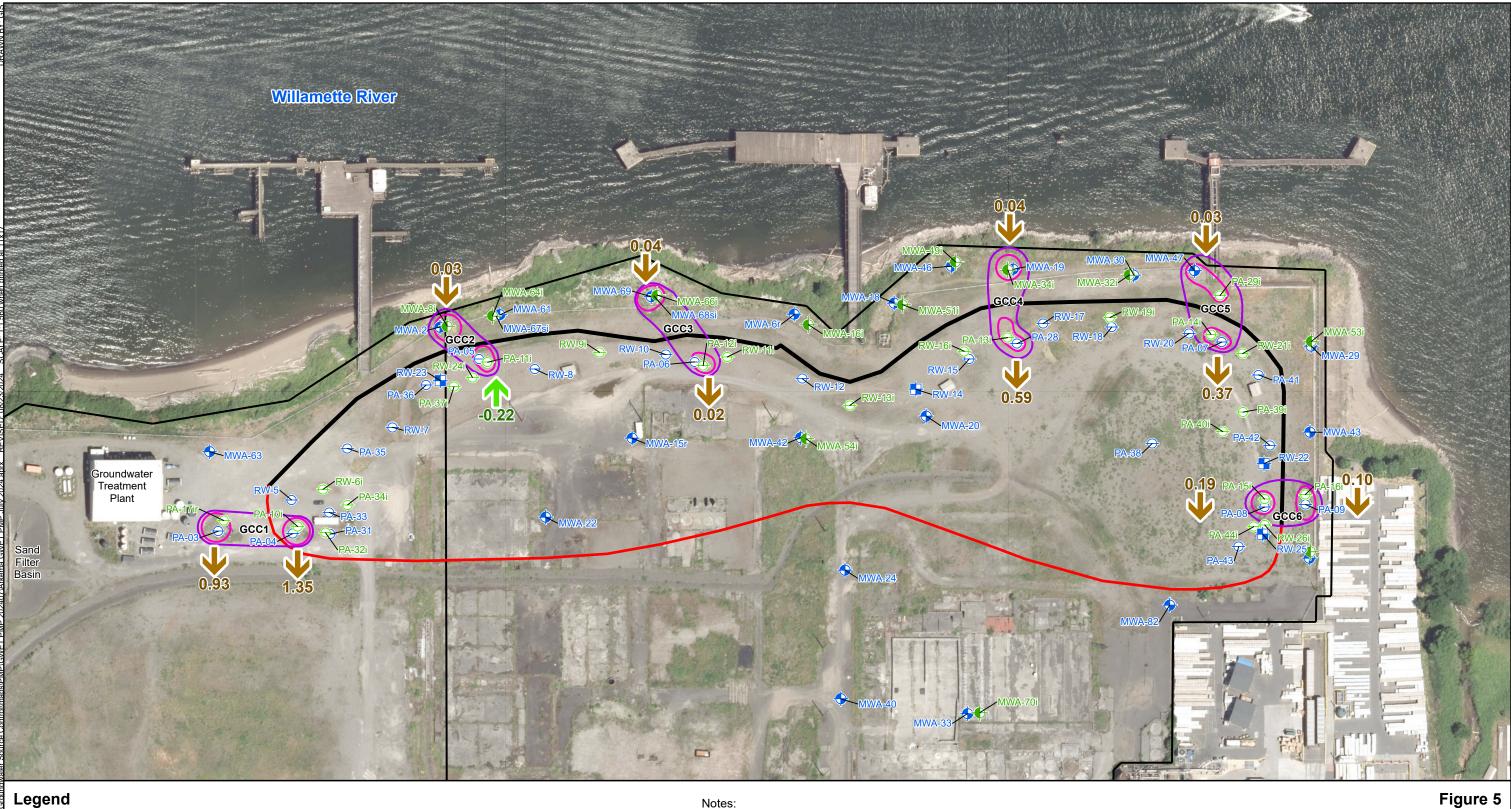
Monthly Progress Report

Groundwater Source Control Measures

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Shallow Zone Monitoring Well

Intermediate Zone Monitoring Well → Shallow Zone Piezometer

→ Intermediate Zone Piezometer

Shallow Zone Recovery Well

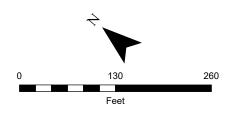
Target Capture Zone Barrier Wall Alignment

Gradient Control Cluster Vertical Flow Cluster

Downward Flow

↑ Upward Flow

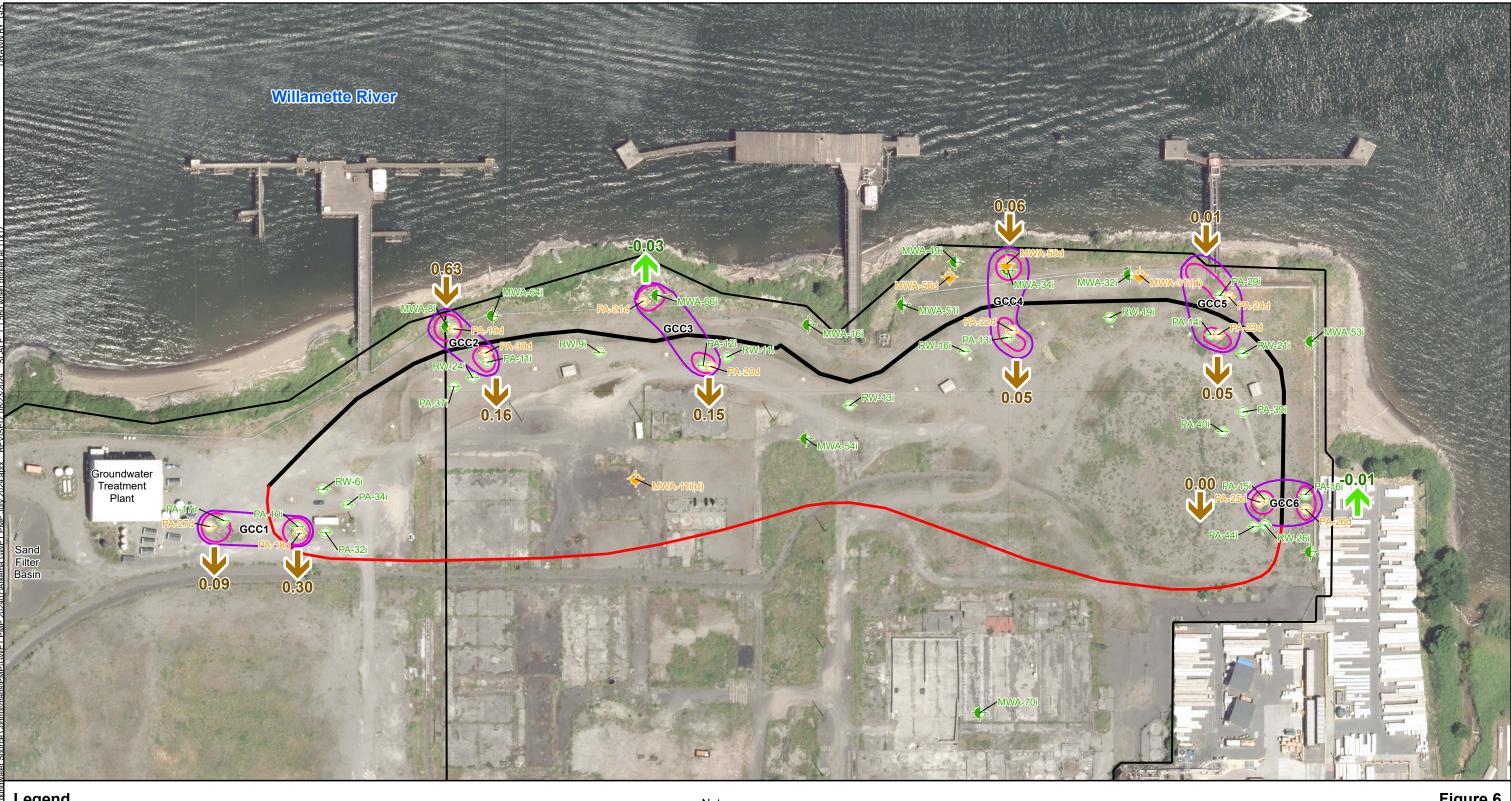
Brown gradient: Downward flow.
Green gradient: Upward flow.
Vertical gradient calculated as shallow zone minus intermediate zone potentiometric surfaces. Water levels collected July 12, 2024. Aerial Photo: City of Portland, Summer 2017.



July 2024 Shallow to Intermediate Zone **Vertical Head Difference**

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Legend

Intermediate Zone Monitoring Well

Deep Zone Monitoring Well

→ Intermediate Zone Piezometer

Deep Zone Piezometer

Target Capture Zone Barrier Wall Alignment

Gradient Control Cluster Vertical Flow Cluster

Brown gradient: Downward flow.
Green gradient: Upward flow.
Vertical gradient calculated as intermediate zone minus deep zone potentiometric surfaces. ↑ Upward Flow

Water levels collected July 12, 2024. Aerial Photo: City of Portland, Summer 2017.

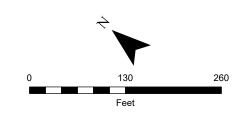


Figure 6 July 2024 Intermediate to Deep Zone Vertical Head Difference

Monthly Progress Report Groundwater Source Control Measures Arkema Inc. Portland, Oregon





ATTACHMENT A-1 TRANSDUCER FLAGS

Attachment A-1. Transducer Flags

Table A-1 Transducer Malfunction Log: July 2024 Arkema Inc. Facility Portland, Oregon

Gradient Cluster	Transducer	Interval	Date Range		ate Range Issue and Repairs Performed						
GCC4	MWA-34iR	Intermediate	5/28/2024	8/1/2024	Transducer to be recalibrated following survey 8/1/2024.						

Notes:

I/O = input/output

LOTO = lockout/tagout

VFD = variable frequency drive



ATTACHMENT A-2 RECOVERY WELL STATUS

Attachment A-2. Recovery Well Status

Table A-2 Recovery Well Status: July 2024

Arkema Inc. Facility Portland, Oregon

Recovery Well ID	Status as of 7/31/2024 (active or inactive)	Issue	Actions to get online	Expected date back online	Transducer Status	Totalizer Status	Average Operational Flow Rate (gpm)	Overall Extraction Rate	Notes
RW-14	Active	None	N/A	N/A	Good	Good	2.17	M**	
RW-22	Inactive	Ground Fault	Replace cable leads	N/A	Good	Good	0.00	OFF*	Cable leads need to be replaced
RW-23	Active	None	N/A	N/A	Good	Good	0.43	P**	
RW-25	Active	None	N/A	N/A	Good	Good	1.42	M**	
EW-01	Active	None	N/A	N/A	Good	Good	1.05	P**	
EW-02	Inactive	Totalizer	Troubleshoot totalizer	8/1/2024	Good	Not working	0.00	OFF*	Totalizer not communicating with PLC
EW-03	Active	None	N/A	N/A	Good	Good	12.51	G	
EW-04	Inactive	Low Water Table	N/A	N/A	Good	Good	2.59	M**	
EW-05	Active	None	N/A	N/A	Good	Good	7.18	G	
EW-06	Inactive	Low Water Table	N/A	N/A	Good	Good	0.00	OFF*	
EW-07	Inactive	Low Water Table	N/A	N/A	Good	Good	1.53	M**	
EW-08	Active	None	N/A	N/A	Good	Good	1.78	M**	Started 7/31/2024
EW-09	Active	None	N/A	N/A	Good	Good	1.15	M**	Started 7/31/2024
EW-10	Inactive	Low Water Table	N/A	N/A	Good	Good	2.37	M**	
EW-11	Active	None	N/A	N/A	Good	Good	1.84	M**	
EW-12	Inactive	None	N/A	N/A	Good	Good	0.00	OFF*	Transducer removed for packer installation
EW-13	Inactive	None	N/A	N/A	Good	Good	7.39	G**	Changed out 1 HP motor and pump on 7/29
EW-14	Active	None	N/A	N/A	Good	Good	6.13	G**	Started 7/29/2024

Notes:

* Recovery wells not in service

** Recovery wells in service part of the month

G = good pumping, greater than 3.0 gpm

gpm = gallons per minute

M = moderate pumping, greater than 1.0 gpm and less than 3.0

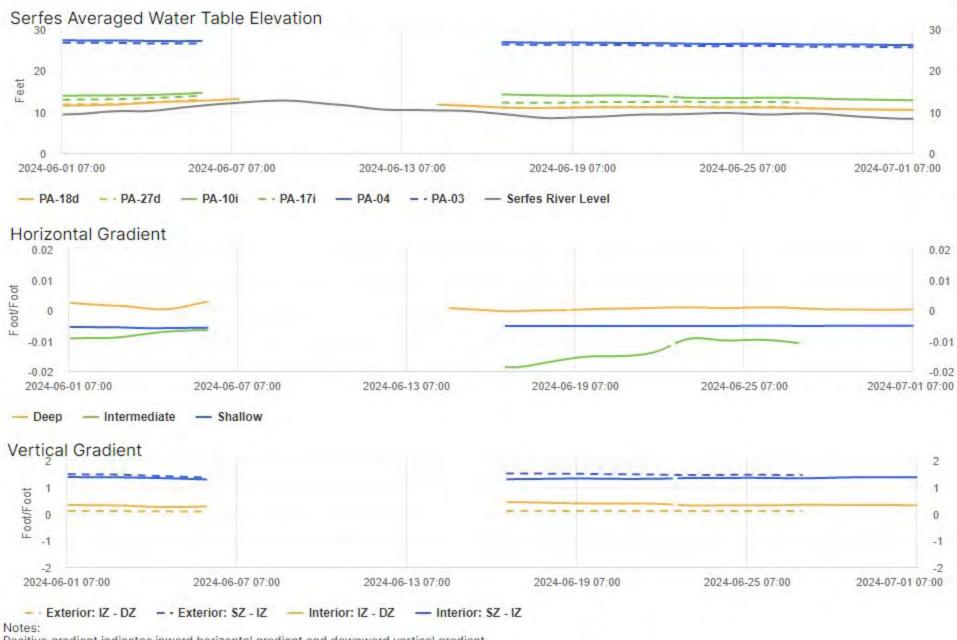
P = poor pumping, less than 1.0 gpm

VFD = variable frequency drive

PA = piezometer

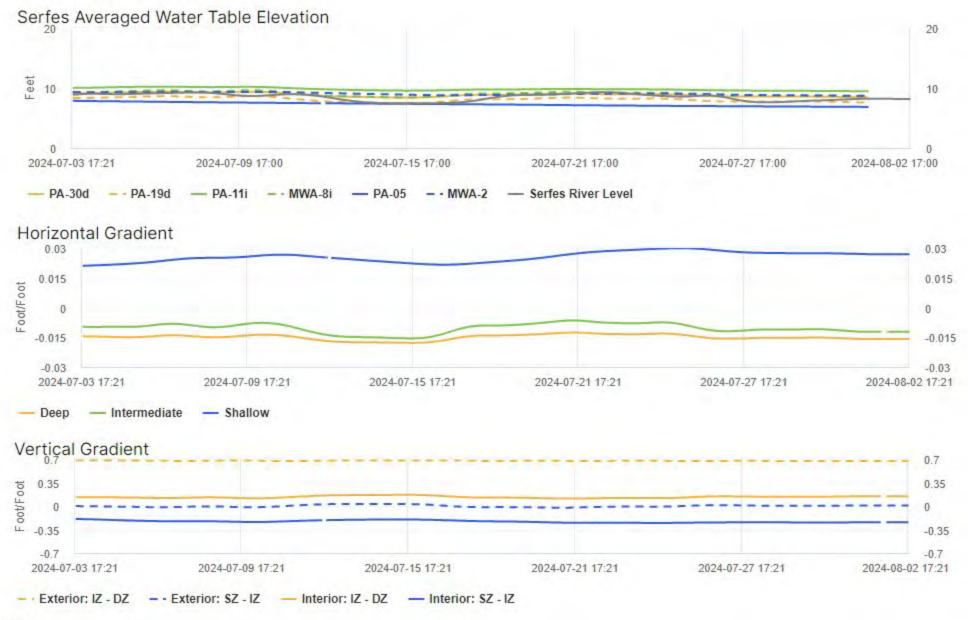


ATTACHMENT B-1 GRADIENT HYDROGRAPHS



Notes:
Positive gradient indicates inward horizontal gradient and downward vertical gradient
Vertical Gradient calculated using (WTE_upper - WTE_lower)/(Bottom of Screen_upper - Top of Screen_lower)
Horizontal gradient calculated as Exterior - Interior. Interior: Upland of the GWBW, Exterior: Riverside of the GWBW
SZ = Shallow Zone

IZ = Intermediate Zone DZ = Deep Zone



Notes:

Positive gradient indicates inward horizontal gradient and downward vertical gradient

Vertical Gradient calculated using (WTE_upper - WTE_lower)/(Bottom of Screen_upper - Top of Screen_lower)

Horizontal gradient calculated as Exterior - Interior. Interior: Upland of the GWBW, Exterior: Riverside of the GWBW

SZ = Shallow Zone

IZ = Intermediate Zone



Notes:

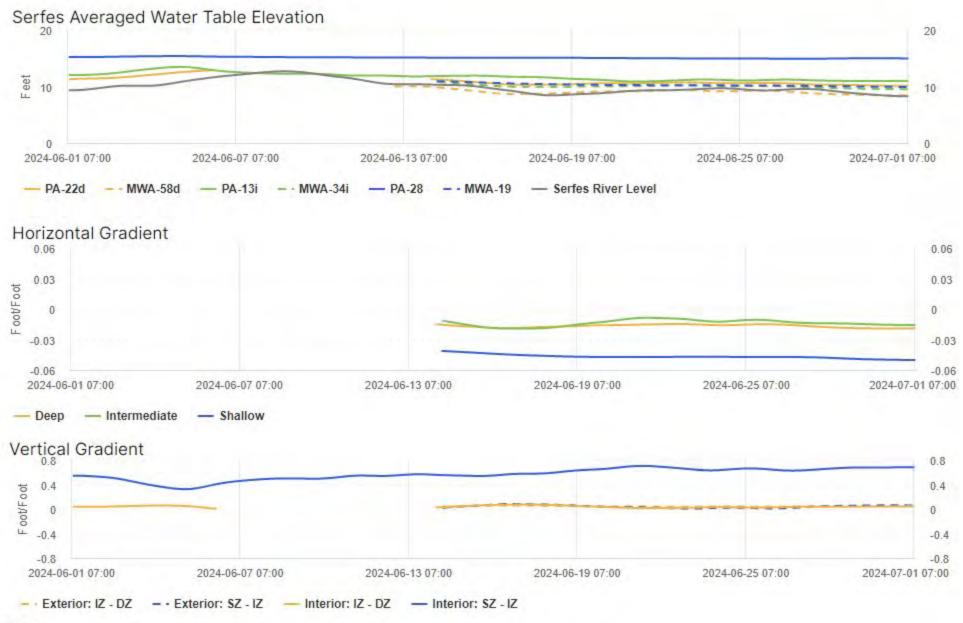
Positive gradient indicates inward horizontal gradient and downward vertical gradient

Vertical Gradient calculated using (WTE_upper - WTE_lower)/(Bottom of Screen_upper - Top of Screen_lower)

Horizontal gradient calculated as Exterior - Interior. Interior: Upland of the GWBW, Exterior: Riverside of the GWBW

SZ = Shallow Zone

IZ = Intermediate Zone



Notes:

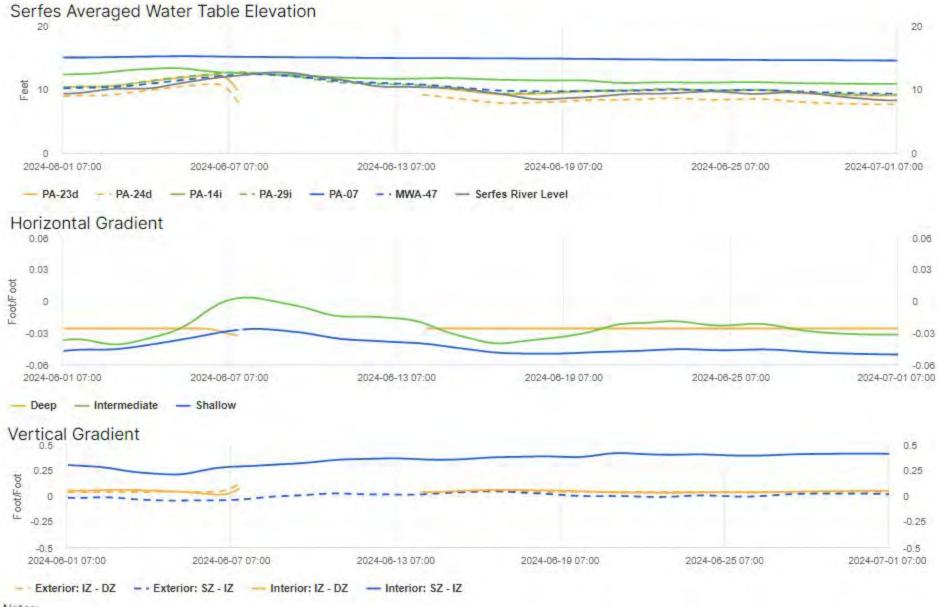
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Vertical Gradient calculated using (WTE_upper - WTE_lower)/(Bottom of Screen_upper - Top of Screen_lower)

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Positive gradient indicates inward horizontal gradient and downward vertical gradient
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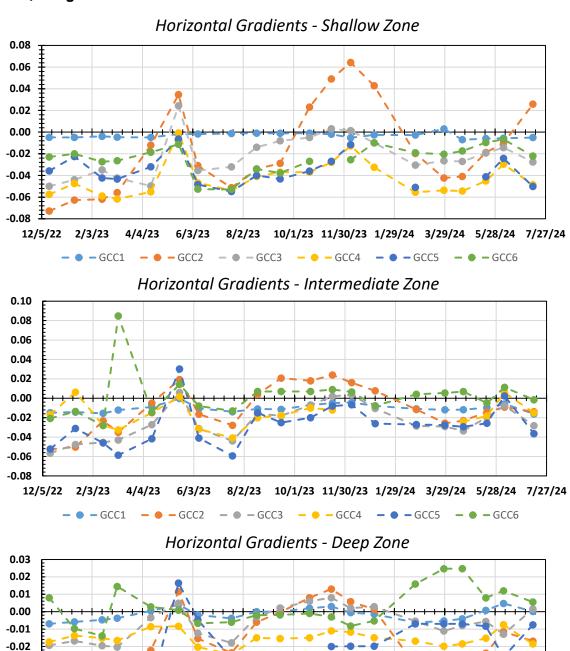
ATTACHMENT B-2 HORIZONTAL GRADIENTS

Attachment B-2

-0.03 -0.04 -0.05 -0.06 -0.07

12/5/22 2/3/23

Horizontal Gradients Summary: July 2024 Arkema Inc. Facility Portland, Oregon



Positive horizontal gradient indicates an inward hydraulic gradient across the GWBW.

6/3/23 8/2/23 10/1/23 11/30/23 1/29/24 3/29/24 5/28/24 7/27/24

- • - GCC2 - • - GCC3 - • - GCC4 - • - GCC5 - • - GCC6

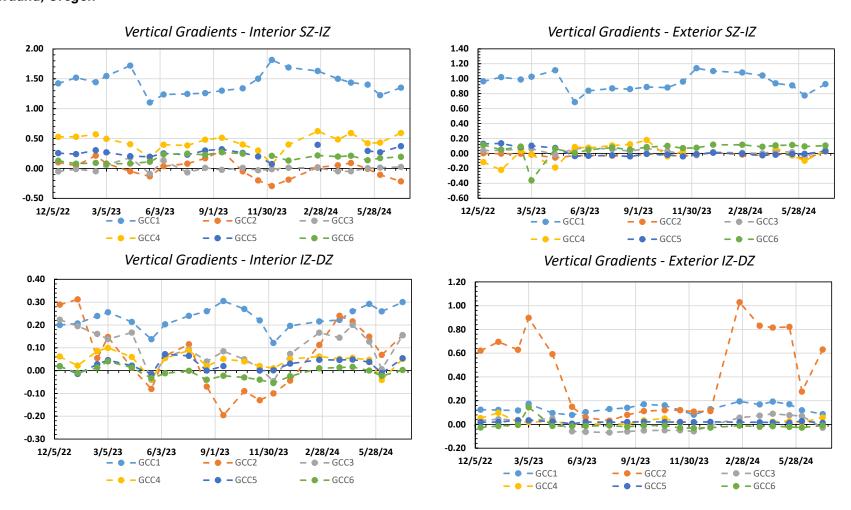
4/4/23



ATTACHMENT B-3 VERTICAL GRADIENTS

Vertical Gradients Summary: July 2024 Arkema Inc. Facility Portland, Oregon

Attachment B-3





ATTACHMENT C PROJECT SCHEDULE

