



ADVANCED INDUSTRIAL RESOURCES, INC.

***PERFORMANCE TEST REPORT  
EMISSION FACTOR VERIFICATION  
ADVANCED MATERIAL RECYCLING SYSTEM (AMRS)  
(EU-144)***

CONDUCTED AT:  
***GEORGIA-PACIFIC TOLEDO, LLC***

PREPARED FOR:



**GEORGIA-PACIFIC TOLEDO, LLC  
1400 SE BUTLER BRIDGE ROAD  
TOLEDO, OREGON 97391**

PREPARED BY:  
**ADVANCED INDUSTRIAL RESOURCES, INC.  
3407 NOVIS POINTE  
ACWORTH, GEORGIA 30101  
*PROJECT ID: KR - 11456***

**TEST DATES:  
JULY 12, 2023**



## REPORT CERTIFICATION SHEET

Having conducted the Technical Review of this report, I hereby certify the data, information, results, and calculations in this report to be accurate and true according to the methods and procedures used.

A handwritten signature in black ink, appearing to read "Derek Stephens", is written over a horizontal line.

Derek Stephens  
VP/QA Director  
Advanced Industrial Resources

September 8, 2023

Date

Having written and prepared this report, I hereby certify that the data, information and results in this report to be correct and all inclusive of the necessary information required for a complete third-party review of the testing event.

A handwritten signature in black ink, appearing to read "Cindy Wu", is written over a horizontal line.

Cindy Wu  
Report Preparation  
Advanced Industrial Resources

September 8, 2023

Date

Having supervised all aspects of the field testing, I hereby certify the equipment preparation, field sample collection procedures, and all equipment calibrations were conducted in accordance to the applicable methodologies.

A handwritten signature in black ink, appearing to read "Dan Kirk", is written over a horizontal line.

Dan Kirk  
Field Project Supervisor  
Advanced Industrial Resources

September 8, 2023

Date

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## 1.0 INTRODUCTION

### 1.1 SUMMARY OF TEST PROGRAM

Georgia-Pacific Toledo, LLC operates a pulp and paper facility located at 1400 SE Butler Bridge Road, Toledo, Oregon 97391. The facility produces containerboard products from “brown stock”. The facility is comprised of all normal paper industry processes except for the pulp bleaching processes.

This document represents the Test Report for the test program to determine whether the Advanced Material Recycling System (AMRS) (EU-144) stack exhaust is operating in compliance with the applicable emissions limits and to verify emission factors established in the facility’s air quality permit (Permit No. 21-0005-TV) for Volatile Organic Compounds (VOC), and Methanol/Formaldehyde in addition to Hazardous Air Pollutants (HAPs) as phenol, acetaldehyde, acrolein, and propionaldehyde.

Testing was conducted July 12, 2023, in accordance with an Oregon Department of Environmental Quality (ODEQ) and EPA approved test protocol. All testing was conducted by Advanced Industrial Resources, Inc. (AIR) in accordance with approved USEPA Methods (i.e., 40 CFR Part 60 Appendix A, Methods 1, 2, 3A, 4, 25A) and NCASI Method 105.01.

### 1.2 KEY PERSONNEL

The key personnel who coordinated the test program and their telephone numbers are:

Scott Austin, <i>Georgia-Pacific Toledo, LLC</i>	541-336-8318
Scott Wilson, Program Director – <i>AIR</i>	800-224-5007
Derek Stephens, MSEE, VP/QA Director – <i>AIR</i>	404-843-2100
Ross Winne, Technical Director – <i>AIR</i>	404-843-2100
Steven Haigh, Report Preparation Director – <i>AIR</i>	404-843-2100
Dan Kirk, Field Project Supervisor, <i>AIR</i>	404-843-2100
Cindy Wu, Technical Project Manager, <i>AIR</i>	225-776-7788

## **2.0 PROCESS AND SAMPLING LOCATION DESCRIPTIONS**

### **2.1 PROCESS DESCRIPTION**

The AMRS (EU-144) is operated in a new processing building constructed near the existing #4 boiler and extracts usable cellulose fiber from mixed solid waste streams that include food, paper, plastics, glass, and metals. OCC rejects can be added to the solid waste stream as it enters the process; however, it is not currently a typical feedstock for operations.

All of the raw materials are collected, baled, and wrapped at an offsite solid waste collection facility. The sealed, plastic wrapped bales are delivered by truck to the Toledo mill where the raw material is unloaded and stored outside of the processing building.

The municipal solid waste streams are staged at predesignated third-party operated transfer stations that are licensed to handle municipal solid waste from commercial and residential sources. The transfer stations have mechanisms in place for both prevention, detection, and removal of hazardous wastes, used oils, asbestos-containing materials, and any other inappropriate solid waste streams. Thus, the AMRS process does not receive or accept hazardous wastes, asbestos-containing materials, or other inappropriate solid waste streams.

At the mill site, the raw material is fed into a rotating autoclave which is a steam pressurized vessel with an internal rotating drum that processes and breaks down the raw materials during the two-hour batch cycle. The system utilizes a proprietary process that sanitizes the feedstock and separates paper fiber from the other commodities inherent in the feedstock stream. Although elevated, the maximum temperature of 270 degrees Fahrenheit in the autoclave is not high enough to decompose wood so the wood fibers in the raw materials or OCC rejects, if processed, leaves the autoclave as fiber in a slurry form. The design capacity of the AMRS is 50,000 lbs/batch of feedstock.

The fiber recovered from the AMRS is sent to the existing OCC plant in slurry form and is further cleaned and refined along with the regular OCC feedstock. The fiber recovered through the AMRS replaced a portion of the OCC wastepaper that is currently brought to and processed in the OCC plant.

Any metals and other residual materials that are not recovered as fiber during the AMRS process are collected, sorted, and sent to off-site recycling facilities or to an off-site

industrial landfill. Any effluent arising from the process are treated in the company's existing wastewater treatment system.

The overall process emissions are controlled first by packed bed tower scrubber followed by a carbon bed and then vented out of a single stack. The carbon bed also controls the building exhaust. The scrubber operating parameters pressure drop ("W.G.) and scrubber liquid rate (gpm), as well as the carbon absorption filters' pressure drop, are recorded during each test run for the AMRS.

## 2.2 SAMPLING LOCATION DESCRIPTION

The AMRS EU-144 carbon filter stack exhaust is circular and has an internal diameter of 39.0 inches and the sampling ports are located 120" upstream (3.1 equivalent diameters) from the stack exhaust (upstream disturbance), and 240" downstream (6.2 equivalent diameters) from the exhaust fan (downstream disturbance). The exhaust stack is equipped with a minimum of two sampling ports oriented 90 degrees to one another on a parallel plane oriented perpendicular to the exhaust gas flow direction.

EPA Method 25A and NCASI Method 105.01 was sampled in accordance with Method 25A Section 8.2, the centroidal region of the sampling locations was used for VOC emission concentration measurements.

### **3.0 SUMMARY AND DISCUSSION OF TEST RESULTS**

#### **3.1 OBJECTIVES AND TEST MATRIX**

Emission factor verification (EFV) performance testing was conducted to confirm source emissions are as expected from the initial unit's permit application and as established in the facility's permit under the plant site emission limits (PSEL) according by permit condition 93. Performance testing was conducted for volatile organic compounds (VOCs) and hazardous air pollutants (HAPs). The total VOC is the sum of total hydrocarbons, methanol, and formaldehyde in accordance with Equation A-1 of ODEQ Guidance for Evaluating VOC emissions. Additional HAPs were also conducted for phenol, acetaldehyde, acrolein, and propionaldehyde.

#### **3.2 FIELD TEST CHANGES, PROBLEMS, & ITEMS OF NOTE**

The testing was conducted in accordance with the ODEQ approved Source Test Plan. No problems were encountered during testing that required deviation from the planned test protocol.

#### **3.3 PRESENTATION OF TEST RESULTS**

Emission Factor Verification emission rates are summarized in Table 3-1 and additional HAPs results are summarized in Table 3-2. Complete emission concentrations and mass rates are presented in Appendix A. Reduced and tabulated data from the field-testing is included in Appendix B. The calculations and nomenclature used to reduce the data are presented in Appendix C. Actual raw field data sheets are presented in Appendix D. Laboratory reports and custody records are presented in Appendix E.

**TABLE 3-1: Emission Factor Verification Results Summary**

Source	Pollutant	Average Measured	Emission factor	Units	% of Allowable
Advanced Material Recycling System (AMRS) (EU-144)	VOC (as THC, C <sub>3</sub> H <sub>8</sub> )	0.21	0.40	lb/ton MSW	54%
	Methanol	0.0140	NA		NA
	Formaldehyde	J 6.27E-05			
	Total VOC (THC + HAPs) <sup>(1)</sup>	0.228	0.246		93%

**Note:**

- (1) Total VOC Mass Rates = THC<sub>(as propane)</sub> + Methanol + Formaldehyde in accordance with Equ. A-1 Attachment 1 of ODEQ Guidance for Evaluating VOC Emissions.
- (< or ND) indicates the analyte was a non-detect or below the MDL, results displayed are the result of the the MDL.
- (J) indicates the analyte was between the MDL and LOQ, the laboratory can positively identify the analyte as present but value is considered to be an estimate.

**TABLE 3-2: Additional HAPs Result Summary**

Source	Pollutant	Average Measured	Emission factor	Units	% of Allowable
Advanced Material Recycling System (AMRS) (EU-144)	Phenol	J 5.30E-04	NA	lb/ton MSW	NA
	Acetaldehyde	0.0106			
	Acrolein	< 1.91E-05			
	Propionaldehyde	J 3.36E-05			

### 3.4 PROCESS MONITORING

Testing was conducted while the applicable processes were operating at a target rate of 18 bales, which represents normal operating conditions. During testing, the process ran exclusively on municipal solid waste (MSW) feedstock. OCC rejects is not a current typical feedstock. GP Toledo ensured that all essential process monitoring equipment was operating properly and recording data throughout the test period to provide process operating rates necessary to determine process weight-based emission rates, as applicable. At a minimum, the facility monitored and recorded during each test run for AMRS EU-144, the scrubber operating parameters pressure drop (“H<sub>2</sub>O”), scrubber liquid flow rate (gpm), damper position, as well as the carbon absorption filters’ pressure drop, and the operating rate. The number of batches processed since the last carbon media replacement was recorded during the 12-consecutive monthly batch cycle tests. This information is presented in Appendix G.

#### 4.0 SAMPLING AND ANALYTICAL PROCEDURES

Performance testing was conducted according to the methodology in the *Title 40 Code of Federal Regulation*, Part 60, Appendix A as applicable. Specifically:

- EPA Method 1 was used for the qualification of the location of sampling ports and for the determination of the number and positions of stack traverse points, as applicable to sample traverses for Method 2.
- EPA Method 2 was employed for the determination of the stack gas velocity and volumetric flow rate during stack sampling using the Type “S” Pitot tube.
- Method 3 and 3A were used for the calculation of the density and dry molecular weight of the effluent stack gas.
- EPA Method 4 was used for the determination of moisture content. ODEQ Method 4 (ODEQ4) was used as the 2<sup>nd</sup> method for determining the moisture content of the stack gas. Specifically, ODEQ4 Equations 4.4-1 and 4.4-2 were used to calculate the theoretical maximum moisture content of the stack gas. The lower of these two values (actual vs. theoretical) was used for calculating dry standard volumetric flow rates (dscfm) and correcting Total Hydrocarbon (THC) emission concentrations to a dry basis.
- EPA Method 25A was used for the determination of volatile organic compounds (VOCs), measured as total hydrocarbons (THC) on a propane calibration basis.
- NCASI Method 105.01 was used to determine methanol, formaldehyde, phenol, acetaldehyde, acrolein, and propionaldehyde emissions. Source gas was drawn through midjet impingers, each containing chilled, organic-free water. Formaldehyde and methanol were absorbed by the water. To ensure QA/QC, a collocated duplicate sample train was operated simultaneously during each test run. The first test run was operated as a duplicate sample while the 2<sup>nd</sup> and 3<sup>rd</sup> runs were spiked with known quantities.

## 5.0 QUALITY ASSURANCE ACTIVITIES

The quality assurance/quality control (QA/QC) measures associated with the sampling and analysis procedures given in the noted EPA reference methodologies, in Subparts A of 40 CFR Part 60 and 40 CFR Part 63, and in the *EPA QA/QC Handbook*, Volume III (EPA 600/R-94/038c) were employed, as applicable. Such measures included, but were not limited to, the procedures detailed below.

### 5.1 PITOT TUBE FACE PLANE ALIGNMENT CHECK

Before field testing, each Type S Pitot tube was examined in order to verify that the face planes of the tube were properly aligned, per Method 2 of 40 CFR Part 60, Appendix A. The external tubing diameter and base-to-face plane distances were measured in order to verify the use of 0.84 as the baseline (isolated) Pitot coefficient. At that time the entire probe assembly (i.e., the sampling probe, nozzle, thermocouple, and Pitot tube) was inspected in order to verify that its components met the interference-free alignment specifications given in EPA Method 2. Because the specifications were met, then the baseline Pitot coefficient was used for the entire probe assembly.

After field testing, the face plane alignment of each Pitot tube was checked. No damage to the tube orifices was noted.

### 5.2 METERING SYSTEM CALIBRATION

Annually each dry gas meter (DGM) console is calibrated at five orifice settings according to Method 5 of 40 CFR Part 60, Appendix A. From the calibration data, calculations of the values of  $Y_m$  and  $\Delta H_{@}$  are made, and an average of each set of values is obtained. The limit of total variation of  $Y_m$  values is  $\pm 0.02$ , and the limit for  $\Delta H_{@}$  values is  $\pm 0.20$ .

After field testing, the calibration of the DGM console was checked by performing three calibration runs at a single intermediate orifice setting that is representative of the range used during field-testing. Each DGM was within the limit of acceptable relative variation from  $Y_m$  of 5.0%.



### **5.3 TEMPERATURE GAUGE CALIBRATION**

After field testing, the temperature measuring instruments on each sampling train was calibrated against standardized mercury-in-glass reference thermometers. Each indicated temperature was within the limit of acceptable variation between the absolute reference temperature and the absolute indicated temperature of 1.5%.

### **5.4 GAS ANALYZER CALIBRATION**

#### **5.4.1 CALIBRATION GAS CONCENTRATION VERIFICATION**

*AIR* obtained a certificate from the gas manufacturer and confirmed that the documentation included all information required by the Environmental Protection Agency Traceability Protocol No. 1. *AIR* confirmed that the manufacturer certification was complete and current and that calibration gases certifications had not expired. This documentation was available on-site for inspection during testing and is presented in Appendix E.

#### **5.4.2 MEASUREMENT SYSTEM PREPARATION**

*AIR* assembled, prepared, and preconditioned each measurement system by following the manufacturer's written instructions for preparing and preconditioning each gas analyzer and, as applicable, the other system components. *AIR* made all necessary adjustments to calibrate the analyzers and the data recorders and to achieve the correct sampling rate.

#### **5.4.3 ANALYZER CALIBRATION ERROR**

After sampling system and analyzer assembly, preparation and calibration, *AIR* conducted a 3-point analyzer calibration error test before the first run. *AIR* introduced the low-, mid-, and high-level calibration gases sequentially in direct calibration mode. During the test, *AIR* made no adjustments to the system except to maintain the correct flow rate. *AIR* recorded the analyzer's response to each calibration gas and calculated the system calibration error. At each calibration gas level (low, mid, and high) the calibration error was within  $\pm 2.0$  percent or 0.5 ppm of the calibration span.

#### 5.4.4 INITIAL SYSTEM BIAS AND CALIBRATION ERROR CHECKS

Before sampling began, *AIR* determined that the high-level calibration gas best approximated the emissions and used it as the upscale gas. *AIR* introduced the upscale gas at the probe upstream of all sample conditioning components in system calibration mode. The time it took for the measured concentration to increase to a value that is within 95 percent of the certified gas concentration was recorded. *AIR* continued to observe the gas concentration reading until it reached a final, stable value and recorded the value.

Next, *AIR* introduced the low-level gas in system calibration mode and recorded the time required for the concentration response to decrease to a value that was within 5.0 percent of the certified low-range gas concentration.

*AIR* continued to observe the low-level gas reading until it reached a final, stable value and recorded the result. *AIR* operated the measurement system at the normal sampling rate during all system bias checks and made only the adjustments necessary to achieve proper calibration gas flow rates at the analyzer. From this data, *AIR* determined the initial system bias was less than 5% of the calibration span for the low- and high- level gases.

#### 5.4.5 MEASUREMENT SYSTEM RESPONSE TIME

*AIR* calculated the measurement system response time from the data collected during the Initial System Bias Check.

### 5.5 NCASI 105.01 SPECIFIC QA CHECKS

Field personnel conducted the various method specific quality assurance checks and activities as required in NCASI 105.01. These included operating a collocated sample train for collecting duplicate and spiked samples as well as submitting a reagent blank. The laboratory also analyzed laboratory blanks, laboratory duplicates, and laboratory matrix spike samples. Each of these checks was conducted to verify the sampling systems' integrity and the laboratory's ability to provide accurate analytical data. The duplicate relative deviation and spike recovery assessments are delineated in the applicable Results table of Appendix A as well as within the laboratory report presented in Appendix E.

As previously stated, the first test run's collocated sample train was operated as a duplicate sample while the 2<sup>nd</sup> and 3<sup>rd</sup> runs were spiked with known quantities in the first impinger.

## **5.6 DATA REDUCTION CHECKS**

*AIR* ran an independent check (using a validated computer program) of the calculations with predetermined data before the field test, and the *AIR* Team Leader conducted spot checks on-site to assure that data was being recorded accurately. After the test, *AIR* checked the data input to assure that the raw data had been transferred to the computer accurately

## **5.7 EXTERNAL QUALITY ASSURANCE**

### **5.7.1 TEST PROTOCOL EVALUATION**

A notification was submitted to ODEQ in advance of testing, which provided regulatory personnel the opportunity to review and comment upon the test and quality assurance procedures used in conducting this testing.

### **5.7.2 ON-SITE TEST EVALUATION**

A test schedule was submitted with the notification and ODEQ personnel were notified of all changes in the schedule. No tests were performed earlier than stated in the original schedule. Therefore, regulatory personnel were afforded the opportunity for on-site evaluation of all test procedures.

## **6.0 DATA QUALITY OBJECTIVES**

The data quality objectives (DQOs) process is generally a seven-step iterative planning approach to ensure development of sampling designs for data collection activities that support decision making. The seven steps are as follows: (1) defining the problem; (2) stating decisions and alternative actions; (3) identifying inputs into the decision; (4) defining the study boundaries; (5) defining statistical parameters, specifying action levels, and developing action logic; (6) specifying acceptable error limits; and (7) selecting resource-effective sampling and analysis plan to meet the performance criteria. The first five steps are primarily focused on identifying qualitative criteria such as the type of data needed and defining how the data will be used. The sixth step defines quantitative criteria and the seventh step is used to develop a data collection design. In regards to emissions sampling, these steps have already been identified for typical monitoring parameters.

Monitoring methods presented in 40 CFR Part 60 Appendix A indicate the following regarding DQOs: Adherence to the requirements of this method will enhance the quality of the data obtained from air pollutant sampling methods. At a minimum, each method provides the following types of information: summary of method; equipment and supplies; reagents and standards; sample collection, preservation, storage, and transportation; quality control; calibration and standardization; analytical procedures, data analysis and calculations; and alternative procedures. These test methods have been designed and tested according to DQOs for emissions testing and analysis. These test methods have been specified and were followed in accordance with the test protocol discussed with GP Toledo to ensure that DQOs were met for this project.

**APPENDIX A**

**TEST RESULTS**

# Advanced Industrial Resources, Inc.

## Test Results

GP Toledo AMRS

Toledo, OR

Carbon Bed Outlet

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		Units	Run 1	Run 2	Run 3	Averages
<b>Test Date</b>			12-Jul-23	12-Jul-23	12-Jul-23	
<b>Start Time</b>			8:45	12:12	15:29	
<b>End Time</b>			11:45	14:32	18:01	
<b>Start Time Monitor Data</b>			8:45	12:12	15:29	
<b>Stop Time Monitor Data</b>			11:14	14:31	18:00	
<b>P<sub>m</sub></b>	Pressure of meter gases	inches Hg	30.23	30.23	30.23	<b>30.23</b>
<b>P<sub>s</sub></b>	Pressure of stack gases	inches Hg	30.14	30.14	30.14	<b>30.14</b>
<b>V<sub>m(std)</sub></b>	Volume of gas sample	dscf	111.62	100.03	107.66	<b>106.43</b>
<b>V<sub>w(std),meas</sub></b>	Meas. volume of water vapor	scf	1.20	0.91	1.79	<b>1.30</b>
<b>B<sub>ws,meas</sub></b>	Measured moisture	dimensionless	0.011	0.009	0.016	<b>0.012</b>
<b>B<sub>ws,theo</sub></b>	Theoretical max. moisture		0.031	0.036	0.036	<b>0.034</b>
<b>B<sub>ws,act</sub></b>	Actual moisture		0.011	0.009	0.016	<b>0.012</b>
<b>M<sub>d</sub></b>	Mol. Wt. Of gas at DGM	lb./lb.-mole	28.84	28.84	28.84	<b>28.84</b>
<b>M<sub>s</sub></b>	Mol. Wt. Of gas at stack	lb./lb.-mole	28.72	28.74	28.66	<b>28.71</b>
<b>v<sub>s</sub></b>	Velocity of stack gas	ft./sec	57.66	57.75	57.85	<b>57.76</b>
<b>A<sub>n</sub></b>	Area of nozzle	ft <sup>2</sup>	0.000218	0.000218	0.000218	<b>0.000218</b>
<b>A<sub>s</sub></b>	Area of stack	ft <sup>2</sup>	8.30	8.30	8.30	<b>8.30</b>
<b>Gas Stream Flow Rates, Temperature, Oxygen</b>						
<b>Q<sub>a</sub></b>	Vol. Flow rate of actual gas	cfm	28,700	28,747	28,796	<b>28,748</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfm	28,416	28,253	28,268	<b>28,312</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfh	1,704,937	1,695,175	1,696,107	<b>1,698,740</b>
<b>Q<sub>sd</sub></b>	Vol. Flow rate of dry gas	dscfm	28,114	27,997	27,807	<b>27,973</b>
<b>T<sub>s</sub></b>	Temperature of stack gas	°F	77	81	82	<b>80</b>
<b>% O<sub>2</sub></b>	Percent O2 by volume	percent (%v)	20.8	20.7	20.8	<b>20.8</b>
<b>Isokinetic Sampling Ratio</b>						
<b>I</b>	Isokinetic sampling ratio	percent	104.9	101.4	102.3	<b>102.9</b>
<b>Process Data</b>						
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/batch	19.9	21.2	21.0	<b>20.7</b>
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/hr	8.18	8.81	8.59	<b>8.53</b>
<b>Methanol Concentrations NCASI 105.01</b>						
<b>Methanol</b>	Conc. Of Methanol in dry stack gas	mg/dscm	0.635	1.22	1.59	<b>1.15</b>
		gr/dscf	0.000277	0.000532	0.000695	<b>0.000502</b>
<b>Methanol Mass Rates NCASI 105.01</b>						
<b>Methanol</b>	Emission rate of Methanol	lb/hour	0.0669	0.128	0.166	<b>0.120</b>
		lb/ton MSW	0.00818	0.0145	0.0193	<b>0.0140</b>
<b>Phenol Concentrations NCASI 105.01</b>						
<b>Phenol</b>	Conc. Of Phenol in dry stack gas	mg/dscm	J 0.0323	J 0.0378	0.0597	<b>0.0432</b>
		gr/dscf	J 0.0000141	J 0.0000165	0.0000261	<b>0.0000189</b>
<b>Phenol Mass Rates NCASI 105.01</b>						
<b>Phenol</b>	Emission rate of Phenol	lb/hour	J 0.00340	J 0.00396	0.00622	<b>0.00453</b>
		lb/ton MSW	J 0.000416	J 0.000450	0.000724	<b>0.000530</b>

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## Test Results

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<b>V<sub>m(std)</sub></b>	Volume of gas sample	dscf	111.62	100.03	107.66	<b>106.43</b>
<b>V<sub>w(std),meas</sub></b>	Meas. volume of water vapor	scf	1.20	0.91	1.79	<b>1.30</b>
<b>B<sub>ws,meas</sub></b>	Measured moisture	dimensionless	0.011	0.009	0.016	<b>0.012</b>
<b>B<sub>ws,theo</sub></b>	Theoretical max. moisture		0.031	0.036	0.036	<b>0.034</b>
<b>B<sub>ws,act</sub></b>	Actual moisture		0.011	0.009	0.016	<b>0.012</b>
<b>M<sub>d</sub></b>	Mol. Wt. Of gas at DGM	lb./lb.-mole	28.84	28.84	28.84	<b>28.84</b>
<b>M<sub>s</sub></b>	Mol. Wt. Of gas at stack	lb./lb.-mole	28.72	28.74	28.66	<b>28.71</b>
<b>v<sub>s</sub></b>	Velocity of stack gas	ft./sec	57.66	57.75	57.85	<b>57.76</b>
<b>A<sub>n</sub></b>	Area of nozzle	ft <sup>2</sup>	0.000218	0.000218	0.000218	<b>0.000218</b>
<b>A<sub>s</sub></b>	Area of stack	ft <sup>2</sup>	8.30	8.30	8.30	<b>8.30</b>
<b>Gas Stream Flow Rates, Temperature, Oxygen</b>						
<b>Q<sub>a</sub></b>	Vol. Flow rate of actual gas	cfm	28,700	28,747	28,796	<b>28,748</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfm	28,416	28,253	28,268	<b>28,312</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfh	1,704,937	1,695,175	1,696,107	<b>1,698,740</b>
<b>Q<sub>sd</sub></b>	Vol. Flow rate of dry gas	dscfm	28,114	27,997	27,807	<b>27,973</b>
<b>T<sub>s</sub></b>	Temperature of stack gas	°F	77	81	82	<b>80</b>
<b>% O<sub>2</sub></b>	Percent O2 by volume	percent (%v)	20.8	20.7	20.8	<b>20.8</b>
<b>Isokinetic Sampling Ratio</b>						
<b>I</b>	Isokinetic sampling ratio	percent	104.9	101.4	102.3	<b>102.9</b>
<b>Process Data</b>						
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/batch	19.9	21.2	21.0	<b>20.7</b>
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/hr	8.18	8.81	8.59	<b>8.53</b>
<b>Acetaldehyde Concentrations NCASI 105.01</b>						
<b>Acetaldehyde</b>	Conc. Of Acetaldehyde in dry stack gas	mg/dscm	0.561	0.960	1.08	<b>0.867</b>
		gr/dscf	0.000245	0.000419	0.000472	<b>0.000379</b>
<b>Acetaldehyde Mass Rates NCASI 105.01</b>						
<b>Acetaldehyde</b>	Emission rate of Acetaldehyde	lb/hour	0.0590	0.101	0.113	<b>0.0908</b>
		lb/ton MSW	0.00722	0.0114	0.0131	<b>0.0106</b>
<b>Acrolein Concentrations NCASI 105.01</b>						
<b>Acrolein</b>	Conc. Of Acrolein in dry stack gas	mg/dscm	< 1.46E-03	< 1.66E-03	< 1.55E-03	<b>&lt; 1.55E-03</b>
		gr/dscf	< 6.36E-07	< 7.26E-07	< 6.75E-07	<b>&lt; 6.79E-07</b>
<b>Acrolein Mass Rates NCASI 105.01</b>						
<b>Acrolein</b>	Emission rate of Acrolein	lb/hour	< 1.53E-04	< 1.74E-04	< 1.61E-04	<b>&lt; 1.63E-04</b>
		lb/ton MSW	< 1.87E-05	< 1.98E-05	< 1.87E-05	<b>&lt; 1.91E-05</b>
<b>Formaldehyde Concentrations NCASI 105.01</b>						
<b>Formaldehyde</b>	Conc. Of Formaldehyde in dry stack gas	mg/dscm	J 3.42E-03	J 5.26E-03	J 6.72E-03	<b>J 5.13E-03</b>
		gr/dscf	J 1.49E-06	J 2.30E-06	J 2.94E-06	<b>J 2.24E-06</b>
<b>Formaldehyde Mass Rates NCASI 105.01</b>						
<b>Formaldehyde</b>	Emission rate of Formaldehyde	lb/hour	J 3.60E-04	J 5.52E-04	J 7.00E-04	<b>J 5.37E-04</b>
		lb/ton MSW	J 4.40E-05	J 6.26E-05	J 8.16E-05	<b>J 6.27E-05</b>

# Advanced Industrial Resources, Inc.

## Test Results

GP Toledo AMRS

Toledo, OR

Carbon Bed Outlet

(< or ND) indicates the analyte was a non-detect or below the MDL, results displayed are the result of the the MDL.

(J) indicates the analyte was between the MDL and LOQ, the laboratory can positively identify the analyte as present but value is considered to be an estimate.

		Units	Run 1	Run 2	Run 3	Averages
<b>Test Date</b>			12-Jul-23	12-Jul-23	12-Jul-23	
<b>Start Time</b>			8:45	12:12	15:29	
<b>End Time</b>			11:45	14:32	18:01	
<b>Start Time Monitor Data</b>			8:45	12:12	15:29	
<b>Stop Time Monitor Data</b>			11:14	14:31	18:00	
<b>P<sub>m</sub></b>	Pressure of meter gases	inches Hg	30.23	30.23	30.23	<b>30.23</b>
<b>P<sub>s</sub></b>	Pressure of stack gases	inches Hg	30.14	30.14	30.14	<b>30.14</b>
<b>V<sub>m(std)</sub></b>	Volume of gas sample	dscf	111.62	100.03	107.66	<b>106.43</b>
<b>V<sub>w(std),meas</sub></b>	Meas. volume of water vapor	scf	1.20	0.91	1.79	<b>1.30</b>
<b>B<sub>ws,meas</sub></b>	Measured moisture	dimensionless	0.011	0.009	0.016	<b>0.012</b>
<b>B<sub>ws,theo</sub></b>	Theoretical max. moisture		0.031	0.036	0.036	<b>0.034</b>
<b>B<sub>ws,act</sub></b>	Actual moisture		0.011	0.009	0.016	<b>0.012</b>
<b>M<sub>d</sub></b>	Mol. Wt. Of gas at DGM	lb./lb.-mole	28.84	28.84	28.84	<b>28.84</b>
<b>M<sub>s</sub></b>	Mol. Wt. Of gas at stack	lb./lb.-mole	28.72	28.74	28.66	<b>28.71</b>
<b>v<sub>s</sub></b>	Velocity of stack gas	ft./sec	57.66	57.75	57.85	<b>57.76</b>
<b>A<sub>n</sub></b>	Area of nozzle	ft <sup>2</sup>	0.000218	0.000218	0.000218	<b>0.000218</b>
<b>A<sub>s</sub></b>	Area of stack	ft <sup>2</sup>	8.30	8.30	8.30	<b>8.30</b>
<b>Gas Stream Flow Rates, Temperature, Oxygen</b>						
<b>Q<sub>a</sub></b>	Vol. Flow rate of actual gas	cfm	28,700	28,747	28,796	<b>28,748</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfm	28,416	28,253	28,268	<b>28,312</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfh	1,704,937	1,695,175	1,696,107	<b>1,698,740</b>
<b>Q<sub>sd</sub></b>	Vol. Flow rate of dry gas	dscfm	28,114	27,997	27,807	<b>27,973</b>
<b>T<sub>s</sub></b>	Temperature of stack gas	°F	77	81	82	<b>80</b>
<b>% O<sub>2</sub></b>	Percent O2 by volume	percent (%v)	20.8	20.7	20.8	<b>20.8</b>
<b>Isokinetic Sampling Ratio</b>						
<b>I</b>	Isokinetic sampling ratio	percent	104.9	101.4	102.3	<b>102.9</b>
<b>Process Data</b>						
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/batch	19.9	21.2	21.0	<b>20.7</b>
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/hr	8.18	8.81	8.59	<b>8.53</b>
<b>Propionaldehyde Concentrations NCASI 105.01</b>						
<b>Propionaldehyde</b>	Conc. Of Propionaldehyde in dry stack gas	mg/dscm	J 2.37E-03	J 2.42E-03	J 3.41E-03	<b>J 2.74E-03</b>
		gr/dscf	J 1.04E-06	J 1.06E-06	J 1.49E-06	<b>J 1.19E-06</b>
<b>Propionaldehyde Mass Rates NCASI 105.01</b>						
<b>Propionaldehyde</b>	Emission rate of Propionaldehyde	lb/hour	J 2.50E-04	J 2.54E-04	J 3.55E-04	<b>J 2.86E-04</b>
		lb/ton MSW	J 3.06E-05	J 2.88E-05	J 4.14E-05	<b>J 3.36E-05</b>
<b>Total Hydrocarbon Concentrations Method 25A</b>						
<b>C<sub>THC</sub></b>	THC concentration (as propane)	ppm	9.23	10.30	9.06	<b>9.53</b>
<b>C<sub>THC</sub></b>	THC concentration (as propane)	mg/dscm	16.9	18.9	16.6	<b>17.4</b>
<b>C<sub>THC</sub></b>	THC concentration (as propane)	gr/dscf	0.0074	0.0082	0.0072	<b>0.0076</b>
<b>Total Hydrocarbon Mass Rates Method 25A</b>						
<b>E<sub>THC</sub></b>	THC emission rate (as propane)	lb/hour	1.78	1.98	1.73	<b>1.83</b>
<b>E<sub>THC</sub></b>	THC emission rate (as propane)	lb/ton MSW	0.22	0.22	0.20	<b>0.21</b>
<b>E<sub>THC All</sub></b>	Allowable THC emission rate	lb/ton MSW	0.40	0.40	0.40	<b>0.40</b>
<b>% Allow</b>	% of Allowable	%	54%	56%	50%	<b>54%</b>



# Advanced Industrial Resources, Inc.

## Test Results

GP Toledo AMRS

Toledo, OR

Carbon Bed Outlet

(< or ND) indicates the analyte was a non-detect or below the MDL, results displayed are the result of the the MDL.

(J) indicates the analyte was between the MDL and LOQ, the laboratory can positively identify the analyte as present but value is considered to be an estimate.

		Units	Run 1	Run 2	Run 3	Averages
<b>Test Date</b>			12-Jul-23	12-Jul-23	12-Jul-23	
<b>Start Time</b>			8:45	12:12	15:29	
<b>End Time</b>			11:45	14:32	18:01	
<b>Start Time Monitor Data</b>			8:45	12:12	15:29	
<b>Stop Time Monitor Data</b>			11:14	14:31	18:00	
<b>P<sub>m</sub></b>	Pressure of meter gases	inches Hg	30.23	30.23	30.23	<b>30.23</b>
<b>P<sub>s</sub></b>	Pressure of stack gases	inches Hg	30.14	30.14	30.14	<b>30.14</b>
<b>V<sub>m(std)</sub></b>	Volume of gas sample	dscf	111.62	100.03	107.66	<b>106.43</b>
<b>V<sub>w(std),meas</sub></b>	Meas. volume of water vapor	scf	1.20	0.91	1.79	<b>1.30</b>
<b>B<sub>ws,meas</sub></b>	Measured moisture	dimensionless	0.011	0.009	0.016	<b>0.012</b>
<b>B<sub>ws,theo</sub></b>	Theoretical max. moisture		0.031	0.036	0.036	<b>0.034</b>
<b>B<sub>ws,act</sub></b>	Actual moisture		0.011	0.009	0.016	<b>0.012</b>
<b>M<sub>d</sub></b>	Mol. Wt. Of gas at DGM	lb./lb.-mole	28.84	28.84	28.84	<b>28.84</b>
<b>M<sub>s</sub></b>	Mol. Wt. Of gas at stack	lb./lb.-mole	28.72	28.74	28.66	<b>28.71</b>
<b>v<sub>s</sub></b>	Velocity of stack gas	ft./sec	57.66	57.75	57.85	<b>57.76</b>
<b>A<sub>n</sub></b>	Area of nozzle	ft <sup>2</sup>	0.000218	0.000218	0.000218	<b>0.000218</b>
<b>A<sub>s</sub></b>	Area of stack	ft <sup>2</sup>	8.30	8.30	8.30	<b>8.30</b>
<b>Gas Stream Flow Rates, Temperature, Oxygen</b>						
<b>Q<sub>a</sub></b>	Vol. Flow rate of actual gas	cfm	28,700	28,747	28,796	<b>28,748</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfm	28,416	28,253	28,268	<b>28,312</b>
<b>Q<sub>w</sub></b>	Vol. Flow rate of wet gas	scfh	1,704,937	1,695,175	1,696,107	<b>1,698,740</b>
<b>Q<sub>sd</sub></b>	Vol. Flow rate of dry gas	dscfm	28,114	27,997	27,807	<b>27,973</b>
<b>T<sub>s</sub></b>	Temperature of stack gas	°F	77	81	82	<b>80</b>
<b>% O<sub>2</sub></b>	Percent O2 by volume	percent (%v)	20.8	20.7	20.8	<b>20.8</b>
<b>Isokinetic Sampling Ratio</b>						
<b>I</b>	Isokinetic sampling ratio	percent	104.9	101.4	102.3	<b>102.9</b>
<b>Process Data</b>						
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/batch	19.9	21.2	21.0	<b>20.7</b>
<b>P<sub>(product input)</sub></b>	Product input MSW	ton/hr	8.18	8.81	8.59	<b>8.53</b>
<b>Total VOC Mass Rates = (THC (as propane) + Methanol + Formaldehyde)</b>						
*Equ. A-1 Attachment 1 of ODEQ Guidance for Evaluating VOC Emissions						
<b>E<sub>THC</sub></b>	Emission rate THC (as propane)	lb/hour	1.78	1.98	1.73	<b>1.83</b>
<b>E<sub>Methanol</sub></b>	Emission rate of Methanol	lb/hour	0.07	0.13	0.17	<b>0.12</b>
<b>E<sub>Formaldehyde</sub></b>	Emission rate of Formaldehyde	lb/hour	J 3.60E-04	J 5.52E-04	J 7.00E-04	<b>J 5.37E-04</b>
<b>*E<sub>Total VOC</sub></b>	Emission rate of Total VOC	lb/hour	1.85	2.11	1.89	<b>1.95</b>
<b>E<sub>Total VOC</sub></b>	Emission rate of Total VOC	lb/ton MSW	0.226	0.239	0.220	<b>0.228</b>
<b>E<sub>Total VOC all</sub></b>	Allowable mission rate of Total VOC	lb/ton MSW	0.246	0.246	0.246	<b>0.246</b>
<b>E<sub>Total VOC all</sub></b>	% of Allowable	%	92%	97%	90%	<b>93%</b>

**APPENDIX B**

**FIELD DATA REDUCTION**

# Advanced Industrial Resources, Inc.

## Data Reduction Sheet

<b>Client:</b>	GP Toledo AMRS	<b>Console ID:</b>	C-009
<b>Location:</b>	Toledo, OR	<b>Y<sub>m</sub>:</b>	1.013
<b>Source:</b>	Carbon Bed Outlet	<b>ΔH<sub>@</sub>:</b>	1.554
<b>Test Team:</b>	JS, DK, DW	<b>C<sub>p</sub>:</b>	0.84
<b>EPA Methods:</b>	1, 2, 3, 4, 25A, NACSI 105.01	<b>Analyte(s):</b>	THC, HAPS

		Units	Run 1	Run 2	Run 3
<b>Test Date</b>			12-Jul-23	12-Jul-23	12-Jul-23
<b>Start Time</b>			8:45	12:12	15:29
<b>End Time</b>			11:45	14:32	18:01
<b>Start Time Monitor Data</b>			8:45	12:12	15:29
<b>Stop Time Monitor Data</b>			11:14	14:31	18:00
<b>V<sub>m</sub></b>	Volume of gas sample	dcf	108.425	98.778	106.568
<b>M<sub>lc</sub></b>	Mass of liquid collected	g	25.4	19.4	37.9
<b>Δp</b>	Velocity head of stack gas	inches H <sub>2</sub> O	1.041	1.037	1.036
<b>(Δp)<sup>1/2</sup></b>	Square root of velocity head	(inches H <sub>2</sub> O) <sup>1/2</sup>	1.019	1.017	1.017
<b>ΔH</b>	Pressure differential	inches H <sub>2</sub> O	1.56	1.56	1.55
<b>θ</b>	Total sampling time	minutes	144.0	134.0	144.0
<b>D<sub>n</sub></b>	Diameter of nozzle	inches	0.200	0.200	0.200
<b>D<sub>s</sub></b>	Diameter of stack	inches	39.0	39.0	39.0
<b>T<sub>m</sub></b>	Temperature of meter	°R	525	533	535
<b>T<sub>s</sub></b>	Temperature of stack gas	°R	537	541	542
<b>P<sub>bar</sub></b>	Barometric pressure	inches Hg	30.12	30.12	30.12
<b>P<sub>g</sub></b>	Gauge pressure of stack gas	inches H <sub>2</sub> O	0.30	0.30	0.30
<b>% O<sub>2</sub></b>	Percent O2 by volume	percent (✓/✓)	20.79	20.72	20.79
<b>% CO<sub>2</sub></b>	Percent CO2 by volume	percent (✓/✓)	0.03	0.05	0.03
<b>% N<sub>2</sub></b>	Percent N2 by volume	percent (✓/✓)	79.2	79.2	79.2
<b>P</b>	Product input MSW	ton/batch	19.9	21.2	21.0
<b>P</b>	Product input MSW	ton/hr	8.2	8.8	8.6
<b>m</b>	Mass of Methanol	mg	2.01	3.45	4.85
<b>m</b>	Mass of Phenol	mg	J 0.10	J 0.11	0.18
<b>m</b>	Mass of Acetaldehyde	mg	1.77	2.72	3.30
<b>m</b>	Mass of Acrolein	mg	< 0.0046	< 0.0047	< 0.0047
<b>m</b>	Mass of Formaldehyde	mg	J 0.011	J 0.015	J 0.021
<b>m</b>	Mass of Proionaldehyde	mg	J 0.008	J 0.007	J 0.010
<b>C<sub>THC(Wet)</sub></b>	THC Conc. (C <sub>3</sub> H <sub>8</sub> ,wet)	ppm <sub>w</sub>	9.13	10.21	8.91
<b>C<sub>THC(Dry)</sub></b>	THC Conc. (C <sub>3</sub> H <sub>8</sub> ,dry)	ppm <sub>D</sub> <sup>1</sup>	9.23	10.30	9.06

(< or ND) indicates the analyte was a non-detect or below the MDL, results displayed are the MDL.

(J) indicates the analyte was between the MDL and LOQ, the laboratory can positively identify the analyte as present but value is considered to be an estimate.

**APPENDIX C**

**EXAMPLE CALCULATIONS**

**AND**

**NOMENCLATURE**

# Advanced Industrial Resources, Inc.

## Sample Calculation Sheet

GP Toledo AMRS, Toledo, OR

Carbon Bed Outlet, Run #1

### Area of nozzle:

$$A_n = 3.1415 \times D_n^2 / 4 / 144 \text{ in}^2/\text{ft}^2$$

$$A_n = 3.1415 \times (0.2) / 4 / 144$$

$$A_n = 0.000218 \text{ ft}^2$$

### Area of stack:

$$A_s = 3.1415 \times D_s^2 / 4 / 144 \text{ in}^2/\text{ft}^2$$

$$A_s = 3.1415 \times (39) / 4 / 144$$

$$A_s = 8.30 \text{ ft}^2$$

### Absolute pressure of meter gases:

$$P_m = P_{\text{bar}} + \Delta H / 13.6$$

$$P_m = 30.12 + 1.562 / 13.6$$

$$P_m = 30.23 \text{ inches Hg}$$

### Absolute pressure of stack gases:

$$P_s = P_{\text{bar}} + p_g / 13.6$$

$$P_s = 30.12 + 0.3 / 13.6$$

$$P_s = 30.14 \text{ inches Hg}$$

### Volume of gas sample, standardized:

$$V_{m(\text{std})} = V_m \times Y_m (T_{\text{std}} / T_m) (P_m / P_{\text{std}})$$

$$V_{m(\text{std})} = (108.425) \times (1.013) \times 17.636 \times (30.23/525)$$

$$V_{m(\text{std})} = 111.54 \text{ dscf}$$

### Volume of water vapor in the gas sample, standardized:

$$V_{w(\text{std})} = (V_{\text{lc}} \times p_w \times R \times T_{\text{std}}) / (M_w \times P_{\text{std}})$$

$$V_{w(\text{std})} = (25.4) \times (0.002201) \times (21.85) \times (528) / (18 \times 29.92)$$

$$V_{w(\text{std})} = 1.20 \text{ scf}$$

### Volume proportion of water in the stack gas stream, measured:

$$B_{ws,\text{meas}} = V_{w(\text{std})} / (V_{m(\text{std})} + V_{w(\text{std})})$$

$$B_{ws,\text{meas}} = (1.2 / (111.54 + 1.2))$$

$$B_{ws,\text{meas}} = 0.0106$$

### Volume proportion of water in the stack gas stream, theoretical maximum:

$$B_{ws,\text{theo}} = \frac{((0.1805 \times \text{EXP}((17.27 \times T_s - 460 - 32)) / (T_s - 460 + 395))) - (((P_s - (0.1805 \times \text{EXP}((17.27 \times T_s - 460 - 32)) / (T_s - 460 + 395)))) \times 0) / (2800 - (1.3 \times T_s - 460))}{P_s}$$

$$B_{ws,\text{theo}} = \frac{((0.1805 \times \text{EXP}((17.27 \times 537.25 - 460 - 32)) / (537.25 - 460 + 395))) - (((30.1420588235294 - (0.1805 \times \text{EXP}((17.27 \times 537.25 - 460 - 32)) / (537.25 - 460 + 395)))) \times 0) / (2800 - (1.3 \times 537.25 - 460))}{30.1420588235294}$$

$$B_{ws,\text{theo}} = 0.0310$$

\*Note: Values may not agree exactly with results shown elsewhere in this report due strictly to rounding

# Advanced Industrial Resources, Inc.

## Sample Calculation Sheet

GP Toledo AMRS, Toledo, OR  
Carbon Bed Outlet, Run #1

### Volume proportion of water in the stack gas stream:

$$B_{ws,act} = \text{lower of } B_{ws,meas} \text{ and } B_{ws,theo}$$

$$B_{ws,act} = 0.0106$$

### Nitrogen content of gas at the DGM:

$$\%N_2 = 100\% - \%CO_2 - \%O_2 - \%CO$$

$$\%N_2 = 100\% - 0.03\% - 20.79\% - 0\%$$

$$\%N_2 = 79.2 \quad \%$$

### Molecular weight of gas at the DGM:

$$M_d = ((44 \times \%CO_2) + (32 \times \%O_2) + (28 \times (\%N_2 + \%CO)))/100\%$$

$$M_d = ((44 \times 0.03) + (32 \times 20.79) + (28 (79.2 + 0)))/100\%$$

$$M_d = 28.84 \quad \text{lb/lb-mole}$$

### Molecular weight of gas at the stack:

$$M_s = M_d (1 - B_{ws}) + M_w \times B_{ws}$$

$$M_s = (28.84 \times (1 - 0.0106)) + (18 \times 0.0106)$$

$$M_s = 28.73 \quad \text{lb/lb-mole}$$

### Velocity of stack gas:

$$v_s = K_p \times C_p [\Delta p]^{1/2} \times [T_s / (P_s M_s)]^{1/2}$$

$$v_s = (85.49 \times 0.84 \times 1.019 \times [537 / (30.14 \times 28.73)]^{1/2}$$

$$v_s = 57.66 \quad \text{ft/s}$$

### Volumetric flow rate of actual stack gas:

$$Q_a = v_s \times A_s \times 60 \text{ sec/min}$$

$$Q_a = (57.66) \times (8.3) \times (60 \text{ sec/min})$$

$$Q_a = 28715 \quad \text{cfm}$$

### Volumetric flow rate of dry stack gas, standardized:

$$Q_{sd} = (60 \text{ sec/min}) \times (1 - B_{ws}) \times v_s \times A_s \times (T_{std} / T_s) \times (P_s / P_{std})$$

$$Q_{sd} = (60 \text{ sec/min}) \times (1 - 0.0106) \times 57.66 \times 8.3 \times (528 / 537) \times (30.14 / 29.92)$$

$$Q_{sd} = 28,114 \quad \text{dscfm}$$

# Advanced Industrial Resources, Inc.

## Sample Calculation Sheet

GP Toledo AMRS, Toledo, OR

Carbon Bed Outlet, Run #1

**Isokinetic sampling ratio expressed as percentage:**

$$I = 100 T_s [(K_s \times M_{ic}) + (Y_m \times V_m \times P_m / T_m)] / (60 \times \theta \times v_s \times P_s \times A_n)$$

$$I = 100 \times (537) \times ((0.002668 \times 25.4) + (1.013 \times 108.425 \times 30.23 / 525)) / (60 \times 150 \times 57.66 \times 30.14 \times 0.000218)$$

$$I = 104.9 \quad \%$$

**Concentration of THC (as C3H8) in dry stack gas, standardized:**

$$c = c_{ppm} \times M_{analyte} / 24.05$$

$$c = 9.23 \times 44 / 24.05$$

$$c = 16.9 \quad \text{mg/dscm}$$

**Emission rate of THC (as C3H8), time basis:**

$$E = (c_{mg/dscm} \times Q_{sd} ((60 \text{ min/hr}) (2.2046 \times 10^{-6} \text{ lb./mg}) / (35.32 \text{ ft}^3 / \text{m}^3))$$

$$E = 16.89 \times 28113.9 \times (60 \text{ min/hr}) (2.2046 \times 10^{-6} \text{ lb./mg}) / (35.32 \text{ ft}^3 / \text{m}^3)$$

$$E = 1.78 \quad \text{lb/hr}$$

**Emission rate of THC (as C3H8), time basis:**

$$E = \text{lb/hr} / \text{tons/MSW}$$

$$E = 1.778 / 8.18$$

$$E = 0.217 \quad \text{lb/ton MSW}$$

# Advanced Industrial Resources, Inc.

## Sample Calculation Sheet

GP Toledo AMRS, Toledo, OR

Carbon Bed Outlet, Run #1

### Concentration of Methanol in dry stack gas, standardized:

$$c = (m / V_{m(\text{std})}) (35.32 \text{ ft}^3 / \text{m}^3)$$

$$c = (2.008 / 111.54) \times 35.32$$

$$c = \mathbf{0.64 \quad \text{mg/dscm}}$$

M

### Concentration of Methanol in dry stack gas, standardized:

$$c = (\text{mg/dscm}) / (35.32 \text{ ft}^3 / \text{m}^3) / (64.8 \text{ mg/gr})$$

$$c = (0.635) / 35.32 / 64.8$$

$$c = \mathbf{0.000277 \quad \text{gr/dscf}}$$

### Emission rate of Methanol, time basis:

$$E = c_{\text{mg/dscm}} \times Q_{\text{sd}} \times (60 \text{ min/hr}) \times (2.2046 \times 10^{-6} \text{ lb/mg}) / (35.32 \text{ ft}^3 / \text{m}^3)$$

$$E = 0.635 \times 28113.9 \times 60 \times 2.2046 \times 10^{-6} / 35.32$$

$$E = \mathbf{0.067 \quad \text{lb/hr}}$$

### Emission rate of Methanol, time basis:

$$E = \text{lb/hr} / \text{tons/MSW}$$

$$E = 0.06686 / 8.18$$

$$E = \mathbf{0.0082 \quad \text{lb/ton MSW}}$$

### Concentration of Formaldehyde in dry stack gas, standardized:

$$c = (m / V_{m(\text{std})}) (35.32 \text{ ft}^3 / \text{m}^3)$$

$$c = (0.0108 / 111.54) \times 35.32$$

$$c = \mathbf{0.0030 \quad \text{mg/dscm}}$$

### Concentration of Formaldehyde in dry stack gas, standardized:

$$c = (\text{mg/dscm}) / (35.32 \text{ ft}^3 / \text{m}^3) / (64.8 \text{ mg/gr})$$

$$c = (0.003) / 35.32 / 64.8$$

$$c = \mathbf{0.0000015 \quad \text{gr/dscf}}$$

### Emission rate of Formaldehyde, time basis:

$$E = c_{\text{mg/dscm}} \times Q_{\text{sd}} \times (60 \text{ min/hr}) \times (2.2046 \times 10^{-6} \text{ lb/mg}) / (35.32 \text{ ft}^3 / \text{m}^3)$$

$$E = 0.003 \times 28113.9 \times 60 \times 2.2046 \times 10^{-6} / 35.32$$

$$E = \mathbf{0.00036 \quad \text{lb/hr}}$$

### Emission rate of Formaldehyde, time basis:

$$E = \text{lb/hr} / \text{tons/MSW}$$

$$E = 0.00036 / 8.18$$

$$E = \mathbf{0.000044 \quad \text{lb/ton MSW}}$$

### Total VOC Mass Rates:

$$E = (\text{THC lb/hr} + \text{Methanol lb/hr} + \text{Formaldehyde lb/hr}) / \text{tons/MSW}$$

$$E = 1.78 + 0.07 + 0.0004 / 8.18$$

$$E = \mathbf{0.226}$$

\*Note: Values may not agree exactly with results shown elsewhere in this report due strictly to rounding



## EXAMPLE CALCULATIONS

$$A_n = D_n^2 \pi / 4$$

$$A_s = D_s^2 \pi / 4$$

$$B_{ws} = V_{w(std)} / (V_{m(std)} + V_{w(std)})$$

$$c_{\text{analyte}} = (m_{\text{analyte}} / V_{m(std)}) (35.31466 \text{ ft}^3/\text{m}^3)$$

$$c'_{\text{analyte}} = (m_{\text{analyte}} / V_{m(std)}) (0.015432 \text{ gr/mg})$$

$$c_{\text{analyte}} = c'_{\text{analyte}} \text{ MW}_{\text{analyte}} / 24.04 \text{ l/mol}$$

$$\text{CC} = t_{0.975} (S_d / n^{1/2})$$

$$d = 1/n (S_{d_i})$$

$$\text{DE} = (E_{\text{Inlet}} - E_{\text{Outlet}}) / E_{\text{Inlet}} \times 100\%$$

$$E_{\text{analyte}} = (m_{\text{analyte}} / V_{m(std)}) Q_{sd} (60 \text{ min/hr}) (2.2046 \times 10^{-6} \text{ lb./mg})$$

$$E_{\text{analyte}} = c_{\text{analyte}} Q_{sd} (60 \text{ min/hr}) (2.2046 \times 10^{-6} \text{ lb./mg})$$

$$I = 100 T_s (K_3 V_{lc} + Y_m V_m P_m / T_m) / (60 \theta v_s P_s A_n)$$

$$\text{where } K_3 = 0.002668 (\text{in. Hg ft}^3) / (\text{mL } ^\circ\text{R})$$

$$K_I = [(2.0084 \times 10^7 \Delta H_{@}) A_n (1 - B_{ws})]^2 (M_d / M_s) (T_m / T_s) (P_s / P_m)$$

$$M_d = 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2) + 0.28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_s = M_d (1 - B_{ws}) + M_w B_{ws}$$

$$P = Q_{sd} / \text{F-Factor} \times 60 \times (20.9 - \text{O}_2) / 20.9$$

$$P_m = P_{\text{bar}} + \Delta H / 13.6$$

$$P_s = P_{\text{bar}} + p_g / 13.6$$

$$Q_a = (60 \text{ s/min}) v_s A_s$$

$$Q_{sd} = (60 \text{ s/min}) (1 - B_{ws}) v_s A_s (T_{\text{std}} / T_s) (P_s / P_{\text{std}})$$

$$\text{RA} = [\text{Abs}(d) + \text{Abs}(\text{CC})] / \text{RM}$$

$$S_d = [(S_{d_i}^2 - (S_{d_i})^2/n)/(n-1)]^{1/2}$$

$$T_m = t_m + 460^\circ$$

$$T_s = t_s + 460^\circ$$

$$V_{m(std)} = 17.636 V_m Y_m (P_m / T_m)$$

$$V_{w(std)} = M_{lc} \times 0.04716$$

$$v_s = K_p C_p [\Delta p]^{1/2} [T_s / (P_s M_s)]^{1/2}$$

## NOMENCLATURE

Symbol	Units	Description
<b>Abs(x)</b>	dimensionless	Absolute value of parameter x
<b>A<sub>n</sub></b>	ft <sup>2</sup>	Area of the nozzle
<b>A<sub>s</sub></b>	ft <sup>2</sup>	Area of the stack
<b>B<sub>ws</sub></b>	dimensionless	Volume proportion of water in the stack gas stream
<b>C<sub>p</sub></b>	dimensionless	Type S pitot tube coefficient
<b>C<sub>analyte</sub></b>	mg/dscm	Concentration of analyte in dry stack gas, standardized
<b>'C<sub>analyte</sub></b>	gr./dscf	Concentration of analyte in dry stack gas, standardized
<b>'C<sub>analyte</sub></b>	ppm	Concentration of analyte in dry stack gas, standardized
<b>CC</b>	dimensionless	One-tailed 2.5% error confidence coefficient
<b>d</b>	ppm	Arithmetic mean of differences
<b>d<sub>i</sub></b>	ppm	Difference between individual CEM and reference method concentration value
<b>D<sub>n</sub></b>	inches	Internal diameter of the nozzle at the entrance orifice
<b>D<sub>s</sub></b>	inches	Internal diameter of the stack at sampling location
<b>DE</b>	percent	Destruction efficiency
<b>ΔH</b>	inches H <sub>2</sub> O	Average pressure differential across the meter orifice
<b>ΔH<sub>@</sub></b>	inches H <sub>2</sub> O	Orifice pressure differential that corresponds to 0.75 cfm of air at 68 °F and 29.92 inches of Hg
<b>Δp</b>	inches H <sub>2</sub> O	Velocity head of stack gas
<b>E<sub>analyte</sub></b>	lb./hour	Emission rate of analyte, time basis
<b>I</b>	percent	Isokinetic sampling ratio expressed as percentage
<b>K<sub>I</sub></b>	dimensionless	K-factor, ratio of DH to DP, ideal
<b>K<sub>p</sub></b>	ft[(lb/lb-mol)(in. Hg)] <sup>1/2</sup>	Type S pitot tube constant,
	s[(°R)(in. H <sub>2</sub> O)] <sup>1/2</sup>	= 85.49
<b>L<sub>p</sub></b>	cfm	Measured post-test leakage rate of the sampling train
<b>M<sub>d</sub></b>	lb./lb.-mole	Molecular weight of gas at the DGM
<b>M<sub>s</sub></b>	lb./lb.-mole	Molecular weight of gas at the stack

## NOMENCLATURE

Symbol	Units	Description
$M_w$	lb./lb.-mole	Molecular weight of water,
		= 18.0
$m_{\text{analyte}}$	mg	Mass of analyte in the sample
$n$	dimensionless	Number of data points
$P$	MMBtu	Fuel firing rate
$P_{\text{bar}}$	inches Hg	Barometric pressure at measurement site
$P_{\text{input}}$	tons/hour	Process dry mass input rate
$p_g$	inches H <sub>2</sub> O	Gauge (static) pressure of stack gas
$P_m$	inches Hg	Absolute pressure of meter gases
$P_s$	inches Hg	Absolute pressure of stack gases
$P_{\text{std}}$	inches Hg	Standard absolute pressure
		= 29.92
$Q_a$	cfm	Volumetric flow rate of actual stack gas
$Q_{\text{sd}}$	dscfm	Volumetric flow rate of dry stack gas, standardized
$R$	(in. Hg)(ft <sup>3</sup> )	Ideal gas constant,
	(lb-mole)(°R)	= 21.85
$RA$	percent	Relative accuracy
$RE$	percent	Removal efficiency
$RM$	ppm	Average reference method concentration
$r_w$	lb/mL	Density of water,
		= 0.002201
$r_a$	g/mL	Density of acetone,
		= 0.7899
$S_d$	dimensionless	Standard deviation
$T_m$	°R	Absolute temperature of dry gas meter
$T_s$	°R	Absolute temperature of stack gas
$T_{\text{std}}$	°R	Standard absolute temperature,
		= 528
$t_{0.975}$	dimensionless	2.5 percent error t-value
$t_m$	°F	Temperature of DGM
$t_s$	°F	Temperature of stack gas
$\theta$	minutes	Total sampling time

## NOMENCLATURE

<b>Symbol</b>	<b>Units</b>	<b>Description</b>
<b>M<sub>lc</sub></b>	g	Total mass of liquid collected
<b>V<sub>m</sub></b>	dcf	Volume of gas sample as measured by the DGM
<b>V<sub>m(std)</sub></b>	dscf	Volume of gas sample as measured by the DGM, standardized
<b>V<sub>w(std)</sub></b>	scf	Volume of water vapor in the gas sample, standardized
<b>v<sub>s</sub></b>	ft./sec	Velocity of stack gas
<b>Y<sub>m</sub></b>	dimensionless	DGM calibration coefficient
<b>Y<sub>c</sub></b>	dimensionless	DGM calibration check value
<b>Y<sub>w</sub></b>	dimensionless	Reference (wet) gas meter calibration coefficient
<b>% CO<sub>2</sub></b>	percent	Percent CO <sub>2</sub> by volume, dry basis
<b>% O<sub>2</sub></b>	percent	Percent O <sub>2</sub> by volume, dry basis
<b>% N<sub>2</sub></b>	percent	Percent N <sub>2</sub> by volume, dry basis

## **APPENDIX D**

## **FIELD DATA**

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 6:30	20.63	0.02	2.38	6.23	
7/12/2023 6:31	20.01	12.36	2.29	6.22	
7/12/2023 6:32	20.00	17.99	2.18	6.19	
7/12/2023 6:33	20.01	17.99	2.16	6.09	
7/12/2023 6:34	19.67	17.99	2.20	6.04	
7/12/2023 6:35	0.00	0.90	2.14	6.02	
7/12/2023 6:36	0.00	0.00	2.06	5.96	
7/12/2023 6:37	0.00	0.00	2.03	5.90	
7/12/2023 6:38	0.00	0.00	1.97	5.85	
7/12/2023 6:39	4.21	6.41	1.88	5.78	
7/12/2023 6:40	11.00	9.00	1.96	5.76	
7/12/2023 6:41	11.00	9.00	2.70	5.74	
7/12/2023 6:42	11.00	9.00	2.03	5.70	
7/12/2023 6:43	0.21	0.60	1.87	5.67	
7/12/2023 6:44	5.90	0.00	2.31	5.63	
7/12/2023 6:45	1.41	0.02	2.76	5.58	
7/12/2023 6:46	0.02	0.02	3.69	5.54	
7/12/2023 6:47	0.02	0.02	1.53	5.50	
7/12/2023 6:48	0.76	0.02	0.94	5.48	
7/12/2023 6:49	11.02	8.45	0.67	5.44	
7/12/2023 6:50	11.02	8.90	0.51	5.41	
7/12/2023 6:51	11.02	8.89	0.47	5.39	
7/12/2023 6:52	11.02	8.90	0.45	5.37	
7/12/2023 6:53	11.02	8.90	0.44	5.35	
7/12/2023 6:54	11.02	8.90	0.88	5.34	
7/12/2023 6:55	11.97	8.01	-0.82	5.35	
7/12/2023 6:56	20.56	0.00	0.03	5.33	
7/12/2023 6:57	20.55	0.00	0.05	5.32	
7/12/2023 6:58	20.08	0.00	36.36	5.32	
7/12/2023 6:59	17.09	0.00	94.79	5.32	
7/12/2023 7:00	16.91	0.00	95.03	5.31	
7/12/2023 7:01	16.91	0.00	95.01	5.32	
7/12/2023 7:02	16.92	0.00	87.09	5.31	
7/12/2023 7:03	18.34	0.00	51.84	5.28	
7/12/2023 7:04	18.39	0.00	49.95	5.23	
7/12/2023 7:05	18.39	0.00	50.02	5.20	
7/12/2023 7:06	18.40	0.00	45.16	5.17	
7/12/2023 7:07	19.05	0.00	35.48	5.13	
7/12/2023 7:08	18.97	0.00	34.98	5.12	
7/12/2023 7:09	18.97	0.00	34.96	5.10	
7/12/2023 7:10	19.06	0.00	23.42	5.08	
7/12/2023 7:11	20.68	0.00	5.25	6.56	
7/12/2023 7:12	20.78	0.01	5.07	4.51	
7/12/2023 7:13	20.77	0.01	5.11	4.28	
7/12/2023 7:14	20.77	0.01	5.13	3.16	
7/12/2023 7:15	20.77	0.02	5.14	0.01	
7/12/2023 7:16	20.77	0.01	5.14	-0.03	
7/12/2023 7:17	20.77	0.01	5.13	-0.04	
7/12/2023 7:18	20.77	0.01	5.11	-0.06	
7/12/2023 7:19	20.77	0.01	5.11	78.20	
7/12/2023 7:20	20.77	0.01	5.11	95.10	
7/12/2023 7:21	20.77	0.01	5.09	95.15	
7/12/2023 7:22	20.77	0.01	5.09	95.05	
7/12/2023 7:23	20.78	0.01	5.06	94.84	
7/12/2023 7:24	20.78	0.01	5.06	94.72	
7/12/2023 7:25	20.78	0.01	5.06	83.09	
7/12/2023 7:26	20.78	0.01	5.06	51.31	
7/12/2023 7:27	20.78	0.01	5.04	50.04	
7/12/2023 7:28	20.79	0.01	5.03	50.02	
7/12/2023 7:29	20.79	0.01	5.03	50.07	
7/12/2023 7:30	20.79	0.01	5.02	35.01	
7/12/2023 7:31	20.79	0.01	5.01	35.25	
7/12/2023 7:32	20.80	0.01	5.00	35.23	
7/12/2023 7:33	20.80	0.01	5.00	35.09	
7/12/2023 7:34	20.79	0.01	5.01	17.79	
7/12/2023 7:35	20.11	15.24	5.02	10.83	
7/12/2023 7:36	20.09	17.98	5.00	1.23	
7/12/2023 7:37	20.08	17.99	5.00	0.73	
7/12/2023 7:38	20.81	14.21	5.00	0.65	
7/12/2023 7:39	20.82	0.02	5.00	0.66	
7/12/2023 7:40	20.81	0.01	5.01	0.67	
7/12/2023 7:41	20.82	0.02	5.00	0.64	
7/12/2023 7:42	20.82	0.01	4.99	0.64	
7/12/2023 7:43	20.83	0.02	4.97	0.64	
7/12/2023 7:44	20.83	0.01	4.97	0.63	
7/12/2023 7:45	20.83	0.01	4.97	0.62	

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 7:46	20.83	0.01	4.97	0.63	
7/12/2023 7:47	20.83	0.01	4.99	0.66	
7/12/2023 7:48	20.84	0.01	4.99	0.67	
7/12/2023 7:49	20.84	0.01	4.97	0.67	
7/12/2023 7:50	20.84	0.01	4.94	0.66	
7/12/2023 7:51	20.85	0.01	4.93	0.64	
7/12/2023 7:52	20.85	0.01	4.91	0.63	
7/12/2023 7:53	20.84	0.01	4.91	0.58	
7/12/2023 7:54	20.85	0.01	4.90	0.58	
7/12/2023 7:55	20.84	0.01	4.88	0.57	
7/12/2023 7:56	20.84	0.01	4.86	0.55	
7/12/2023 7:57	20.84	0.01	4.85	0.55	
7/12/2023 7:58	20.85	0.01	4.83	0.54	
7/12/2023 7:59	20.85	0.01	4.81	0.51	
7/12/2023 8:00	20.84	0.01	4.82	0.51	
7/12/2023 8:01	20.84	0.01	4.82	0.52	
7/12/2023 8:02	20.85	0.01	4.84	0.51	
7/12/2023 8:03	20.85	0.01	4.83	0.50	
7/12/2023 8:04	20.85	0.01	4.82	0.50	
7/12/2023 8:05	20.85	0.01	4.83	0.49	
7/12/2023 8:06	20.84	0.01	4.82	0.49	
7/12/2023 8:07	20.85	0.01	4.82	0.47	
7/12/2023 8:08	20.85	0.02	4.82	0.49	
7/12/2023 8:09	20.85	0.02	4.81	0.47	
7/12/2023 8:10	20.85	0.01	4.82	0.46	
7/12/2023 8:11	20.85	0.01	4.82	0.45	
7/12/2023 8:12	20.85	0.01	4.81	0.45	
7/12/2023 8:13	20.85	0.01	4.80	0.46	
7/12/2023 8:14	20.85	0.01	4.78	0.45	
7/12/2023 8:15	20.85	0.01	4.78	0.46	
7/12/2023 8:16	20.85	0.01	4.79	0.47	
7/12/2023 8:17	20.85	0.01	4.80	0.47	
7/12/2023 8:18	20.86	0.01	4.80	0.47	
7/12/2023 8:19	20.86	0.01	4.80	0.49	
7/12/2023 8:20	20.86	0.01	4.81	0.48	
7/12/2023 8:21	20.85	0.01	4.81	0.49	
7/12/2023 8:22	20.85	0.01	4.83	0.49	
7/12/2023 8:23	20.86	0.01	4.82	0.49	
7/12/2023 8:24	20.86	0.01	4.80	0.49	
7/12/2023 8:25	20.86	0.01	4.80	0.49	
7/12/2023 8:26	20.85	0.01	4.82	0.51	
7/12/2023 8:27	20.85	0.01	4.83	0.52	
7/12/2023 8:28	20.86	0.01	4.84	0.53	
7/12/2023 8:29	20.86	0.01	4.85	0.54	
7/12/2023 8:30	20.85	0.01	4.85	0.55	
7/12/2023 8:31	20.85	0.01	4.85	0.55	
7/12/2023 8:32	20.85	0.01	4.83	0.53	
7/12/2023 8:33	20.85	0.01	4.83	0.53	
7/12/2023 8:34	20.86	0.01	4.82	0.53	
7/12/2023 8:35	20.86	0.01	4.82	0.46	
7/12/2023 8:36	20.85	0.01	4.80	0.44	
7/12/2023 8:37	20.85	0.01	4.80	0.45	
7/12/2023 8:38	20.85	0.01	4.82	0.49	
7/12/2023 8:39	20.85	0.01	4.83	0.52	
7/12/2023 8:40	20.85	0.01	4.83	0.53	
7/12/2023 8:41	20.85	0.01	4.83	0.53	
7/12/2023 8:42	20.85	0.01	4.86	0.53	
7/12/2023 8:43	20.85	0.01	4.87	0.53	
7/12/2023 8:44	20.85	0.01	4.88	0.52	
Run 1 Start					
7/12/2023 8:45	20.86	0.01	4.89	0.53	-831%
7/12/2023 8:46	20.85	0.01	4.91	0.54	-814%
7/12/2023 8:47	20.85	0.01	4.91	0.55	-798%
7/12/2023 8:48	20.85	0.01	4.91	0.55	-796%
7/12/2023 8:49	20.85	0.01	4.92	0.62	-698%
7/12/2023 8:50	20.85	0.01	4.95	0.88	-465%
7/12/2023 8:51	20.85	0.01	4.99	1.35	-270%
7/12/2023 8:52	20.84	0.02	5.02	2.92	-72%
7/12/2023 8:53	20.84	0.03	5.07	4.59	-10%
7/12/2023 8:54	20.84	0.04	5.10	4.79	-6%
7/12/2023 8:55	20.83	0.04	5.14	3.82	-34%
7/12/2023 8:56	20.83	0.05	5.17	4.25	-22%
7/12/2023 8:57	20.84	0.06	5.18	3.17	-64%
7/12/2023 8:58	20.84	0.06	5.20	3.32	-56%
7/12/2023 8:59	20.85	0.05	5.33	2.95	-81%
7/12/2023 9:00	20.82	0.06	5.42	74.07	93%

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 9:01	20.82	0.08	5.85	42.11	86%
7/12/2023 9:02	20.81	0.09	5.54	29.59	81%
7/12/2023 9:03	20.85	0.11	5.21	7.75	33%
7/12/2023 9:04	20.86	0.06	5.15	5.02	-3%
7/12/2023 9:05	20.86	0.04	5.11	4.42	-16%
7/12/2023 9:06	20.86	0.03	5.08	4.20	-21%
7/12/2023 9:07	20.86	0.02	5.06	4.15	-22%
7/12/2023 9:08	20.86	0.02	5.06	4.15	-22%
7/12/2023 9:09	20.86	0.02	5.07	4.17	-22%
7/12/2023 9:10	20.86	0.02	5.07	4.17	-22%
7/12/2023 9:11	20.87	0.02	5.09	4.12	-23%
7/12/2023 9:12	20.86	0.01	5.10	4.05	-26%
7/12/2023 9:13	20.86	0.01	5.13	3.95	-30%
7/12/2023 9:14	20.87	0.01	5.15	3.84	-34%
7/12/2023 9:15	20.86	0.02	5.17	3.71	-39%
7/12/2023 9:16	20.86	0.02	5.17	3.58	-44%
7/12/2023 9:17	20.86	0.01	5.19	3.46	-50%
7/12/2023 9:18	20.86	0.01	5.21	3.34	-56%
7/12/2023 9:19	20.86	0.01	5.23	3.19	-64%
7/12/2023 9:20	20.86	0.01	5.25	3.10	-69%
7/12/2023 9:21	20.85	0.01	5.26	3.03	-74%
7/12/2023 9:22	20.86	0.01	5.29	2.95	-79%
7/12/2023 9:23	20.85	0.01	5.31	2.89	-84%
7/12/2023 9:24	20.85	0.01	5.34	2.83	-89%
7/12/2023 9:25	20.85	0.01	5.35	2.77	-93%
7/12/2023 9:26	20.85	0.01	5.36	2.73	-97%
7/12/2023 9:27	20.85	0.01	5.38	2.69	-100%
7/12/2023 9:28	20.84	0.01	5.41	2.65	-104%
7/12/2023 9:29	20.85	0.01	5.44	2.62	-108%
7/12/2023 9:30	20.85	0.01	5.48	2.59	-111%
7/12/2023 9:31	20.85	0.01	5.50	2.56	-115%
7/12/2023 9:32	20.85	0.01	5.52	2.54	-118%
7/12/2023 9:33	20.85	0.01	5.52	2.51	-120%
7/12/2023 9:34	20.85	0.01	5.54	2.48	-124%
7/12/2023 9:35	20.85	0.01	5.56	2.45	-127%
7/12/2023 9:36	20.86	0.01	5.58	2.43	-130%
7/12/2023 9:37	20.85	0.01	5.61	2.43	-131%
7/12/2023 9:38	20.85	0.02	5.61	2.45	-130%
7/12/2023 9:39	20.85	0.02	5.65	2.47	-129%
7/12/2023 9:40	20.85	0.01	5.68	2.48	-129%
7/12/2023 9:41	20.85	0.01	5.70	2.49	-129%
7/12/2023 9:42	20.86	0.01	5.71	2.51	-128%
7/12/2023 9:43	20.85	0.01	5.73	2.52	-128%
7/12/2023 9:44	20.85	0.01	5.73	2.51	-128%
7/12/2023 9:45	20.85	0.01	5.75	2.49	-131%
7/12/2023 9:46	20.85	0.01	5.76	2.46	-134%
7/12/2023 9:47	20.85	0.01	5.76	2.44	-136%
7/12/2023 9:48	20.85	0.01	5.75	2.41	-138%
7/12/2023 9:49	20.85	0.01	5.74	2.40	-140%
7/12/2023 9:50	20.85	0.01	5.74	2.37	-142%
7/12/2023 9:51	20.85	0.01	5.73	2.35	-144%
7/12/2023 9:52	20.85	0.01	5.73	2.32	-147%
7/12/2023 9:53	20.85	0.01	5.76	2.32	-149%
7/12/2023 9:54	20.85	0.01	5.78	2.34	-148%
7/12/2023 9:55	20.85	0.02	5.79	2.34	-147%
7/12/2023 9:56	20.85	0.01	5.80	2.31	-151%
7/12/2023 9:57	20.85	0.01	5.82	2.31	-151%
7/12/2023 9:58	20.85	0.01	5.85	2.31	-153%
7/12/2023 9:59	20.85	0.01	5.85	2.29	-156%
7/12/2023 10:00	20.85	0.01	5.87	2.28	-157%
7/12/2023 10:01	20.85	0.01	5.90	2.31	-156%
7/12/2023 10:02	20.85	0.01	5.91	2.30	-157%
7/12/2023 10:03	20.85	0.01	5.92	2.29	-159%
7/12/2023 10:04	20.84	0.01	5.94	2.28	-160%
7/12/2023 10:05	20.85	0.02	5.98	2.28	-162%
7/12/2023 10:06	20.85	0.02	5.99	2.28	-163%
7/12/2023 10:07	20.85	0.01	6.01	2.29	-162%
7/12/2023 10:08	20.85	0.01	6.03	2.31	-161%
7/12/2023 10:09	20.85	0.01	6.06	2.34	-159%
7/12/2023 10:10	20.85	0.01	6.08	2.37	-157%
7/12/2023 10:11	20.84	0.01	6.11	2.37	-158%
7/12/2023 10:12	20.85	0.01	6.12	2.39	-156%
7/12/2023 10:13	20.83	0.01	6.55	10.27	36%
7/12/2023 10:14	20.58	0.09	8.58	91.64	91%
7/12/2023 10:15	20.69	0.61	9.02	91.41	90%
7/12/2023 10:16	20.80	0.49	8.62	32.46	73%



Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 10:17	20.82	0.20	8.22	14.33	43%
7/12/2023 10:18	20.83	0.10	7.92	9.27	15%
7/12/2023 10:19	20.84	0.07	7.68	6.02	-28%
7/12/2023 10:20	20.83	0.05	7.50	4.54	-65%
7/12/2023 10:21	20.84	0.04	7.36	4.50	-63%
7/12/2023 10:22	20.84	0.04	7.22	4.76	-52%
7/12/2023 10:23	20.84	0.03	7.11	4.77	-49%
7/12/2023 10:24	20.84	0.03	7.03	4.44	-58%
7/12/2023 10:25	20.84	0.02	6.96	4.09	-70%
7/12/2023 10:26	20.84	0.02	6.89	2.94	-134%
7/12/2023 10:27	20.84	0.02	6.91	2.76	-151%
7/12/2023 10:28	20.84	0.02	6.94	2.79	-149%
7/12/2023 10:29	20.84	0.02	6.91	2.78	-149%
7/12/2023 10:30	20.84	0.02	6.86	2.70	-154%
7/12/2023 10:31	20.82	0.02	6.90	16.92	59%
7/12/2023 10:32	20.82	0.04	6.94	11.70	41%
7/12/2023 10:33	20.82	0.04	7.28	11.22	35%
7/12/2023 10:34	20.82	0.04	8.43	11.46	26%
7/12/2023 10:35	20.82	0.04	10.66	13.81	23%
7/12/2023 10:36	20.82	0.05	12.41	17.89	31%
7/12/2023 10:37	20.82	0.06	13.25	19.63	33%
7/12/2023 10:38	20.82	0.07	14.12	20.04	30%
7/12/2023 10:39	20.82	0.08	14.94	19.87	25%
7/12/2023 10:40	20.81	0.08	15.67	19.79	21%
7/12/2023 10:41	20.81	0.08	16.42	18.59	12%
7/12/2023 10:42	20.81	0.08	17.00	17.32	2%
7/12/2023 10:43	20.82	0.08	17.33	17.43	1%
7/12/2023 10:44	20.82	0.08	17.66	17.72	0%
7/12/2023 10:45	20.81	0.08	17.96	18.21	1%
7/12/2023 10:46	20.81	0.08	18.12	18.78	4%
7/12/2023 10:47	20.81	0.07	18.23	19.30	6%
7/12/2023 10:48	20.82	0.07	18.38	20.11	9%
7/12/2023 10:49	20.81	0.07	18.48	21.17	13%
7/12/2023 10:50	20.81	0.07	18.55	22.06	16%
7/12/2023 10:51	20.81	0.07	18.61	22.50	17%
7/12/2023 10:52	20.81	0.07	18.74	23.27	19%
7/12/2023 10:53	20.81	0.07	18.75	23.91	22%
7/12/2023 10:54	20.80	0.07	18.86	26.89	30%
7/12/2023 10:55	20.80	0.07	18.92	26.85	30%
7/12/2023 10:56	20.80	0.07	19.07	25.69	26%
7/12/2023 10:57	20.80	0.07	19.02	25.58	26%
7/12/2023 10:58	20.80	0.07	18.96	36.05	47%
7/12/2023 10:59	20.80	0.07	18.93	40.33	53%
7/12/2023 11:00	20.79	0.07	18.92	28.51	34%
7/12/2023 11:01	20.79	0.07	19.06	28.36	33%
7/12/2023 11:02	20.79	0.07	19.22	28.83	33%
7/12/2023 11:03	20.79	0.07	19.37	29.27	34%
7/12/2023 11:04	20.79	0.07	19.55	29.72	34%
7/12/2023 11:05	20.79	0.07	19.75	30.05	34%
7/12/2023 11:06	20.79	0.07	19.92	30.20	34%
7/12/2023 11:07	20.79	0.07	20.05	30.31	34%
7/12/2023 11:08	20.79	0.07	20.02	30.10	33%
7/12/2023 11:09	20.79	0.07	20.03	29.85	33%
7/12/2023 11:10	20.78	0.07	20.07	29.66	32%
7/12/2023 11:11	20.78	0.07	20.00	29.47	32%
7/12/2023 11:12	20.77	0.07	19.78	29.28	32%
7/12/2023 11:13	20.77	0.07	19.56	28.82	32%
7/12/2023 11:14	20.76	0.07	19.43	28.25	31%
<b>Run 1 Avg</b>	<b>20.83</b>	<b>0.04</b>	<b>9.13</b>	<b>11.50</b>	<b>21%</b>
7/12/2023 11:15	20.76	0.06	18.94	27.79	
7/12/2023 11:16	20.76	0.06	18.28	28.29	
7/12/2023 11:17	20.75	0.05	17.66	24.62	
7/12/2023 11:18	20.75	0.04	16.56	24.03	
7/12/2023 11:19	20.75	0.04	15.47	23.90	
7/12/2023 11:20	20.75	0.04	14.55	23.76	
7/12/2023 11:21	20.75	0.04	13.63	23.80	
7/12/2023 11:22	20.75	0.04	12.99	23.70	
7/12/2023 11:23	20.75	0.04	12.67	23.60	
7/12/2023 11:24	14.88	0.02	12.56	27.58	
7/12/2023 11:25	0.02	0.00	12.52	39.53	
7/12/2023 11:26	0.03	0.00	12.15	55.64	
7/12/2023 11:27	2.36	1.18	11.68	63.53	
7/12/2023 11:28	20.01	17.73	11.21	65.80	
7/12/2023 11:29	20.01	17.73	10.80	70.05	
7/12/2023 11:30	20.01	17.73	10.44	72.21	

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 11:31	11.45	10.41	10.14	75.52	
7/12/2023 11:32	11.00	8.95	9.91	89.98	
7/12/2023 11:33	11.00	8.95	9.72	97.52	
7/12/2023 11:34	18.49	2.10	9.55	97.52	
7/12/2023 11:35	20.77	0.02	9.40	97.52	
7/12/2023 11:36	20.77	0.02	9.25	49.26	
7/12/2023 11:37	20.77	0.01	9.11	18.67	
7/12/2023 11:38	20.77	0.02	9.16	20.44	
7/12/2023 11:39	20.64	0.01	7.83	20.11	
7/12/2023 11:40	20.54	0.00	5.68	11.87	
7/12/2023 11:41	20.54	0.00	3.39	0.71	
7/12/2023 11:42	20.54	0.00	2.74	0.79	
7/12/2023 11:43	20.60	0.00	2.61	0.91	
7/12/2023 11:44	20.77	0.00	1.07	0.82	
7/12/2023 11:45	20.78	0.01	0.00	0.74	
7/12/2023 11:46	20.78	0.01	-0.02	0.69	
7/12/2023 11:47	20.77	0.01	-0.01	0.67	
7/12/2023 11:48	20.77	0.01	25.38	0.67	
7/12/2023 11:49	20.77	0.01	34.97	0.65	
7/12/2023 11:50	20.78	0.01	35.10	0.13	
7/12/2023 11:51	20.78	0.01	34.98	-0.02	
7/12/2023 11:52	20.77	0.01	34.91	0.01	
7/12/2023 11:53	20.77	0.01	18.24	0.08	
7/12/2023 11:54	20.77	0.01	2.05	0.08	
7/12/2023 11:55	20.77	0.01	1.90	0.05	
7/12/2023 11:56	20.77	0.01	2.17	0.09	
7/12/2023 11:57	20.77	0.02	5.33	0.21	
7/12/2023 11:58	20.78	0.02	5.93	0.20	
7/12/2023 11:59	20.79	0.02	5.99	0.29	
7/12/2023 12:00	20.79	0.02	6.05	0.15	
7/12/2023 12:01	20.79	0.02	6.17	7.70	
7/12/2023 12:02	20.79	0.02	6.35	35.39	
7/12/2023 12:03	20.79	0.02	6.42	35.39	
7/12/2023 12:04	20.79	0.02	6.49	35.38	
7/12/2023 12:05	20.79	0.01	6.57	28.61	
7/12/2023 12:06	20.78	0.01	6.62	24.95	
7/12/2023 12:07	20.78	0.01	6.67	4.10	
7/12/2023 12:08	20.78	0.02	6.72	1.84	
7/12/2023 12:09	20.78	0.02	6.79	1.75	
7/12/2023 12:10	20.78	0.02	6.86	1.59	
7/12/2023 12:11	20.77	0.01	6.94	1.75	
Run 2 Start					
7/12/2023 12:12	20.76	0.02	7.07	5.03	-41%
7/12/2023 12:13	20.75	0.02	7.30	8.70	16%
7/12/2023 12:14	20.74	0.02	7.57	21.37	65%
7/12/2023 12:15	20.73	0.03	7.80	27.17	71%
7/12/2023 12:16	20.72	0.04	7.96	28.04	72%
7/12/2023 12:17	20.72	0.05	8.09	25.16	68%
7/12/2023 12:18	20.71	0.06	8.19	26.57	69%
7/12/2023 12:19	20.72	0.07	8.26	19.96	59%
7/12/2023 12:20	20.72	0.07	8.31	21.41	61%
7/12/2023 12:21	20.73	0.06	8.39	18.28	54%
7/12/2023 12:22	20.72	0.06	8.48	22.32	62%
7/12/2023 12:23	20.72	0.05	8.60	12.74	33%
7/12/2023 12:24	20.69	0.05	8.86	72.84	88%
7/12/2023 12:25	20.70	0.08	9.10	45.98	80%
7/12/2023 12:26	20.70	0.08	8.74	30.41	71%
7/12/2023 12:27	20.73	0.09	7.96	4.68	-70%
7/12/2023 12:28	20.73	0.06	7.55	2.38	-218%
7/12/2023 12:29	20.73	0.04	7.31	1.95	-275%
7/12/2023 12:30	20.73	0.03	7.16	1.73	-314%
7/12/2023 12:31	20.73	0.02	7.02	1.58	-343%
7/12/2023 12:32	20.73	0.02	6.92	1.49	-364%
7/12/2023 12:33	20.73	0.02	6.82	1.42	-380%
7/12/2023 12:34	20.72	0.02	6.76	1.37	-394%
7/12/2023 12:35	20.73	0.02	6.66	1.33	-401%
7/12/2023 12:36	20.72	0.02	6.63	1.31	-406%
7/12/2023 12:37	20.73	0.02	6.58	1.29	-412%
7/12/2023 12:38	20.73	0.01	6.54	1.25	-422%
7/12/2023 12:39	20.73	0.01	6.49	1.23	-429%
7/12/2023 12:40	20.72	0.02	6.47	1.20	-439%
7/12/2023 12:41	20.73	0.01	6.43	1.19	-440%
7/12/2023 12:42	20.73	0.02	6.40	1.21	-430%
7/12/2023 12:43	20.72	0.01	6.37	1.20	-430%
7/12/2023 12:44	20.73	0.01	6.36	1.23	-419%
7/12/2023 12:45	20.73	0.02	6.31	1.23	-415%

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 12:46	20.72	0.02	6.31	1.24	-409%
7/12/2023 12:47	20.72	0.01	6.33	1.25	-405%
7/12/2023 12:48	20.73	0.02	6.34	1.29	-392%
7/12/2023 12:49	20.72	0.02	6.34	1.32	-381%
7/12/2023 12:50	20.72	0.02	6.36	1.34	-373%
7/12/2023 12:51	20.72	0.01	6.38	1.30	-391%
7/12/2023 12:52	20.72	0.02	6.40	1.36	-372%
7/12/2023 12:53	20.72	0.02	6.41	1.39	-361%
7/12/2023 12:54	20.72	0.02	6.44	1.43	-352%
7/12/2023 12:55	20.72	0.02	6.49	1.53	-325%
7/12/2023 12:56	20.72	0.02	6.54	1.56	-319%
7/12/2023 12:57	20.72	0.02	6.57	1.52	-333%
7/12/2023 12:58	20.73	0.02	6.55	1.48	-342%
7/12/2023 12:59	20.72	0.02	6.55	1.48	-341%
7/12/2023 13:00	20.72	0.02	6.55	1.47	-344%
7/12/2023 13:01	20.72	0.02	6.55	1.49	-340%
7/12/2023 13:02	20.72	0.02	6.53	1.49	-339%
7/12/2023 13:03	20.72	0.02	6.50	1.51	-330%
7/12/2023 13:04	20.72	0.02	6.49	1.51	-330%
7/12/2023 13:05	20.72	0.02	6.48	1.52	-325%
7/12/2023 13:06	20.72	0.02	6.45	1.53	-321%
7/12/2023 13:07	20.72	0.02	6.42	1.54	-318%
7/12/2023 13:08	20.72	0.02	6.41	1.56	-311%
7/12/2023 13:09	20.72	0.02	6.39	1.56	-310%
7/12/2023 13:10	20.72	0.02	6.35	1.54	-313%
7/12/2023 13:11	20.72	0.02	6.32	1.55	-307%
7/12/2023 13:12	20.72	0.01	6.33	1.56	-307%
7/12/2023 13:13	20.72	0.01	6.34	1.55	-310%
7/12/2023 13:14	20.72	0.02	6.34	1.54	-310%
7/12/2023 13:15	20.71	0.02	6.34	1.55	-310%
7/12/2023 13:16	20.72	0.02	6.31	1.55	-307%
7/12/2023 13:17	20.72	0.02	6.31	1.57	-302%
7/12/2023 13:18	20.73	0.02	6.31	1.62	-291%
7/12/2023 13:19	20.72	0.02	6.31	1.65	-283%
7/12/2023 13:20	20.72	0.02	6.28	1.64	-283%
7/12/2023 13:21	20.72	0.02	6.26	1.64	-282%
7/12/2023 13:22	20.72	0.02	6.25	1.68	-272%
7/12/2023 13:23	20.72	0.02	6.25	1.67	-275%
7/12/2023 13:24	20.72	0.02	6.25	1.67	-274%
7/12/2023 13:25	20.72	0.02	6.25	1.71	-266%
7/12/2023 13:26	20.72	0.02	6.23	1.72	-263%
7/12/2023 13:27	20.72	0.02	6.22	1.74	-257%
7/12/2023 13:28	20.73	0.02	6.25	1.72	-263%
7/12/2023 13:29	20.73	0.02	6.23	1.76	-254%
7/12/2023 13:30	20.73	0.02	6.22	1.79	-248%
7/12/2023 13:31	20.73	0.02	6.22	1.81	-243%
7/12/2023 13:32	20.73	0.01	6.22	1.84	-239%
7/12/2023 13:33	20.74	0.02	6.24	1.87	-233%
7/12/2023 13:34	20.74	0.02	6.25	1.85	-239%
7/12/2023 13:35	20.74	0.02	6.25	1.94	-222%
7/12/2023 13:36	20.73	0.02	6.78	29.43	77%
7/12/2023 13:37	20.49	0.10	8.45	95.44	91%
7/12/2023 13:38	20.61	0.60	8.55	75.27	89%
7/12/2023 13:39	20.71	0.45	8.27	18.79	56%
7/12/2023 13:40	20.74	0.17	8.06	9.84	18%
7/12/2023 13:41	20.75	0.10	7.88	5.76	-37%
7/12/2023 13:42	20.75	0.07	7.70	2.98	-158%
7/12/2023 13:43	20.76	0.05	7.57	2.01	-277%
7/12/2023 13:44	20.76	0.04	7.47	2.22	-236%
7/12/2023 13:45	20.76	0.04	7.37	2.90	-154%
7/12/2023 13:46	20.76	0.03	7.30	3.16	-131%
7/12/2023 13:47	20.75	0.03	7.24	3.37	-115%
7/12/2023 13:48	20.76	0.03	7.18	2.77	-160%
7/12/2023 13:49	20.75	0.02	7.15	1.79	-299%
7/12/2023 13:50	20.75	0.02	7.31	1.81	-305%
7/12/2023 13:51	20.75	0.02	7.56	18.75	60%
7/12/2023 13:52	20.74	0.03	7.56	37.99	80%
7/12/2023 13:53	20.74	0.04	7.60	37.60	80%
7/12/2023 13:54	20.74	0.04	8.29	38.25	78%
7/12/2023 13:55	20.74	0.05	10.83	42.82	75%
7/12/2023 13:56	20.74	0.05	13.38	48.04	72%
7/12/2023 13:57	20.74	0.06	14.89	49.66	70%
7/12/2023 13:58	20.74	0.07	16.02	50.47	68%
7/12/2023 13:59	20.74	0.07	17.04	51.57	67%
7/12/2023 14:00	20.74	0.07	17.85	52.04	66%
7/12/2023 14:01	20.74	0.07	18.41	51.71	64%

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 14:02	20.74	0.07	18.75	48.46	61%
7/12/2023 14:03	20.74	0.07	19.06	47.33	60%
7/12/2023 14:04	20.74	0.07	19.33	47.87	60%
7/12/2023 14:05	20.74	0.07	19.53	48.25	60%
7/12/2023 14:06	20.74	0.07	19.87	48.29	59%
7/12/2023 14:07	20.74	0.07	19.98	49.11	59%
7/12/2023 14:08	20.73	0.07	20.11	50.65	60%
7/12/2023 14:09	20.73	0.07	20.14	51.43	61%
7/12/2023 14:10	20.73	0.07	20.08	52.72	62%
7/12/2023 14:11	20.73	0.07	20.28	53.94	62%
7/12/2023 14:12	20.72	0.06	20.28	56.76	64%
7/12/2023 14:13	20.72	0.06	20.35	57.45	65%
7/12/2023 14:14	20.72	0.06	20.40	58.32	65%
7/12/2023 14:15	20.72	0.07	20.43	57.42	64%
7/12/2023 14:16	20.72	0.07	20.48	60.31	66%
7/12/2023 14:17	20.71	0.07	20.48	60.49	66%
7/12/2023 14:18	20.71	0.07	20.48	60.87	66%
7/12/2023 14:19	20.71	0.06	20.36	61.10	67%
7/12/2023 14:20	20.71	0.06	20.44	62.80	67%
7/12/2023 14:21	20.71	0.06	20.75	82.55	75%
7/12/2023 14:22	20.70	0.07	20.79	69.29	70%
7/12/2023 14:23	20.70	0.07	20.67	61.67	66%
7/12/2023 14:24	20.70	0.07	20.77	60.02	65%
7/12/2023 14:25	20.71	0.06	20.85	57.02	63%
7/12/2023 14:26	20.70	0.06	20.84	54.44	62%
7/12/2023 14:27	20.70	0.06	20.73	52.65	61%
7/12/2023 14:28	20.70	0.06	20.65	44.93	54%
7/12/2023 14:29	20.70	0.06	20.34	36.04	44%
7/12/2023 14:30	20.70	0.06	19.84	32.74	39%
7/12/2023 14:31	20.70	0.06	19.17	28.95	34%
<b>Run 2 Avg</b>	<b>20.72</b>	<b>0.05</b>	<b>10.21</b>	<b>20.32</b>	<b>50%</b>
7/12/2023 14:32	20.69	0.06	18.55	24.49	
7/12/2023 14:33	20.69	0.06	18.03	20.67	
7/12/2023 14:34	20.69	0.06	17.41	18.53	
7/12/2023 14:35	20.69	0.06	16.74	10.23	
7/12/2023 14:36	20.69	0.05	15.91	6.44	
7/12/2023 14:37	20.69	0.04	14.97	5.16	
7/12/2023 14:38	20.68	0.04	14.13	4.34	
7/12/2023 14:39	14.49	0.03	13.39	3.89	
7/12/2023 14:40	0.03	0.02	12.68	2.63	
7/12/2023 14:41	0.03	0.02	12.21	2.10	
7/12/2023 14:42	0.03	0.02	11.91	1.99	
7/12/2023 14:43	13.35	10.48	11.58	1.91	
7/12/2023 14:44	20.01	17.94	11.24	1.86	
7/12/2023 14:45	20.01	17.94	10.93	1.83	
7/12/2023 14:46	20.01	17.94	10.58	1.81	
7/12/2023 14:47	20.01	17.94	10.24	1.79	
7/12/2023 14:48	18.02	17.19	9.96	0.58	
7/12/2023 14:49	10.95	8.95	9.69	0.01	
7/12/2023 14:50	10.95	8.95	9.49	3.63	
7/12/2023 14:51	17.43	3.00	9.29	35.05	
7/12/2023 14:52	20.67	0.02	9.15	35.37	
7/12/2023 14:53	20.67	0.02	9.03	35.36	
7/12/2023 14:54	20.67	0.02	9.27	30.34	
7/12/2023 14:55	20.44	0.01	7.02	3.50	
7/12/2023 14:56	20.44	0.00	4.01	2.26	
7/12/2023 14:57	20.45	0.00	2.85	1.95	
7/12/2023 14:58	20.44	0.00	2.44	1.82	
7/12/2023 14:59	20.45	0.00	2.28	1.74	
7/12/2023 15:00	20.44	0.00	2.21	1.68	
7/12/2023 15:01	20.45	0.00	2.17	1.63	
7/12/2023 15:02	20.44	0.00	0.57	1.60	
7/12/2023 15:03	20.44	0.00	-0.02	1.57	
7/12/2023 15:04	20.44	0.00	-0.02	1.57	
7/12/2023 15:05	19.96	0.00	22.70	1.58	
7/12/2023 15:06	18.83	0.00	35.60	1.54	
7/12/2023 15:07	18.82	0.00	34.94	1.51	
7/12/2023 15:08	18.82	0.00	34.97	1.49	
7/12/2023 15:09	18.83	0.00	35.02	1.48	
7/12/2023 15:10	19.84	0.00	13.74	1.45	
7/12/2023 15:11	20.29	0.00	8.76	1.43	
7/12/2023 15:12	20.61	0.01	5.59	1.42	
7/12/2023 15:13	20.63	0.00	5.49	1.41	
7/12/2023 15:14	20.65	0.00	5.99	1.41	
7/12/2023 15:15	20.68	0.01	6.08	1.40	

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 15:16	20.68	0.02	6.10	1.40	
7/12/2023 15:17	20.69	0.02	6.08	1.38	
7/12/2023 15:18	20.70	0.02	6.08	1.39	
7/12/2023 15:19	20.71	0.02	6.08	1.33	
7/12/2023 15:20	20.71	0.02	6.06	1.32	
7/12/2023 15:21	20.72	0.02	6.06	1.33	
7/12/2023 15:22	20.72	0.02	6.05	1.34	
7/12/2023 15:23	20.72	0.02	6.04	1.33	
7/12/2023 15:24	20.73	0.02	6.05	1.37	
7/12/2023 15:25	20.73	0.02	6.02	1.38	
7/12/2023 15:26	20.73	0.02	6.04	1.42	
7/12/2023 15:27	20.74	0.02	6.05	1.47	
7/12/2023 15:28	20.74	0.02	6.04	1.54	
Run 3 Start					
7/12/2023 15:29	20.74	0.02	6.05	1.47	-313%
7/12/2023 15:30	20.74	0.02	6.04	1.34	-350%
7/12/2023 15:31	20.74	0.02	6.02	1.30	-364%
7/12/2023 15:32	20.74	0.02	6.04	2.85	-112%
7/12/2023 15:33	20.74	0.02	6.10	8.85	31%
7/12/2023 15:34	20.74	0.02	6.20	13.96	56%
7/12/2023 15:35	20.73	0.03	6.32	20.35	69%
7/12/2023 15:36	20.73	0.04	6.35	15.80	60%
7/12/2023 15:37	20.73	0.05	6.34	18.61	66%
7/12/2023 15:38	20.73	0.06	6.32	19.34	67%
7/12/2023 15:39	20.72	0.06	6.30	34.22	82%
7/12/2023 15:40	20.73	0.08	6.24	22.55	72%
7/12/2023 15:41	20.74	0.07	6.21	21.10	71%
7/12/2023 15:42	20.74	0.06	6.16	22.39	72%
7/12/2023 15:43	20.74	0.06	6.17	22.60	73%
7/12/2023 15:44	20.74	0.06	6.14	23.11	73%
7/12/2023 15:45	20.74	0.06	6.09	25.32	76%
7/12/2023 15:46	20.73	0.06	6.29	34.46	82%
7/12/2023 15:47	20.73	0.06	6.43	67.49	90%
7/12/2023 15:48	20.72	0.09	6.77	48.71	86%
7/12/2023 15:49	20.72	0.09	6.42	23.22	72%
7/12/2023 15:50	20.75	0.09	6.19	3.38	-83%
7/12/2023 15:51	20.76	0.06	6.10	2.50	-144%
7/12/2023 15:52	20.76	0.04	6.00	2.14	-180%
7/12/2023 15:53	20.76	0.03	5.91	2.08	-185%
7/12/2023 15:54	20.76	0.02	5.82	1.78	-228%
7/12/2023 15:55	20.76	0.02	5.77	1.89	-206%
7/12/2023 15:56	20.76	0.02	5.73	1.74	-230%
7/12/2023 15:57	20.77	0.02	5.72	1.74	-228%
7/12/2023 15:58	20.77	0.02	5.72	1.73	-230%
7/12/2023 15:59	20.77	0.02	5.71	1.66	-245%
7/12/2023 16:00	20.77	0.02	5.69	1.62	-250%
7/12/2023 16:01	20.77	0.02	5.69	1.61	-253%
7/12/2023 16:02	20.78	0.02	5.69	1.62	-252%
7/12/2023 16:03	20.78	0.02	5.69	1.49	-282%
7/12/2023 16:04	20.78	0.02	5.67	1.57	-262%
7/12/2023 16:05	20.78	0.02	5.65	1.58	-258%
7/12/2023 16:06	20.78	0.02	5.65	1.59	-255%
7/12/2023 16:07	20.78	0.02	5.63	1.59	-255%
7/12/2023 16:08	20.79	0.02	5.60	1.50	-274%
7/12/2023 16:09	20.79	0.02	5.58	1.56	-258%
7/12/2023 16:10	20.79	0.02	5.56	1.63	-241%
7/12/2023 16:11	20.79	0.02	5.55	1.67	-233%
7/12/2023 16:12	20.79	0.02	5.55	1.63	-241%
7/12/2023 16:13	20.79	0.02	5.54	1.61	-244%
7/12/2023 16:14	20.79	0.02	5.54	1.65	-236%
7/12/2023 16:15	20.79	0.02	5.52	1.61	-242%
7/12/2023 16:16	20.79	0.02	5.51	1.48	-273%
7/12/2023 16:17	20.79	0.02	5.51	1.59	-246%
7/12/2023 16:18	20.79	0.02	5.49	1.52	-262%
7/12/2023 16:19	20.79	0.02	5.51	1.65	-234%
7/12/2023 16:20	20.79	0.02	5.53	1.67	-231%
7/12/2023 16:21	20.79	0.02	5.54	1.63	-241%
7/12/2023 16:22	20.79	0.02	5.58	1.74	-221%
7/12/2023 16:23	20.79	0.02	5.63	1.76	-220%
7/12/2023 16:24	20.79	0.02	5.68	1.94	-193%
7/12/2023 16:25	20.79	0.02	5.72	1.87	-206%
7/12/2023 16:26	20.78	0.02	5.76	1.84	-214%
7/12/2023 16:27	20.79	0.02	5.80	1.84	-215%
7/12/2023 16:28	20.79	0.02	5.81	1.85	-214%
7/12/2023 16:29	20.79	0.02	5.81	1.77	-228%
7/12/2023 16:30	20.79	0.02	5.80	1.81	-221%

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 16:31	20.79	0.02	5.83	1.77	-229%
7/12/2023 16:32	20.78	0.02	5.86	1.98	-197%
7/12/2023 16:33	20.78	0.02	5.87	1.96	-200%
7/12/2023 16:34	20.79	0.02	5.86	1.90	-208%
7/12/2023 16:35	20.79	0.02	5.83	1.90	-207%
7/12/2023 16:36	20.79	0.02	5.81	1.84	-215%
7/12/2023 16:37	20.79	0.02	5.80	1.86	-211%
7/12/2023 16:38	20.78	0.02	5.77	1.82	-217%
7/12/2023 16:39	20.79	0.02	5.76	1.82	-216%
7/12/2023 16:40	20.78	0.02	5.76	1.85	-212%
7/12/2023 16:41	20.78	0.02	5.78	1.87	-209%
7/12/2023 16:42	20.78	0.02	5.79	1.91	-204%
7/12/2023 16:43	20.78	0.02	5.83	1.88	-209%
7/12/2023 16:44	20.78	0.02	5.87	1.90	-210%
7/12/2023 16:45	20.78	0.02	5.90	1.90	-210%
7/12/2023 16:46	20.77	0.02	5.88	1.94	-204%
7/12/2023 16:47	20.77	0.02	5.87	1.96	-200%
7/12/2023 16:48	20.77	0.02	5.85	1.84	-218%
7/12/2023 16:49	20.77	0.02	5.85	1.97	-197%
7/12/2023 16:50	20.77	0.02	5.85	1.93	-203%
7/12/2023 16:51	20.77	0.02	5.85	1.96	-199%
7/12/2023 16:52	20.77	0.02	5.88	2.05	-187%
7/12/2023 16:53	20.77	0.02	5.91	2.04	-189%
7/12/2023 16:54	20.77	0.02	5.93	2.14	-178%
7/12/2023 16:55	20.77	0.02	5.92	2.13	-178%
7/12/2023 16:56	20.77	0.02	5.92	2.15	-175%
7/12/2023 16:57	20.77	0.02	5.93	2.14	-176%
7/12/2023 16:58	20.77	0.02	5.94	2.12	-180%
7/12/2023 16:59	20.75	0.02	6.37	28.55	78%
7/12/2023 17:00	20.51	0.09	7.97	92.62	91%
7/12/2023 17:01	20.62	0.63	8.05	77.37	90%
7/12/2023 17:02	20.71	0.50	7.88	25.33	69%
7/12/2023 17:03	20.74	0.21	7.71	11.70	34%
7/12/2023 17:04	20.75	0.11	7.57	6.75	-12%
7/12/2023 17:05	20.76	0.07	7.43	3.26	-128%
7/12/2023 17:06	20.76	0.06	7.32	2.42	-202%
7/12/2023 17:07	20.76	0.04	7.20	2.22	-225%
7/12/2023 17:08	20.76	0.04	7.08	3.35	-111%
7/12/2023 17:09	20.76	0.04	6.99	3.46	-102%
7/12/2023 17:10	20.76	0.03	6.92	3.60	-92%
7/12/2023 17:11	20.76	0.02	6.86	2.98	-130%
7/12/2023 17:12	20.77	0.02	6.79	1.86	-264%
7/12/2023 17:13	20.76	0.02	6.73	1.63	-314%
7/12/2023 17:14	20.76	0.02	7.00	10.66	34%
7/12/2023 17:15	20.76	0.03	6.91	16.21	57%
7/12/2023 17:16	20.76	0.04	6.76	25.13	73%
7/12/2023 17:17	20.75	0.04	6.75	21.50	69%
7/12/2023 17:18	20.75	0.04	7.04	26.67	74%
7/12/2023 17:19	20.74	0.04	8.44	34.45	75%
7/12/2023 17:20	20.75	0.04	9.90	36.44	73%
7/12/2023 17:21	20.74	0.05	11.05	44.02	75%
7/12/2023 17:22	20.74	0.05	12.13	46.95	74%
7/12/2023 17:23	20.73	0.06	13.37	47.79	72%
7/12/2023 17:24	20.72	0.07	14.56	47.18	69%
7/12/2023 17:25	20.71	0.07	15.35	46.39	67%
7/12/2023 17:26	20.71	0.07	15.95	46.82	66%
7/12/2023 17:27	20.70	0.07	16.35	46.11	65%
7/12/2023 17:28	20.69	0.07	16.51	40.80	60%
7/12/2023 17:29	20.69	0.07	16.60	40.16	59%
7/12/2023 17:30	20.68	0.07	16.68	40.75	59%
7/12/2023 17:31	20.67	0.07	16.80	42.34	60%
7/12/2023 17:32	20.67	0.06	16.97	43.06	61%
7/12/2023 17:33	20.66	0.06	17.17	42.57	60%
7/12/2023 17:34	20.66	0.06	17.43	44.61	61%
7/12/2023 17:35	20.66	0.06	17.56	44.58	61%
7/12/2023 17:36	20.66	0.06	17.57	43.96	60%
7/12/2023 17:37	20.66	0.06	17.73	44.81	60%
7/12/2023 17:38	20.65	0.06	17.75	45.45	61%
7/12/2023 17:39	20.65	0.06	17.59	45.29	61%
7/12/2023 17:40	20.65	0.06	17.51	47.43	63%
7/12/2023 17:41	20.65	0.06	17.66	47.20	63%
7/12/2023 17:42	20.65	0.06	17.67	46.68	62%
7/12/2023 17:43	20.65	0.06	17.63	47.56	63%
7/12/2023 17:44	20.64	0.06	17.65	56.79	69%
7/12/2023 17:45	20.64	0.06	17.77	70.27	75%
7/12/2023 17:46	20.65	0.07	17.79	48.17	63%

Carbon Bed I/O Time	O2 %	CO2 %	VOC Out ppm	VOC In ppm	Destruction Eff. %
7/12/2023 17:47	20.65	0.06	17.83	47.38	62%
7/12/2023 17:48	20.65	0.06	17.87	46.33	61%
7/12/2023 17:49	20.65	0.06	17.88	44.37	60%
7/12/2023 17:50	20.65	0.06	17.84	41.74	57%
7/12/2023 17:51	20.65	0.06	17.78	38.67	54%
7/12/2023 17:52	20.65	0.06	17.67	37.18	52%
7/12/2023 17:53	20.65	0.06	17.52	34.81	50%
7/12/2023 17:54	20.65	0.06	17.32	31.43	45%
7/12/2023 17:55	20.65	0.06	17.05	26.11	35%
7/12/2023 17:56	20.65	0.05	16.78	20.02	16%
7/12/2023 17:57	20.65	0.05	16.28	16.98	4%
7/12/2023 17:58	20.66	0.05	15.47	12.16	-27%
7/12/2023 17:59	20.65	0.05	14.85	10.03	-48%
7/12/2023 18:00	20.65	0.05	13.82	11.43	-21%
<b>Run 3 Avg</b>	<b>20.74</b>	<b>0.05</b>	<b>8.91</b>	<b>17.37</b>	<b>49%</b>
7/12/2023 18:01	20.65	0.04	12.86	16.27	
7/12/2023 18:02	20.64	0.04	14.65	29.63	
7/12/2023 18:03	20.35	0.04	8.48	30.97	
7/12/2023 18:04	20.44	0.01	3.24	11.08	
7/12/2023 18:05	20.45	0.00	1.02	6.58	
7/12/2023 18:06	20.45	0.00	0.63	5.37	
7/12/2023 18:07	18.07	0.00	0.51	3.38	
7/12/2023 18:08	0.03	0.02	0.45	2.80	
7/12/2023 18:09	0.03	0.02	0.41	2.63	
7/12/2023 18:10	3.50	3.47	0.39	2.43	
7/12/2023 18:11	18.83	12.19	0.37	1.70	
7/12/2023 18:12	20.01	18.24	0.36	1.48	
7/12/2023 18:13	20.01	18.24	0.03	1.35	
7/12/2023 18:14	17.01	16.56	-0.01	1.26	
7/12/2023 18:15	11.00	8.98	0.00	1.25	
7/12/2023 18:16	11.00	9.00	11.99	1.21	
7/12/2023 18:17	11.00	9.00	34.49	1.12	
7/12/2023 18:18	11.00	9.00	35.01	1.07	
7/12/2023 18:19	15.06	4.35	35.01	1.11	
7/12/2023 18:20	18.86	0.00	34.96	1.07	
7/12/2023 18:21	18.86	0.00	34.72	1.12	
7/12/2023 18:22	19.99	0.00	5.65	3.80	
7/12/2023 18:23	20.65	0.01	7.06	0.79	
7/12/2023 18:24	20.68	0.02	6.36	0.20	
7/12/2023 18:25	20.69	0.02	6.18	-0.01	
7/12/2023 18:26	20.70	0.02	6.09	-0.04	
7/12/2023 18:27	20.71	0.02	6.00	-0.04	
7/12/2023 18:28	20.72	0.02	2.56	30.38	
7/12/2023 18:29	20.74	0.02	1.21	35.12	
7/12/2023 18:30	20.76	0.02	1.51	35.32	
7/12/2023 18:31	20.76	0.02	3.34	35.30	
7/12/2023 18:32	20.78	0.02	1.82	29.87	
7/12/2023 18:33	20.80	0.02	1.35	1.11	
7/12/2023 18:34	20.81	0.02	1.39	1.07	

Carbon Bed I/O  
 Calibration Error Test at Run 1  
 Operator: Dan Kirk

Date	7/12/2023					O2	CO2	VOC Out	VOC In
Analyte	O2	CO2	VOC Out	VOC In		O2	CO2	VOC Out	VOC In
Units	%	%	ppm	ppm					
Zero Ref Cyl	0.0	0.0	0.0	0.0					
Zero Avg	-0.003	0.002	0.048	-0.035	Times	6:37	6:37	6:57	7:16
Zero Error%	0.0%	0.01%	0.1%	0.0%					
Zero CALERR PASS?	PASS	PASS	PASS	PASS					
Mid Ref Cyl	10.96	8.91	50.00	50.00					
Mid Avg	11.00	9.00	50.02	50.02	Times	6:41	6:41	7:05	7:28
Mid Error%	0.2%	0.5%	0.02%	0.02%					
Mid CALERR PASS?	PASS	PASS	PASS	PASS					
High Ref Cyl	20.00	17.92	95.00	95.00					
High Avg	20.01	17.99	95.01	95.05	Times	6:33	6:33	7:01	7:22
High Error%	0.1%	0.4%	0.0%	0.1%					
High CALERR PASS?	PASS	PASS	PASS	PASS					
Low Ref Cyl			35.00	35.00					
Low Avg			34.96	35.23				7:09	7:32



Carbon Bed I/O  
 Initial System Bias Check for Run 1  
 Operator:

Dan Kirk

Date	7/12/2023					O2	CO2	VOC Out	VOC In
Analyte	O2	CO2	VOC Out	VOC In					
Units	%	%	ppm	ppm					
Zero Ref Cyl	0	0	0	0					
Zero Cal	-0.003	0.002	0.048	-0.035					
Zero Avg	0.023	0.020	0.048	-0.035	Times	6:46	6:46	6:57	7:16
Zero Bias%	0.13%	0.10%	0.00%	0.00%					
Zero IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Span Ref Cyl	20.00	8.91	35.00	35.00					
Span Cal	20.01	9.00	34.96	35.23					
Span Avg	20.08	8.90	34.96	35.23	Times	7:37	6:52	7:09	7:32
Span Bias%	0.35%	-0.55%	0.00%	0.00%					
Span IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					

Carbon Bed I/O  
 Final System Bias Check for Run 1  
 Operator:

Dan Kirk

Date	7/12/2023								
Analyte	O2	CO2	VOC Out	VOC In		O2	CO2	VOC Out	VOC In
Units	%	%	ppm	ppm					
Zero Ref Cyl	0.00	0.00	0.00	0.00					
Zero Cal	0.00	0.00	0.05	-0.03					
Zero Avg	0.03	0.00	-0.02	0.20	Times	11:26	11:26	11:46	11:58
Zero Bias%	0.14%	0.01%	-0.07%	0.25%					
Zero IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Zero Drift%	0.01%	0.10%	0.07%	0.25%					
Zero Drift (≤ 3%)?	PASS	PASS	PASS	PASS					
Span Ref Cyl	20.00	8.91	35.00	35.00					
Span Cal	20.01	9.00	34.96	35.23					
Span Avg	20.01	8.95	35.10	35.38	Times	11:29	11:33	11:50	12:04
Span Bias%	0.00%	-0.26%	0.15%	0.16%					
Span IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Span Drift%	0.35%	0.30%	0.15%	0.16%					
Span Drift (≤ 3%)?	PASS	PASS	PASS	PASS					
	Run 1								
Ini Zero Avg	0.02	0.02	0.05	-0.03					
Ini Span Avg	20.08	8.90	34.96	35.23					
Run Avg	20.83	0.04	9.13	11.50					
Co	0.02	0.01							
Cm	20.05	8.92							
Correct Avg	20.79	0.03							

Carbon Bed I/O  
 Final System Bias Check for Run 2  
 Operator:

Dan Kirk

Date	7/12/2023								
Analyte	O2	CO2	VOC Out	VOC In		O2	CO2	VOC Out	VOC In
Units	%	%	ppm	ppm					
Zero Ref Cyl	0.00	0.00	0.00	0.00					
Zero Cal	-0.003	0.002	0.048	-0.035					
Zero Avg	0.034	0.024	-0.016	0.006	Times	14:41	14:41	15:04	14:49
Zero Bias%	0.18%	0.12%	-0.07%	0.04%					
Zero IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Zero Drift%	0.04%	0.12%	0.00%	0.21%					
Zero Drift (≤ 3%)?	PASS	PASS	PASS	PASS					
Span Ref Cyl	20.00	8.91	35.00	35.00					
Span Cal	20.01	9.00	34.96	35.23					
Span Avg	20.01	8.95	34.97	35.36	Times	14:45	14:50	15:08	14:53
Span Bias%	0.00%	-0.25%	0.01%	0.14%					
Span IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Span Drift%	0.00%	0.01%	0.14%	0.02%					
Span Drift (≤ 3%)?	PASS	PASS	PASS	PASS					
	Run 2								
Ini Zero Avg	0.03	0.00	-0.02	0.20					
Ini Span Avg	20.01	8.95	35.10	35.38					
Run Avg	20.72	0.05	10.21	20.32					
Co	0.03	0.01							
Cm	20.01	8.95							
Correct Avg	20.71	0.03							

Carbon Bed I/O  
Final System Bias Check for Run 3

Operator: Dan Kirk

Date	7/12/2023								
Analyte	O2	CO2	VOC Out	VOC In		O2	CO2	VOC Out	VOC In
Units	%	%	ppm	ppm					
Zero Ref Cyl	0	0	0	0					
Zero Cal	0.00	0.00	0.05	-0.03					
Zero Avg	0.03	0.02	0.00	-0.04	Times	18:09	18:09	18:15	18:26
Zero Bias%	0.18%	0.12%	-0.05%	0.00%					
Zero IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Zero Drift%	0.00%	0.01%	0.01%	0.04%					
Zero Drift (≤ 3%)?	PASS	PASS	PASS	PASS					
Span Ref Cyl	20.00	8.91	35.00	35.00					
Span Cal	20.01	9.00	34.96	35.23					
Span Avg	20.01	9.00	34.96	35.3	Times	18:13	18:17	18:20	18:31
Span Bias%	0.00%	0.01%	0.00%	0.07%					
Span IBIAS (≤ 5%)?	PASS	PASS	PASS	PASS					
Span Drift%	0.00%	0.26%	0.01%	0.06%					
Span Drift (≤ 3%)?	PASS	PASS	PASS	PASS					
	Run 3								
Ini Zero Avg	0.03	0.02	-0.02	0.01					
Ini Span Avg	20.01	8.95	34.97	35.36					
Run Avg	20.74	0.05	8.91	16.97					
Co	0.03	0.02							
Cm	20.01	8.97							
Correct Avg	20.73	0.02							

# Advanced Industrial Resources, Inc.

## Field Data Sheet

**Client:** GP Toledo AMRS  
**Location:** Toledo, OR  
**Source:** Carbon Bed Outlet  
**Test Team:** JS, DK, DW  
**EPA Methods:** 1, 2, 3, 4  
**D<sub>s</sub> (in.):** 39.0  
**% O<sub>2</sub>** 20.79  
**% CO<sub>2</sub>** 0.03  
**Start Run:** 8:45 AM  
**End Run:** 11:45 AM  
**Run Number:** 1 Filter ID \_\_\_\_\_

**Test Date:** July 12, 2023  
**Console ID:** C-009  
**Y<sub>m</sub> / ΔH<sub>@</sub>:** 1.013 1.554  
**Sampling Box ID:** B-1  
**Probe Assembly ID:** OR-P8-01  
**D<sub>n</sub> (in.):** 0.200 **D<sub>n</sub> ID:** OR-GN-200  
**Cp:** 0.84  
**P<sub>bar</sub> (in. Hg):** 30.12  
**p<sub>g</sub> (in. H<sub>2</sub>O):** 0.30  
**Minutes/Point:** 7.5  
**K-Factor:** 1.5

Point	Meter (dcf)	Inches H <sub>2</sub> O			Temperature Readings (°F)						Vacuum (in. Hg)
		Δp	ΔH	(Δp) <sup>1/2</sup>	t <sub>s</sub>	Probe	Filter	Last Impinger	t <sub>m</sub> Average	Filter CPM	
1	934.551	0.89	1.34	0.943	71	260	257	58	63	254	1
2	936.46	1.00	1.50	1.000	72	257	259	55	63	255	1
3	944.54	1.00	1.50	1.000	72	258	258	53	63	254	1
4	949.65	1.00	1.50	1.000	71	254	258	52	62	254	1
5	954.71	1.00	1.50	1.000	71	259	256	52	63	251	1
6	959.89	1.10	1.65	1.049	71	260	258	52	63	254	1
7	964.95	1.20	1.80	1.095	71	262	257	52	63	253	1
8	971.08	1.20	1.80	1.095	71	262	257	53	63	252	1
9	977.20	1.10	1.65	1.049	72	257	257	53	64	252	1
10	983.32	1.00	1.50	1.000	72	259	260	53	64	257	1
11	989.37	1.00	1.50	1.000	72	259	258	54	64	253	1
12	995.63	1.00	1.50	1.000	72	257	256	54	64	251	1
13	1001.59	0.84	1.26	0.917	74	258	258	55	65	255	1
14	1007.66	1.00	1.50	1.000	73	259	258	55	66	254	1
15	1013.10	0.99	1.49	0.995	73	261	256	56	67	252	1
16	1018.26	1.00	1.50	1.000	83	257	259	56	67	256	1
17	1024.22	1.10	1.65	1.049	93	260	256	57	67	251	1
18	1029.89	1.10	1.65	1.049	96	260	256	57	68	250	1
19	1034.98	1.10	1.65	1.049	97	259	254	57	68	250	1
20	1040.42	1.20	1.80	1.095	98	260	257	58	67	253	1
End	1042.976										

**Total moisture collected (g):** 25.4  
**Theoretical maximum moisture collection at saturation (g):** 76.6  
**Pre System Leak Check (cfm):** 0.000 @ 16"  
**Post System Leak Check (cfm):** 0.000 @ 16"

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
Pre-test:	850.5	811.5	822.3		980.7	3465.0 g
Post-test:	853.8	815.5	827.8		993.3	3490.4 g
Net gain:	3.3	4	5.5	0	12.6	25.4 g

# Advanced Industrial Resources, Inc.

## Field Data Sheet

**Client:** GP Toledo AMRS  
**Location:** Toledo, OR  
**Source:** Carbon Bed Outlet  
**Test Team:** JS, DK, DW  
**EPA Methods:** 1, 2, 3, 4  
**D<sub>s</sub> (in.):** 39.0  
**% O<sub>2</sub>** 20.7  
**% CO<sub>2</sub>** 0.1  
**Start Run:** 12:12 PM  
**End Run:** 2:32 PM  
**Run Number:** 2 Filter ID \_\_\_\_\_

**Test Date:** July 12, 2023  
**Console ID:** C-009  
**Y<sub>m</sub> / ΔH<sub>@</sub>:** 1.013 1.554  
**Sampling Box ID:** B-1  
**Probe Assembly ID:** OR-P8-01  
**D<sub>n</sub> (in.):** 0.200 **D<sub>n</sub> ID:** OR-GN-200  
**Cp:** 0.84  
**P<sub>bar</sub> (in. Hg):** 30.12  
**p<sub>g</sub> (in. H<sub>2</sub>O):** 0.30  
**Minutes/Point:** 7.5  
**K-Factor:** 1.5

Point	Meter (dcf)	Inches H <sub>2</sub> O			Temperature Readings (°F)						Vacuum (in. Hg)
		Δp	ΔH	(Δp) <sup>1/2</sup>	t <sub>s</sub>	Probe	Filter	Last Impinger	t <sub>m</sub> Average	Filter CPM	
1	45.194	0.88	1.32	0.938	80	258	257	67	69	253	1
2	50.58	0.99	1.49	0.995	79	256	258	59	69	254	1
3	56.00	1.00	1.50	1.000	78	256	259	59	69	254	1
4	61.44	1.00	1.50	1.000	77	257	255	59	69	251	1
5	67.00	1.00	1.50	1.000	77	257	257	59	69	254	1
6	71.41	1.10	1.65	1.049	77	259	258	59	69	255	1
7	75.98	1.20	1.80	1.095	77	260	258	59	69	253	1
8	83.24	1.20	1.80	1.095	77	260	258	58	69	254	1
9	88.69	1.20	1.80	1.095	77	259	260	58	69	256	1
10	94.13	1.00	1.50	1.000	77	258	256	57	69	253	1
11	99.56	1.00	1.50	1.000	77	256	256	57	69	252	1
12	105.02	1.00	1.50	1.000	77	258	254	57	70	250	1
13	110.69	0.90	1.35	0.949	76	260	257	57	71	254	1
14	115.93	1.00	1.50	1.000	76	261	258	56	77	255	1
15	121.47	1.00	1.50	1.000	90	260	257	56	81	253	1
16	127.50	1.00	1.50	1.000	96	257	257	56	87	253	1
17	133.21	1.10	1.65	1.049	97	256	258	56	88	254	1
18	138.96	1.10	1.65	1.049	97	259	257	56	88	253	1
End	143.972										

**Total moisture collected (g):** 19.4  
**Theoretical maximum moisture collection at saturation (g):** 78.5  
**Pre System Leak Check (cfm):** 0.013 @ 18"  
**Post System Leak Check (cfm):** 0.014 @ 19"

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total	
Pre-test:	803.4	821.6	805.6		998.2	3428.8	g
Post-test:	813.3	826.3	808.1		1000.5	3448.2	g
Net gain:	9.9	4.7	2.5	0	2.3	19.4	g

# Advanced Industrial Resources, Inc.

## Field Data Sheet

**Client:** GP Toledo AMRS  
**Location:** Toledo, OR  
**Source:** Carbon Bed Outlet  
**Test Team:** JS, DK, DW  
**EPA Methods:** 1, 2, 3, 4  
**D<sub>s</sub> (in.):** 39.0  
**% O<sub>2</sub>** 20.8  
**% CO<sub>2</sub>** 0.0  
**Start Run:** 3:29 PM  
**End Run:** 6:01 PM  
**Run Number:** 3 Filter ID \_\_\_\_\_

**Test Date:** July 12, 2023  
**Console ID:** C-009  
**Y<sub>m</sub> / ΔH<sub>@</sub>:** 1.013 1.554  
**Sampling Box ID:** B-1  
**Probe Assembly ID:** OR-P8-01  
**D<sub>n</sub> (in.):** 0.200 **D<sub>n</sub> ID:** OR-GN-200  
**Cp:** 0.84  
**P<sub>bar</sub> (in. Hg):** 30.12  
**p<sub>g</sub> (in. H<sub>2</sub>O):** 0.30  
**Minutes/Point:** 7.5  
**K-Factor:** 1.5

Point	Meter (dcf)	Inches H <sub>2</sub> O			Temperature Readings (°F)						Vacuum (in. Hg)
		Δp	ΔH	(Δp) <sup>1/2</sup>	t <sub>s</sub>	Probe	Filter	Last Impinger	t <sub>m</sub> Average	Filter Error CPM	
1	151.295	0.90	1.35	0.949	78	258	256	62	94	253	4
2	156.86	1.00	1.50	1.000	78	259	257	47	93	253	4
3	162.70	1.00	1.50	1.000	78	259	255	48	93	251	4
4	169.05	1.00	1.50	1.000	76	257	257	48	86	252	4
5	174.76	1.00	1.50	1.000	77	260	257	49	79	252	4
6	180.49	1.10	1.65	1.049	77	259	258	49	74	254	4
7	185.86	1.10	1.65	1.049	77	259	257	49	72	253	4
8	191.96	1.20	1.80	1.095	78	256	260	49	71	256	4
9	196.41	1.20	1.80	1.095	78	259	259	49	70	253	4
10	202.07	1.00	1.50	1.000	78	260	258	49	69	254	4
11	207.42	1.00	1.50	1.000	78	257	257	49	69	253	4
12	213.37	1.00	1.50	1.000	78	258	255	49	69	251	4
13	219.56	0.89	1.34	0.943	78	260	258	50	68	254	4
14	223.57	1.00	1.50	1.000	78	260	258	50	68	254	4
15	227.59	1.00	1.50	1.000	78	258	257	50	68	253	4
16	235.41	1.00	1.50	1.000	92	259	255	50	69	251	4
17	240.79	1.10	1.65	1.049	99	260	257	50	69	253	4
18	246.12	1.10	1.65	1.049	99	256	259	51	69	252	4
19	251.51	1.10	1.65	1.049	100	258	258	51	69	254	4
End	257.863										

**Total moisture collected (g):** 37.9  
**Theoretical maximum moisture collection at saturation (g):** 86.3  
**Pre System Leak Check (cfm):** 0.016 @ 16"  
**Post System Leak Check (cfm):** 0.016 @ 16"

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total	
Pre-test:	832.7	823.6	806.2		1000.5	3463.0	g
Post-test:	860.0	827.8	809.4		1003.7	3500.9	g
Net gain:	27.3	4.2	3.2	0	3.2	37.9	g



# Advanced Industrial Resources, Inc.

## Field Data Sheet

Client: GP Toledo (Juno)      Test Date: 7-12-23  
 Location: Toledo, OK      Console ID: C-009  
 Source: Carbon Bed Outlet      Y<sub>m</sub> / ΔH@: 1.013/1.554  
 Test Team: W, DK, DW      Sampling Box ID: B-1  
 EPA Methods: NCASI 105-01      Probe Assembly ID: 02-18-01  
 D<sub>s</sub> (in.): 39      D<sub>n</sub> (in.): .200      D<sub>n</sub> ID: OK-6N-200  
 % O<sub>2</sub>: 20.79      Assumed B<sub>ws</sub>: 1%  
 % CO<sub>2</sub>: 0.03      P<sub>bar</sub> (in. Hg): 30.12  
 Start Run: 845      P<sub>g</sub> (in. H<sub>2</sub>O): .30  
 End Run: 1115      Minutes/Point: 7.5  
 Run Number: 1      Filter ID: \_\_\_\_\_      K-Factor: 1.5

2 hour  
24 min  
Run time

Point	Meter (dcf)	Inches H <sub>2</sub> O		Temperature Readings (°F)							Filter Exit (M5 or CPM)	Vacuum (in. Hg)
		Δp	ΔH	t <sub>s</sub>	Probe	Filter Box	Last Impinger	t <sub>m</sub>				
								Inlet	Outlet			
1	934.551	.89	1.38	71	260	257	58	63	63	254	1	
2	936.461	1.0	1.5	72	257	259	55	63	63	255	1	
3	944.539	1.0	1.5	72	258	258	53	63	63	254	1	
4	949.650	1.0	1.5	71	254	258	52	62	62	254	1	
5	954.713	1.0	1.5	71	259	256	52	63	63	251	1	
6	959.888	1.1	1.65	71	260	258	52	63	63	254	1	
7	964.953	1.2	1.80	71	262	257	52	63	63	253	1	
8	971.081	1.2	1.80	71	262	257	53	63	63	252	1	
9	977.199	1.1	1.65	72	257	257	53	64	64	252	1	
10	983.319	1.0	1.5	72	259	260	53	64	64	257	1	
11	989.370	1.0	1.5	72	259	258	54	64	64	253	1	
12	995.631	1.0	1.5	72	257	256	54	64	64	251	1	
Change Ports												
1	1001.593	.84	1.26	74	258	258	55	65	65	255	1	
2	1007.1657	1.0	1.5	73	259	258	55	66	66	254	1	
3	1013.097	.79	1.485	73	261	256	56	67	67	252	1	
4	1018.263	1.0	1.5	83	257	259	56	67	67	256	1	
5	1024.222	1.1	1.65	93	260	256	57	67	67	251	1	
6	1029.886	1.1	1.65	96	260	256	57	68	68	250	1	
7	1034.978	1.1	1.65	97	259	254	57	68	68	250	1	
8	1040.415	1.2	1.80	98	260	257	58	67	67	253	1	
9	1047.976											
10												
11												
12												
End												

	Moisture collected (g)					
	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
Pre-test:	850.5	811.5	822.3		980.7	3645
Post-test:	853.8	815.5	827.8		993.3	3490.4
Net gain:	3.3	4.0	5.5		12.6	25.4

Pre-Run Leak Checks (dcfm @ "Hg)  
 Sampling Line: 0.000 @ 16"  
 Pitot A: ✓  
 Pitot B: ✓

Reference Wt ID: OR-WS-500      OR-WS-100  
 Actual / Response    500 g / 500      100 g / 100

Post-Run Leak Checks (dcfm @ "Hg)  
 Sampling Line: 0.000 @ 16"  
 Pitot A: ✓  
 Pitot B: ✓

Test Team Leader Review: \_\_\_\_\_ Reagent 1: Hexane      Lot No: 20390188  
 Data Entry Review: \_\_\_\_\_ Reagent 2: \_\_\_\_\_      Lot No: \_\_\_\_\_

REV102921



# Advanced Industrial Resources, Inc.

## Field Data Sheet

Client: Gr Toledo (SUND) Test Date: 7-12-23  
 Location: Toledo, OR Console ID: C-004  
 Source: Carbon Bed Outlet  $Y_m / \Delta H @$ : 1.023/1.655  
 Test Team: JS, DK, DW Sampling Box ID: B-2  
 EPA Methods: NAAS1 105.01 Probe Assembly ID: \_\_\_\_\_  
 $D_s$  (in.): 39  $D_n$  (in.): 200  $D_n$  ID: OR-GN-200  
 % O<sub>2</sub>: 20.79 Assumed B<sub>ws</sub>: 1%  
 % CO<sub>2</sub>: 0.03 P<sub>bar</sub> (in. Hg): 30.12  
 Start Run: 845 P<sub>g</sub> (in. H<sub>2</sub>O): .30  
 End Run: 1115 Minutes/Point: 7.5  
 Run Number: 1 Daye Filter ID: \_\_\_\_\_ K-Factor: 1.6

2 hours  
24 min  
Run time

Point	Meter (dcf)	Inches H <sub>2</sub> O		Temperature Readings (°F)							Filter Exit (M5 or CPM)	Vacuum (in. Hg)
		$\Delta p$	$\Delta H$	$t_s$	Probe	Filter Box	Last Impinger	$t_m$				
								Inlet	Outlet			
1	742.572	.88	1.32	71	260	257	63	68	68	253	1	
2	747.372	1.0	1.6	72	262	256	60	68	68	252	1	
3	752.412	1.0	1.6	72	257	259	54	68	68	255	1	
4	757.567	1.0	1.6	71	255	255	53	69	69	251	1	
5	762.703	1.0	1.6	71	259	255	52	69	69	251	1	
6	767.873	1.0	1.6	71	257	256	52	69	69	252	1	
7	773.104	1.1	1.76	71	257	256	52	71	71	253	1	
8	778.783	1.2	1.92	71	256	256	52	71	71	253	1	
9	784.645	1.2	1.92	72	257	259	52	71	71	254	1	
10	790.463	1.2	1.92	72	259	256	53	71	71	253	1	
11	796.211	1.2	1.92	72	258	258	53	71	71	255	1	
12	802.148	1.2	1.92	72	260	259	53	72	72	256	1	
Change Ports												
1	807.775	.87	1.392	74	260	257	53	72	72	257	1	
2	813.590	.98	1.568	73	258	258	53	74	74	254	1	
3	819.064	1.0	1.60	73	258	257	54	74	74	253	1	
4	824.203	1.0	1.60	83	259	259	56	74	74	254	1	
5	830.114	1.1	1.76	83	256	259	57	75	75	256	1	
6	836.271	1.1	1.76	96	259	256	57	75	75	253	1	
7	841.088	1.2	1.92	97	258	257	57	75	75	254	1	
8	846.606	1.2	1.92	98	262	257	58	74	74	253	1	
9	848.870											
10												
11												
12												
End												

Moisture collected (g)

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
Pre-test:	910.1	875.1	859.6		950.7	3595.5 g
Post-test:	907.7	875.4	859.2		952.2	3594.5 g
Net gain:	-2.4	.3	-.4		1.5	-1 g

Pre-Run Leak Checks (dcfm @ "Hg)

Sampling Line: 0.015 @ 17"  
 Pitot A: ✓  
 Pitot B: ✓

Post-Run Leak Checks (dcfm @ "Hg)

Sampling Line: 0.012 @ 16"  
 Pitot A: ✓  
 Pitot B: ✓

Reference Wt ID: OR-WS-570 OR-WS-100  
 Actual / Response 500 g / 570 100 g / 100

Test Team Leader Review: \_\_\_\_\_ Reagent 1: Hexane Lot No: 20390188  
 Data Entry Review: \_\_\_\_\_ Reagent 2: \_\_\_\_\_ Lot No: \_\_\_\_\_

REV102921



# Advanced Industrial Resources, Inc.

## Field Data Sheet

Client: GP Toledo (JUNO) Test Date: 7-12-23  
 Location: Toledo, OH Console ID: L-009  
 Source: Carbon Bed Outlet  $Y_m / \Delta H @$ : 1.013/1.554  
 Test Team: JS, DK, DLW Sampling Box ID: B-1  
 EPA Methods: NCA51 105.01 Probe Assembly ID: 02-18-02  
 $D_s$  (in.): 39  $D_n$  (in.): 200  $D_n$  ID: OR-GAN-220  
 % O<sub>2</sub>: 20.72 Assumed B<sub>ws</sub>: 1%  
 % CO<sub>2</sub>: 0.05 P<sub>bar</sub> (in. Hg): 30.37  
 Start Run: 12:12 p<sub>g</sub> (in. H<sub>2</sub>O): .30  
 End Run: 14:32 Minutes/Point: 7.5  
 Run Number: 2 Filter ID: \_\_\_\_\_ K-Factor: 1.5

2:14  
Run Time

Point	Meter (dcf)	Inches H <sub>2</sub> O		Temperature Readings (°F)							Filter Exit (M5 or CPM)	Vacuum (in. Hg)
		$\Delta p$	$\Delta H$	$t_s$	Probe	Filter Box	Last Impinger	$t_m$				
								Inlet	Outlet			
1	45.194	.88	1.32	80	258	257	67	69	69	253	1	
2	52.584	.97	1.485	79	256	258	59	69	69	254	1	
3	56.002	1.0	1.5	78	256	259	59	69	69	254	1	
4	61.437	1.0	1.5	77	257	255	59	69	69	251	1	
5	67.004	1.0	1.5	77	257	257	59	69	69	254	1	
6	71.408	1.1	1.65	77	259	258	59	69	69	255	1	
7	75.980	1.2	1.80	77	260	258	59	69	69	253	1	
8	83.239	1.2	1.80	77	260	258	58	69	69	254	1	
9	88.687	1.2	1.65	77	259	260	58	69	69	256	1	
10	94.125	1.0	1.50	77	258	256	57	69	69	253	1	
11	99.564	1.0	1.50	77	256	256	57	69	69	252	1	
12	105.020	1.0	1.50	77	258	254	57	70	70	250	1	
Change Ports												
1	110.688	.90	1.35	76	260	257	57	71	71	254	1	
2	115.927	1.0	1.50	76	261	258	56	77	77	255	1	
3	121.477	1.0	1.50	90	260	257	56	81	81	253	1	
4	127.498	1.0	1.50	96	257	257	56	87	87	253	1	
5	133.214	1.1	1.65	97	256	258	56	88	88	254	1	
6	138.962	1.1	1.65	97	259	257	56	88	88	253	1	
7	143.972											
8												
9												
10												
11												
12												
End												

6:00  
Port change

Moisture collected (g)

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
Pre-test:	803.4	821.6	805.6		998.2	3428.8 g
Post-test:	813.3	826.3	805.1		1000.5	3448.2 g
Net gain:						19.4 g

Pre-Run Leak Checks (dcfm @ "Hg)  
 Sampling Line: 0.013 @ 18"  
 Pitot A: ✓  
 Pitot B: ✓

Reference Wt ID: OR-WS-500 OR-WS-100  
 Actual / Response    500 g / 500    100 g / 100

Post-Run Leak Checks (dcfm @ "Hg)  
 Sampling Line: 0.014 @ 19"  
 Pitot A: ✓  
 Pitot B: ✓

Test Team Leader Review: \_\_\_\_\_ Reagent 1: Hexane Lot No: 20390188  
 Data Entry Review: \_\_\_\_\_ Reagent 2: \_\_\_\_\_ Lot No: \_\_\_\_\_

REV102921



# Advanced Industrial Resources, Inc.

## Field Data Sheet

Client: GP Toledo (Juno) Test Date: 7-12-23  
 Location: Toledo, OR Console ID: C-004  
 Source: Carbon Bed Outfall  $Y_m / \Delta H @$ : 1.023 / 1:655  
 Test Team: JS, DK, DW Sampling Box ID: B-2  
 EPA Methods: NCASI 105.01 Probe Assembly ID: OR-PB-01  
 $D_s$  (in.): 39  $D_n$  (in.): 200  $D_n$  ID: GN-OR-200  
 % O<sub>2</sub>: 20.72 Assumed B<sub>ws</sub>: 1%  
 % CO<sub>2</sub>: 0.05 P<sub>bar</sub> (in. Hg): 30.12  
 Start Run: 12:12 P<sub>g</sub> (in. H<sub>2</sub>O): .30  
 End Run: 14:32 Minutes/Point: 7.5  
 Run Number: 2 Low Spike Filter ID: \_\_\_\_\_ K-Factor: 1.6

2:14  
Runtime

Point	Meter (dcf)	Inches H <sub>2</sub> O		Temperature Readings (°F)							Vacuum (in. Hg)
		$\Delta p$	$\Delta H$	$t_s$	Probe	Filter Box	Last Impinger	$t_m$		Filter Exit (M5 or CPM)	
								Inlet	Outlet		
1	856.964	.88	1.408	80	260	258	66	73	73	254	1
2	856.117	.97	1.552	79	259	258	57	73	73	254	1
3	861.332	1.0	1.60	78	257	257	56	74	74	254	1
4	866.471	1.0	1.60	77	259	258	55	75	75	254	1
5	871.780	1.0	1.60	77	260	258	55	75	75	254	1
6	876.914	1.0	1.60	77	260	257	56	76	76	254	1
7	880.225	1.1	1.76	77	258	258	56	75	75	255	1
8	887.181	1.2	1.92	77	257	257	56	77	77	253	1
9	892.304	1.2	1.92	77	259	256	57	77	77	252	1
10	897.642	1.2	1.92	77	258	255	57	78	78	252	1
11	903.511	1.2	1.92	77	259	257	57	81	81	253	1
12	908.344	1.2	1.92	77	259	259	57	81	81	256	1
Change Ports											
1	913.831	.88	1.408	77	260	256	58	83	83	252	1
2	919.065	1.0	1.60	76	258	257	58	85	85	253	1
3	924.491	1.0	1.60	90	259	258	58	86	86	254	1
4	930.520	1.0	1.60	96	258	256	59	88	88	252	1
5	936.351	1.0	1.60	96	259	257	59	90	90	243	1
6	942.120	1.1	1.76	96	257	257	59	90	90	243	1
7	947.208										
8											
9											
10											
11											
12											
End											

6:00  
Part change

### Moisture collected (g)

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
810.8 Pre-test:	805.6	832.1	816.6		952.2	3406.5 g
821.9 Post-test:	815.8	838.3	822.1		970.2	3446.4 g
Net gain:						39.9 g

### Pre-Run Leak Checks (dcfm @ "Hg)

Sampling Line: 0.002 @ 19"  
 Pitot A:   
 Pitot B:

### Post-Run Leak Checks (dcfm @ "Hg)

Sampling Line: 0.003 @ 17"  
 Pitot A:   
 Pitot B:

Reference Wt ID: OR-WS-500 OK-WS-100  
 Actual / Response 500 g / 500 100 g / 100

Test Team Leader Review: \_\_\_\_\_ Reagent 1: Hexane Lot No: 20390188  
 Data Entry Review: \_\_\_\_\_ Reagent 2: \_\_\_\_\_ Lot No: \_\_\_\_\_

REV102921



# Advanced Industrial Resources, Inc.

## Field Data Sheet

Client: GP Toledo (Juno)  
 Location: Toledo, OR  
 Source: Carbon Bed Outlet  
 Test Team: SS, DK, DW  
 EPA Methods: NCASI 105.01  
 D<sub>s</sub> (in.): 39  
 % O<sub>2</sub>: 20.79  
 % CO<sub>2</sub>: 0.07  
 Start Run: 15:29  
 End Run: 18:01  
 Run Number: 3 Filter ID: \_\_\_\_\_

Test Date: 7.12.13  
 Console ID: L-009  
 Y<sub>m</sub> / ΔH@: 1.013/1.554  
 Sampling Box ID: B-1  
 Probe Assembly ID: P8-01  
 D<sub>n</sub> (in.): 200 D<sub>n</sub> ID: OR-GN-200  
 Assumed B<sub>wss</sub>: 1%  
 P<sub>bar</sub> (in. Hg): 30.12  
 P<sub>g</sub> (in. H<sub>2</sub>O): .30  
 Minutes/Point: 7.5  
 K-Factor: 1.5

2:24  
Run Time

6:00  
Port  
Change

Point	Meter (dcf)	Inches H <sub>2</sub> O		Temperature Readings (°F)							Filter Exit (M5 or CPM)	Vacuum (in. Hg)
		Δp	ΔH	t <sub>s</sub>	Probe	Filter Box	Last Impinger	t <sub>m</sub>				
								Inlet	Outlet			
1	151.295	.90	1.35	78	258	256	62	94	94	253	4	
2	156.862	1.0	1.50	78	259	257	47	93	93	253	4	
3	162.645	1.0	1.50	78	259	255	48	93	93	251	4	
4	169.046	1.0	1.50	76	257	257	48	86	86	252	4	
5	174.760	1.0	1.50	77	260	257	49	79	79	252	4	
6	180.492	1.1	1.65	77	259	258	49	74	74	254	4	
7	185.860	1.1	1.65	77	259	257	49	72	72	253	4	
8	191.956	1.2	1.80	78	256	260	49	71	71	256	4	
9	196.461	1.2	1.80	78	259	257	49	70	70	253	4	
10	202.071	1.0	1.50	78	260	258	49	69	69	254	4	
11	207.422	1.0	1.50	78	257	257	49	69	69	253	4	
12	213.373	1.0	1.50	78	253	255	49	69	69	251	4	
Change Ports												
1	219.563	.89	1.375	78	260	258	50	68	68	254	4	
2	223.570	1.0	1.50	78	260	258	50	68	68	254	4	
3	227.588	1.0	1.50	78	258	257	50	68	68	253	4	
4	235.411	1.0	1.50	92	259	255	50	69	69	251	4	
5	240.791	1.1	1.65	99	260	257	50	69	69	253	4	
6	246.115	1.1	1.65	99	256	259	51	69	69	252	4	
7	251.512	1.1	1.65	100	258	258	51	69	69	254	4	
8	257.863											
9												
10												
11												
12												
End												

Moisture collected (g)

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
Pre-test:	832.7	827.6	806.2		1000.5	3468 g
Post-test:	860.0	827.9	809.4		1003.7	3500.9 g
Net gain:						32.9 g

Pre-Run Leak Checks (dcfm @ "Hg)  
 Sampling Line: 0.016 @ 16"  
 Pitot A:   
 Pitot B:

Reference Wt ID: WS-OR-500      WS-OR-100  
 Actual / Response    500 g / 500      100 g / 100

Post-Run Leak Checks (dcfm @ "Hg)  
 Sampling Line: 0.016 @ 16"  
 Pitot A:   
 Pitot B:

Test Team Leader Review: \_\_\_\_\_ Reagent 1: Hexane Lot No: 20390188  
 Data Entry Review: \_\_\_\_\_ Reagent 2: \_\_\_\_\_ Lot No: \_\_\_\_\_



# Advanced Industrial Resources, Inc.

## Field Data Sheet

Client: GP Toledo (Juno) Test Date: 7-12-23  
 Location: Toledo, OR Console ID: ~~C-001~~ C-004  
 Source: Carbon Bed Outlet Y<sub>m</sub> / ΔH@: 1.023/1.655  
 Test Team: SS, DE, DW Sampling Box ID: B-2  
 EPA Methods: MSA 105.01 Probe Assembly ID: P8-02  
 D<sub>s</sub> (in.): 39 D<sub>n</sub> (in.): .200 D<sub>n</sub> ID: GN-OR-200  
 % O<sub>2</sub>: 20.79 Assumed B<sub>ws</sub>: 1%  
 % CO<sub>2</sub>: 0.03 P<sub>bar</sub> (in. Hg): 1<sup>st</sup> 30.12  
 Start Run: 1529 p<sub>g</sub> (in. H<sub>2</sub>O): .30  
 End Run: 18:01 Minutes/Point: 7.5  
 Run Number: 3 high spike Filter ID: \_\_\_\_\_ K-Factor: 1.6

Point	Meter (dcf)	Inches H <sub>2</sub> O		Temperature Readings (°F)							Filter Exit (M5 or CPM)	Vacuum (in. Hg)
		Δp	ΔH	t <sub>s</sub>	Probe	Filter Box	Last Impinger	t <sub>m</sub>				
								Inlet	Outlet			
1	947.975	.91	1.456	78	259	256	64	89	89	253	1	
2	952.996	1.0	1.60	78	259	257	49	88	88	254	1	
3	959.154	1.0	1.60	78	257	257	49	87	87	254	1	
4	<del>971.717</del>	1.0	1.60	76	259	257	49	85	85	254	1	
5	970.710	1.0	1.60	76	261	256	49	84	84	253	1	
6	972.612	1.1	1.76	75	260	258	49	82	82	256	1	
7	981.400	1.2	1.92	75	260	257	50	81	81	257	1	
8	987.065	1.2	1.92	78	258	257	50	80	80	254	1	
9	991.395	1.2	1.92	78	257	259	50	81	81	256	1	
10	996.974	1.2	1.92	78	258	256	50	80	80	252	1	
11	1002.030	1.2	1.92	78	256	258	50	79	79	255	1	
12	1007.717	1.2	1.92	78	259	257	50	79	79	254	1	
Change Ports												
1	1013.511	.90	1.44	78	259	258	50	78	78	255	1	
2	1018.420	1.0	1.60	78	259	257	50	78	78	253	1	
3	1022.008	1.0	1.60	78	260	257	51	78	78	253	1	
4	1029.003	1.0	1.60	98	261	258	51	79	79	254	1	
5	1034.455	1.0	1.60	99	257	257	51	78	78	252	1	
6	1039.823	1.1	1.76	99	257	259	51	78	78	253	1	
7	1045.113	1.1	1.76	100	257	258	52	77	77	253	1	
8	1051.307											
9												
10												
11												
12												
End												

96497A  
6:00 Part Change

### Moisture collected (g)

	Imp. 1	Imp. 2	Imp. 3	Imp. 4	SG Imp.	Total
Pre-test:	854.0	793.4	806.8		970.2	3424.4 g
Post-test:	879.2	797.6	806.6		983.3	3466.7 g
Net gain:						42.3 g

### Pre-Run Leak Checks (dcfm @ "Hg)

Sampling Line: 0.001 @ 16"  
 Pitot A: ✓  
 Pitot B: ✓

### Post-Run Leak Checks (dcfm @ "Hg)

Sampling Line: 0.002 @ 17"  
 Pitot A: ✓  
 Pitot B: ✓

Reference Wt ID: WS-OR-500      WS-OR-100  
 Actual / Response    500 g / 500      100 g / 100

Test Team Leader Review: \_\_\_\_\_ Reagent 1: Hexane Lot No: 20390188  
 Data Entry Review: \_\_\_\_\_ Reagent 2: \_\_\_\_\_ Lot No: \_\_\_\_\_

REV102921





**APPENDIX E**

**LABORATORY REPORTS**

# Advanced Industrial Resources, Inc.

3407 Novis Pointe NW  
Acworth, GA 30101

Georgia Pacific  
Juno Toledo, OR  
Client Project # KR11456

Analytical Report  
(0623-263)

## *NCASI Method A105.01*

Methanol, Phenol (By GC/FID)  
Acetaldehyde, Formaldehyde, Propionaldehyde, Acrolein (By GC/NPD)



## Enthalpy Analytical, LLC

Phone: (919) 850 - 4392 / Fax: (919) 850 - 9012 / [www.enthalpy.com](http://www.enthalpy.com)  
800-1 Capitola Drive Durham, NC 27713-4385



I certify that to the best of my knowledge all analytical data presented in this report:

- Have been checked for completeness
- Are accurate, error-free, and legible
- Have been conducted in accordance with approved protocol, and that all deviations and analytical problems are summarized in the appropriate narrative(s)

This analytical report was prepared in Portable Document Format (.PDF). This report shall not be reproduced except in full without approval of the laboratory. This will provide assurance that parts of a report are not taken out of context.



QA Review Performed by – Jennifer Bowker

Report Issued: 8/4/23



# Summary of Results

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/FID) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Summary Table

Catch Weight (ug)

Sample ID	Methanol	Phenol
Test 1 Normal	2,008	102 J
Test 1 DUP	34.6 ND	47.8 ND
Test 2 Normal	3,451	107 J
Test 2 Low SPK	4,374	575
Test 3 Normal	4,853	182
Test 3 High SPK	11,347	23,138
Train Spike	7,093	23,629
Field SPK - Low	591	619
Field SPK - High	7,161	22,439
BHA Blank	17.7 ND	24.4 ND

## Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

### Summary Table

Compound / Catch Weight (ug)

Sample ID	Acetaldehyde	Acrolein	Formaldehyde	Propionaldehyde
Test 1 Normal	1,772	4.60 ND	10.8 J	7.50 J
Test 1 DUP	29.5 J	6.69 ND	9.50 J	11.5 J
Test 2 Normal	2,720	4.71 ND	14.9 J	6.86 J
Test 2 Low SPK	3,514	206	272	265
Test 3 Normal	3,296	4.71 ND	20.5 J	10.4 J
Test 3 High SPK	13,496	12,208	6,744	13,614
Train Spike	11,003	12,863	7,287	14,202
Field SPK - Low	346	300	301	361
Field SPK - High	10,374	12,197	7,177	13,346
BHA Blank	13.7 J	13.6 J	8.13 J	15.9 J

# Results

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/FID) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Methanol

Sample ID	Filename	MDL	Curve Min	Curve Max	Ret Time (min)	Conc. (ug/mL)	DF	Liquid Vol (mL)	Catch Weight (ug)	Flag
Test 1 Normal	001F0201.D	0.0679	0.380	949	11.72	6.08	1	330	2,008	
Test 1 DUP	002F0301.D	0.0679	0.380	949	NA	0.0679	1	510	34.6	ND
Test 2 Normal	003F0401.D	0.0679	0.380	949	11.74	9.86	1	350	3,451	
Test 2 Low SPK	004F0501.D	0.0679	0.380	949	11.74	12.1	1	360	4,374	
Test 3 Normal	006F0701.D	0.0679	0.380	949	11.73	13.9	1	350	4,853	
Test 3 High SPK	007F0801.D	0.0679	0.380	949	11.73	36.6	1	310	11,347	
Train Spike	008F0901.D	0.0679	0.380	949	11.74	22.5	1	315	7,093	
									Spike Amount	7,354
									Spike Recovery (%)	96.4%
Field SPK - Low	009F1001.D	0.0679	0.380	949	11.73	1.94	1	305	591	
									Spike Amount	513
									Spike Recovery (%)	115%
Field SPK - High	011F1101.D	0.0679	0.380	949	11.74	22.6	1	317	7,161	
									Spike Amount	7,354
									Spike Recovery (%)	97.4%
BHA Blank	097F0401.D	0.0679	0.380	949	NA	0.0679	1	260	17.7	ND

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/FID) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Phenol

Sample ID	Filename	MDL	Curve Min	Curve Max	Ret Time (min)	Conc. (ug/mL)	DF	Liquid Vol (mL)	Catch Weight (ug)	Flag
Test 1 Normal	001F0201.D	0.0938	0.419	1,047	24.83	0.310	1	330	102	J
Test 1 DUP	002F0301.D	0.0938	0.419	1,047	NA	0.0938	1	510	47.8	ND
Test 2 Normal	003F0401.D	0.0938	0.419	1,047	24.86	0.306	1	350	107	J
Test 2 Low SPK	004F0501.D	0.0938	0.419	1,047	24.84	1.60	1	360	575	
Test 3 Normal	006F0701.D	0.0938	0.419	1,047	24.85	0.520	1	350	182	
Test 3 High SPK	007F0801.D	0.0938	0.419	1,047	24.83	74.6	1	310	23,138	
Train Spike	008F0901.D	0.0938	0.419	1,047	24.84	75.0	1	315	23,629	
									Spike Amount	22,198
									Spike Recovery (%)	106%
Field SPK - Low	009F1001.D	0.0938	0.419	1,047	24.84	2.03	1	305	619	
									Spike Amount	498
									Spike Recovery (%)	124%
Field SPK - High	011F1101.D	0.0938	0.419	1,047	24.84	70.8	1	317	22,439	
									Spike Amount	22,198
									Spike Recovery (%)	101%
BHA Blank	097F0401.D	0.0938	0.419	1,047	NA	0.0938	1	260	24.4	ND

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/FID) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## QC Samples

QC Type	QC Sample Name		Methanol	Phenol
Spiked Blank Solvent	gcprep5570 #LCS-L-BHA	catch (ug)	514	515
	spiked:	spike (ug)	513	498
	spikeprep2042.SP-LOW * 100uL	recovery	100%	104%
Spiked Blank Solvent	gcprep5570 #LCS-H-BHA	catch (ug)	7,082	22,697
	spiked:	spike (ug)	7,355	22,198
	spikeprep2042.SP-HIGH * 1000uL	recovery	96.3%	102%
Lab Dup	LD / Test 2 Low SPK	ug/mL	11.5	1.80
	Test 2 Low SPK	ug/mL	12.1	1.60
		RD	5.8%	12.1%
Blank Solvent	gcprep5570 #MB-BHA	ug/mL	ND	ND



# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/FID) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Spike and Recovery Calculations

---

Analyte: Methanol

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 2</b>	591	Spiked Train		4,374	96.244	171%
		Un-spiked Train		3,451	98.778	

Analyte: Methanol

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 3</b>	7,161	Spiked Train		11,347	103.832	92.4%
		Un-spiked Train		4,853	106.568	

Analyte: Phenol

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 2</b>	619	Spiked Train		575	96.244	76.0%
		Un-spiked Train	J	107	98.778	

Analyte: Phenol

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 3</b>	22,439	Spiked Train		23,138	103.832	102%
		Un-spiked Train		182	106.568	

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/FID) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Duplicate % Difference Calculations

---

Analyte: Methanol

	Flag	Catch (ug)	Sample Volume	Difference (%)
<b>Test 1</b>		2,008	108.425	NA
	ND	34.6	106.298	

Analyte: Phenol

	Flag	Catch (ug)	Sample Volume	Difference (%)
<b>Test 1</b>	J	102	108.425	NA
	ND	47.8	106.298	

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Acetaldehyde

Client's Sample Name	Filename #1	MDL	Curve Min	Curve Max	Ret Time (min)	Conc #1 (ug/mL)	DF	Liquid Vol (mL)	Catch Weight (ug)	Flag
Test 1 Normal	026B0801.D	0.0519	0.473	108	NA	20.6	1	86.0	1,772	
Test 1 DUP	027B0901.D	0.0519	0.473	108	NA	0.236	1	125	29.5	J
Test 2 Normal	028B1001.D	0.0519	0.473	108	NA	30.9	1	88.0	2,720	
Test 2 Low SPK	029B1101.D	0.0519	0.473	108	NA	38.2	1	92.0	3,514	
Test 3 Normal	031B1301.D	0.0519	0.473	108	NA	37.5	1	88.0	3,296	
Test 3 High SPK	044B0601.D	0.0519	0.473	108	NA	18.7	10	72.0	13,496	
Train Spike	043B0501.D	0.0519	0.473	108	NA	32.7	4	84.0	11,003	
									Spike Amount	10,080
									Spike Recovery (%)	109%
Field SPK - Low	034B1701.D	0.0519	0.473	108	NA	4.33	1	80.0	346	
									Spike Amount	310
									Spike Recovery (%)	112%
Field SPK - High	042B0401.D	0.0519	0.473	108	NA	30.2	4	86.0	10,374	
									Spike Amount	10,080
									Spike Recovery (%)	103%
BHA Blank	036B1901.D	0.0519	0.473	108	NA	0.208	1	66.0	13.7	J

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Acrolein

Client's Sample Name	Filename #1	MDL	Curve Min	Curve Max	Ret Time (min)	Conc #1 (ug/mL)	DF	Liquid Vol (mL)	Catch Weight (ug)	Flag
Test 1 Normal	026B0801.D	0.0535	0.499	113	NA	0.0535	1	86.0	4.60	ND
Test 1 DUP	027B0901.D	0.0535	0.499	113	NA	0.0535	1	125	6.69	ND
Test 2 Normal	028B1001.D	0.0535	0.499	113	NA	0.0535	1	88.0	4.71	ND
Test 2 Low SPK	029B1101.D	0.0535	0.499	113	NA	2.24	1	92.0	206	
Test 3 Normal	031B1301.D	0.0535	0.499	113	NA	0.0535	1	88.0	4.71	ND
Test 3 High SPK	044B0601.D	0.0535	0.499	113	NA	17.0	10	72.0	12,208	
Train Spike	043B0501.D	0.0535	0.499	113	NA	38.3	4	84.0	12,863	
									Spike Amount	13,050
									Spike Recovery (%)	98.6%
Field SPK - Low	034B1701.D	0.0535	0.499	113	NA	3.74	1	80.0	300	
									Spike Amount	310
									Spike Recovery (%)	96.7%
Field SPK - High	042B0401.D	0.0535	0.499	113	NA	35.5	4	86.0	12,197	
									Spike Amount	13,050
									Spike Recovery (%)	93.5%
BHA Blank	036B1901.D	0.0535	0.499	113	NA	0.206	1	66.0	13.6	J

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Formaldehyde

Client's Sample Name	Filename #1	MDL	Curve Min	Curve Max	Ret Time (min)	Conc #1 (ug/mL)	DF	Liquid Vol (mL)	Catch Weight (ug)	Flag
Test 1 Normal	026B0801.D	0.0485	0.485	110	8.11	0.126	1	86.0	10.8	J
Test 1 DUP	027B0901.D	0.0485	0.485	110	8.14	0.0760	1	125	9.50	J
Test 2 Normal	028B1001.D	0.0485	0.485	110	8.14	0.170	1	88.0	14.9	J
Test 2 Low SPK	029B1101.D	0.0485	0.485	110	8.12	2.95	1	92.0	272	
Test 3 Normal	031B1301.D	0.0485	0.485	110	8.14	0.233	1	88.0	20.5	J
Test 3 High SPK	032B1401.D	0.0485	0.485	110	8.11	93.7	1	72.0	6,744	
Train Spike	033B1501.D	0.0485	0.485	110	8.11	86.7	1	84.0	7,287	
									Spike Amount	7,077
									Spike Recovery (%)	103%
Field SPK - Low	034B1701.D	0.0485	0.485	110	8.12	3.77	1	80.0	301	
									Spike Amount	303
									Spike Recovery (%)	99.3%
Field SPK - High	035B1801.D	0.0485	0.485	110	8.11	83.5	1	86.0	7,177	
									Spike Amount	7,077
									Spike Recovery (%)	101%
BHA Blank	036B1901.D	0.0485	0.485	110	8.14	0.123	1	66.0	8.13	J

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Propionaldehyde

Client's Sample Name	Filename #1	MDL	Curve Min	Curve Max	Ret Time (min)	Conc #1 (ug/mL)	DF	Liquid Vol (mL)	Catch Weight (ug)	Flag
Test 1 Normal	026B0801.D	0.0593	0.482	110	NA	0.0872	1	86.0	7.50	J
Test 1 DUP	027B0901.D	0.0593	0.482	110	NA	0.0918	1	125	11.5	J
Test 2 Normal	028B1001.D	0.0593	0.482	110	NA	0.0780	1	88.0	6.86	J
Test 2 Low SPK	029B1101.D	0.0593	0.482	110	NA	2.88	1	92.0	265	
Test 3 Normal	031B1301.D	0.0593	0.482	110	NA	0.118	1	88.0	10.4	J
Test 3 High SPK	044B0601.D	0.0593	0.482	110	NA	18.9	10	72.0	13,614	
Train Spike	043B0501.D	0.0593	0.482	110	NA	42.3	4	84.0	14,202	
									Spike Amount	13,644
									Spike Recovery (%)	104%
Field SPK - Low	034B1701.D	0.0593	0.482	110	NA	4.52	1	80.0	361	
									Spike Amount	305
									Spike Recovery (%)	118%
Field SPK - High	042B0401.D	0.0593	0.482	110	NA	38.8	4	86.0	13,346	
									Spike Amount	13,644
									Spike Recovery (%)	97.8%
BHA Blank	036B1901.D	0.0593	0.482	110	NA	0.241	1	66.0	15.9	J

## Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

### QC Samples

QC Type	QC Sample Name		Acetaldehyde	Acrolein	Formaldehyde	Propionaldehyde
Spiked Blank Solvent	gcprep5570 #LCS-L-HEX	catch (ug)	313	281	298	302
	spiked:	spike (ug)	310	310	303	305
	spikeprep2042.SP-LOW * 100uL	recovery	101%	90.8%	98.4%	99.1%
Spiked Blank Solvent	gcprep5570 #LCS-H-HEX	catch (ug)	10,601	12,619	7,371	13,708
	spiked:	spike (ug)	10,080	13,050	7,077	13,644
	spikeprep2042.SP-HIGH * 1000uL	recovery	105%	96.7%	104%	100%
Lab Dup	LD / Test 2 Low SPK	ug/mL	37.9	2.23	2.93	2.89
	Test 2 Low SPK	ug/mL	38.2	2.24	2.95	2.88
		RD	0.8%	0.3%	0.6%	0.3%
Blank Solvent	gcprep5570 #MB-HEX	ug/mL	0.132	0.204	0.0820	0.211

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Spike and Recovery Calculations

---

Analyte: Acetaldehyde

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 2</b>	346	Spiked Train		3,514	96.244	250%
		Un-spiked Train		2,720	98.778	

Analyte: Acetaldehyde

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 3</b>	10,374	Spiked Train		13,496	103.832	99.1%
		Un-spiked Train		3,296	106.568	

Analyte: Acrolein

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 2</b>	300	Spiked Train		206	96.244	68.8%
		Un-spiked Train	ND	4.71	98.778	

Analyte: Acrolein

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 3</b>	12,197	Spiked Train		12,208	103.832	100%
		Un-spiked Train	ND	4.71	106.568	

Analyte: Formaldehyde

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 2</b>	301	Spiked Train		272	96.244	85.4%
		Un-spiked Train	J	14.9	98.778	



# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Spike and Recovery Calculations

---

Analyte: Formaldehyde

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 3</b>	7,177	Spiked Train		6,744	103.832	93.7%
		Un-spiked Train	J	20.5	106.568	

Analyte: Propionaldehyde

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 2</b>	361	Spiked Train		265	96.244	71.6%
		Un-spiked Train	J	6.86	98.778	

Analyte: Propionaldehyde

	Spike Amount		Flag	Catch (ug)	Sample Volume	Recovery (%)
<b>Test 3</b>	13,346	Spiked Train		13,614	103.832	102%
		Un-spiked Train	J	10.4	106.568	

# Enthalpy Analytical

Company: Advanced Industrial Resources

Job No.: 0623-263 - NCASI A105.01 (GC/NPD) Analysis

Client No.: KR11456 Site: GP-Juno Toledo, OR

## Duplicate % Difference Calculations

---

Analyte: Acetaldehyde

	Flag	Catch (ug)	Sample Volume	Difference (%)
<b>Test 1</b>		1,772	108.425	193%
	J	29.5	106.298	

Analyte: Acrolein

	Flag	Catch (ug)	Sample Volume	Difference (%)
<b>Test 1</b>	ND	4.60	108.425	NA
	ND	6.69	106.298	

Analyte: Formaldehyde

	Flag	Catch (ug)	Sample Volume	Difference (%)
<b>Test 1</b>	J	10.8	108.425	10.9%
	J	9.50	106.298	

Analyte: Propionaldehyde

	Flag	Catch (ug)	Sample Volume	Difference (%)
<b>Test 1</b>	J	7.50	108.425	43.8%
	J	11.5	106.298	

# Narrative Summary



# Enthalpy Analytical Narrative Summary

Company Job No. Client ID.	Advanced Industrial Resources 0623-263 NCASI Method A105.01 KR11456 Site: GP – Juno Toledo, OR
Custody	<p>Alyssa Miller received the samples on 7/14/23 at 4.6 °C after being relinquished by Advanced Industrial Resources. The samples were received in good condition.</p> <p>Prior to, during, and after analysis, the samples were kept under lock with access only to authorized personnel by Enthalpy Analytical, LLC.</p>
Analysis	<p>The samples were analyzed for methanol, phenol, acetaldehyde, acrolein, formaldehyde, and propionaldehyde using the analytical procedures in NCASI Method ISS/FP-A105.01, "Impinger Source Sampling Method for Selected Aldehydes, Ketones, and Polar Compounds".</p> <p>The initial volumes of the combined aqueous BHA/hexane samples were measured. The combined samples were transferred to separatory funnels for the first extraction. The samples were shaken for 30 seconds and the hexane and BHA layers allowed to separate. Two additional extractions were performed by adding fresh hexane to the aqueous BHA samples in the separatory funnels, shaking for 30 seconds and allowing the hexane layers to separate. The hexane extracts were combined for each sample. The final hexane and BHA volumes were measured and recorded.</p> <p>The Gas Chromatograph "Lolita" was used for the analyses of the hexane extract fractions for acetaldehyde, acrolein, formaldehyde, and propionaldehyde.</p> <p>The Gas Chromatograph "Fester" was used for the analyses of the aqueous BHA fractions for methanol and phenol.</p>
Calibration	<p>The calibration curves are located in the back of this report. For each calibration curve used, the first page of the curve contains all method specific parameters (i.e., curve type, origin, weight, etc.) used to quantify the samples. The calibration curve section also includes a table with the Retention Time (RetTime), Level (Lvl), Amount (corresponding units), Area, Response Factor (Amt/Area) and the analyte Name. The calibration table is used to identify (by retention time) and quantify each target compound.</p>
Chrom. Conditions	<p>The acquisition methods (FESTER0258.M and LOLITA0349X.M) may be made available upon request.</p>

## Enthalpy Analytical Narrative Summary

Company	Advanced Industrial Resources
Job No.	0623-263 NCASI Method A105.01
Client ID.	KR11456 Site: GP – Juno Toledo, OR

QC Notes	<p>Methanol, phenol were not present at concentrations above their MDL value in the analysis of the client's Field Blank. While acetaldehyde, acrolein, formaldehyde, and propionaldehyde were present at concentrations greater than their MDL value, but below their LOQ value.</p> <p>Phenol, acetaldehyde, acrolein, formaldehyde, and propionaldehyde were present at concentrations greater than MDL value, but below the LOQ in the analysis of the laboratory method blank. Methanol was not present at concentration greater than the MDL in the analysis of the method blank.</p> <p>Laboratory Duplicates (LD) were prepared and analyzed with the samples using aliquots of sample <b>Test 2 Low Spike</b>. The percent difference values were 12.1% or less.</p> <p>The laboratory prepared eight <b>Low</b> aqueous spike solutions containing 435 µg/mL of methanol (plus an additional 78.0 µg/mL of methanol from formaldehyde) , 498 µg/mL of phenol, 310 µg/mL of of acetaldehyde, 310 µg/mL of acrolein, 303 µg/mL of formaldehyde, and 305 µg/mL of propionaldehyde. The The laboratory also prepared five <b>High</b> aqueous spike solutions containing 5,536 µg/mL of methanol (plus an additional 1,818 µg/mL of methanol from formaldehyde) , 22,198 µg/mL of phenol, 10,080 µg/mL of of acetaldehyde, 13,050 µg/mL of acrolein, 7,077 µg/mL of formaldehyde, and 13,644 µg/mL of propionaldehyde. Two vials (of each level) of the spike solution were provided to the client prior to sample collection while two were retained by the lab to be analyzed as Laboratory Control Samples (LCS).</p> <p>The lab prepared, extracted, and analyzed a LCS from each level, with the samples, and yielded recovery values between 90.8% and 105%.</p>
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Reporting Notes	<p>Acetaldehyde, acrolein, and propionaldehyde are identified as two peaks ("1" and "2"). This is normal for the method's derivatization process, and results for both peaks are combined on the chromatograms and the results pages. Only the total results are included on the results tables.</p> <p>A fresh aliquot of samples <b>Run 1 Duplicate</b>, <b>Run 2 Low Spike</b>, and <b>Field Spike -Low</b> were analyzed for methanol and phenol, confirming the original results. Only the original data is included in this report.</p> <p>A fresh aliquot of samples <b>Run 1 Duplicate</b>, <b>Run 2</b>, <b>Run 2 Low Spike</b>, and <b>Blank</b> were analyzed for acetaldehyde, acrolein, formaldehyde, and propionaldehyde, confirming the original results. Only the original data is included in this report.</p>
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# Enthalpy Analytical Narrative Summary

Company	Advanced Industrial Resources
Job No.	0623-263 NCASI Method A105.01
Client ID.	KR11456 Site: GP – Juno Toledo, OR

Reporting Notes (Continued)	<p>These analyses met the requirements of the TNI Standard. Any deviations from the requirements of the reference method or TNI Standard have been stated above.</p> <p>The results presented in this report are representative of the samples as provided to the laboratory.</p>
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## General Reporting Notes

The following are general reporting notes that are applicable to all Enthalpy Analytical, LLC data reports, unless specifically noted otherwise.

- Any analysis which refers to the method as “**Type**” represents a planned deviation from the reference method. For instance a Hydrogen Sulfide assay from a Tedlar bag would be labeled as “EPA Method 16-Type” because Tedlar bags are not mentioned as one of the collection options in EPA Method 16.
- The acronym **MDL** represents the Minimum Detection Limit. Below this value the laboratory cannot determine the presence of the analyte of interest reliably.
- The acronym **LOQ** represents the Limit of Quantification. Below this value the laboratory cannot quantitate the analyte of interest within the criteria of the method.
- The acronym **ND** following a value indicates a non-detect or analytical result below the MDL.
- The letter **J** in the Qualifier or Flag column in the results indicates that the value is between the MDL and the LOQ. The laboratory can positively identify the analyte of interest as present, but the value should be considered an estimate.
- The letter **E** in the Qualifier or Flag column indicates an analytical result exceeding 100% of the highest calibration point. The associated value should be considered as an estimate.
- Sample results are presented ‘as measured’ for single injection methodologies, or an average value if multiple injections are made. If all injections are below the MDL, the sample is considered non-detect and the ND value is presented. If one, but not all, are below the MDL, the MDL value is used for any injections that are below the MDL. For example, if the MDL is 0.500 and LOQ is 1.00, and the instrument measures 0.355, 0.620, and 0.442 - the result reported is the average of 0.500, 0.620, and 0.500 - - - i.e. 0.540 with a J flag.
- When a spike recovery (Bag Spike, Collocated Spike Train, or liquid matrix spike) is being calculated, the native (unspiked) sample result is used in the calculations, as long as the value is above the MDL. If a sample is ND, then 0 is used as the native amount (not the MDL value).
- The acronym **DF** represents Dilution Factor. This number represents dilution of the sample during the preparation and/or analysis process. The analytical result taken from a laboratory instrument is multiplied by the DF to determine the final undiluted sample results.
- The addition of **MS** to the Sample ID represents a Matrix Spike. An aliquot of an actual sample is spiked with a known amount of analyte so that a percent recovery value can be determined. The MS analysis indicates what effect the sample matrix may have on the target analyte, i.e. whether or not anything in the sample matrix interferes with the analysis of the analyte(s).



# General Reporting Notes

(continued)

- The addition of **MSD** to the Sample ID represents a Matrix Spike Duplicate. Prepared in the same manner as a MS, the use of duplicate matrix spikes allows further confirmation of laboratory quality by showing the consistency of results gained by performing the same steps multiple times.
- The addition of **LD** to the Sample ID represents a Laboratory Duplicate. The analyst prepares an additional aliquot of sample for testing and the results of the duplicate analysis are compared to the initial result. The result should have a difference value of within 10% of the initial result (if the results of the original analysis are greater than the LOQ).
- The addition of **AD** to the Sample ID represents an Alternate Dilution. The analyst prepares an additional aliquot at a different dilution factor (usually double the initial factor). This analysis helps confirm that no additional compound is present and coeluting or sharing absorbance with the analyte of interest, as they would have a different response/absorbance than the analyte of interest.
- The Sample ID **LCS** represents a Laboratory Control Sample. Clean matrix, similar to the client sample matrix, prepared and analyzed by the laboratory using the same reagents, spiking standards and procedures used for the client samples. The LCS is used to assess the control of the laboratory's analytical system. Whenever spikes are prepared for our client projects, two spikes are retained as LCSs. The LCSs are labeled with the associated project number and kept in-house at the appropriate temperature conditions. When the project samples are received for analysis, the LCSs are analyzed to confirm that the analyte could be recovered from the media, separate from the samples which were used on the project and which may have been affected by source matrix, sample collection, and/or sample transport.
- **Significant Figures:** Where the reported value is much greater than unity (1.00) in the units expressed, the number is rounded to a whole number of units, rather than to 3 significant figures. For example, a value of 10,456.45 ug catch is rounded to 10,456 ug. There are five significant digits displayed, but no confidence should be placed on more than two significant digits. In the case of small numbers, generally 3 significant figures are presented, but still only 2 should be used with confidence. Many neat materials are only certified to 3 digits, and as the mathematically correct final result is always 1 digit less than all its pre-cursors - 2 significant figures are what are most defensible.
- **Manual Integration:** The data systems used for processing will flag manually integrated peaks with an "M". There are several reasons a peak may be manually integrated. These reasons will be identified by the following two letter designations on sample chromatograms, if provided in the report. The peak was *not integrated* by the software "NI", the peak was *integrated incorrectly* by the software "II" or the *wrong peak* was integrated by the software "WP". These codes will accompany the analyst's manual integration stamp placed next to the compound name on the chromatogram.





# Sample Custody



# Advanced Industrial Resources, Inc.

## Compliance Sample Custody Record

Client: GP  
Juno Toledo, OR  
 \_\_\_\_\_  
 \_\_\_\_\_

Analysis Desired:				Sample Condition
Method 105.01				

Sample ID	Date	Source	Description	Matrix						Comments
KR11456	1	7/12/2023	Carbon Bed Outlet	Test 1 Normal	M5	x				
KR11456	2	7/12/2023	Carbon Bed Outlet	Test 1 Duplicate	M5	x				
KR11456	3	7/12/2023	Carbon Bed Outlet	Test 2 Normal	M5	x				
KR11456	4	7/12/2023	Carbon Bed Outlet	Test 2 Low Spike	M5	x				
KR11456	5	7/12/2023	Carbon Bed Outlet	Test 3 Normal	M5	x				
KR11456	6	7/12/2023	Carbon Bed Outlet	Test 3 High Spike	M5	x				
KR11456	7	7/12/2023	Carbon Bed Outlet	Train Spike	M6	x				
KR11456	8	7/12/2023	Carbon Bed Outlet	Filed Spike Low	M7	x				
KR11456	9	7/12/2023	Carbon Bed Outlet	Filed Spike High	M8	x				
KR11456	10	7/12/2023	Carbon Bed Outlet	BHA Blank	M9	x				

Relinquished By/Sign:	Date/Time	Received By / Sign:	Relinquished By / Sign:	Date/Time	Received By / Sign:
		<i>[Signature]</i>			

<p><b>Field Team Members:</b> _____ DJK <i>07-14-23</i></p> <p><b>AIR Field Supervisor:</b> _____ Dan Kirk</p> <p><b>Field Supervisor Sign:</b> _____</p> <p><b>AIR Contact Name:</b> _____ Derek Stephens</p> <p><b>AIR Contact Number:</b> _____ (404) 843-2100</p>	<p><b>Analyses To Be Performed By:</b> _____ Enthalpy</p> <p><i>0930</i> <i>mmmm</i> <i>07-14-23</i></p>
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*4.6°C Raytek 2  
 good condition  
 Amm 3 07-14-23*

# Raw Data

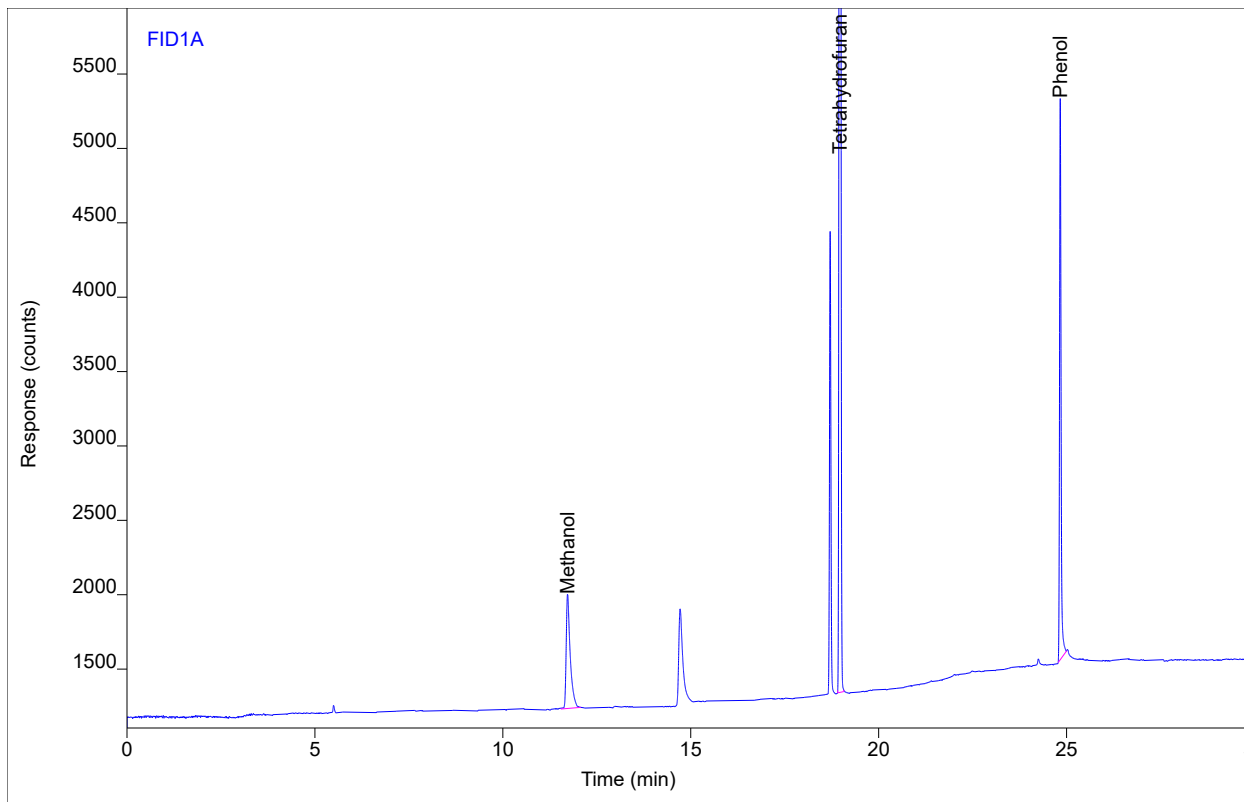


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #4  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 010F0101.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 2:25 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type  
 Vial Number 10  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



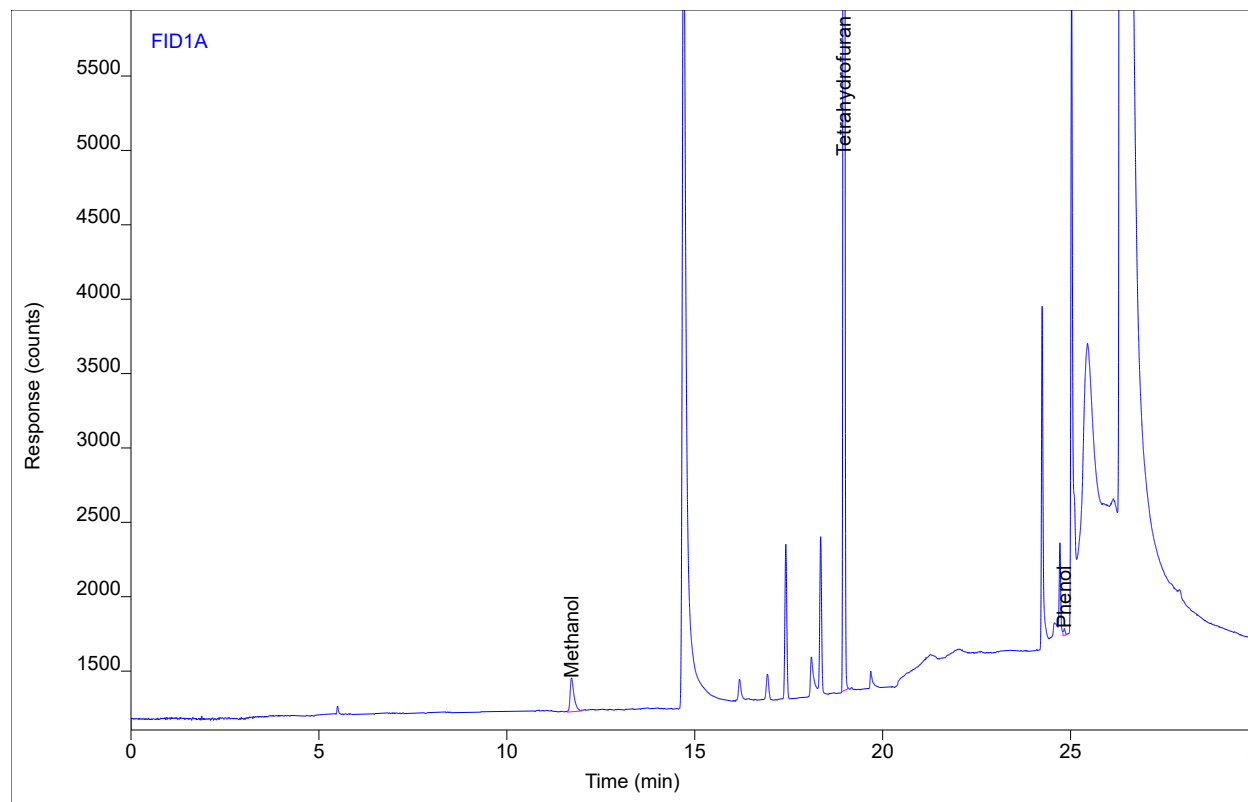
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.72	5741.96	771.254	22.9728	1	22.9728	ug/mL
Tetrahydrofuran	I BB	18.97	52837.6	20364.3	149.190			ug/mL
Phenol	BB	24.83	10453.0	3770.91	24.6150	1	24.6150	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R1.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 001F0201.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 3:47 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type  
 Vial Number 1  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



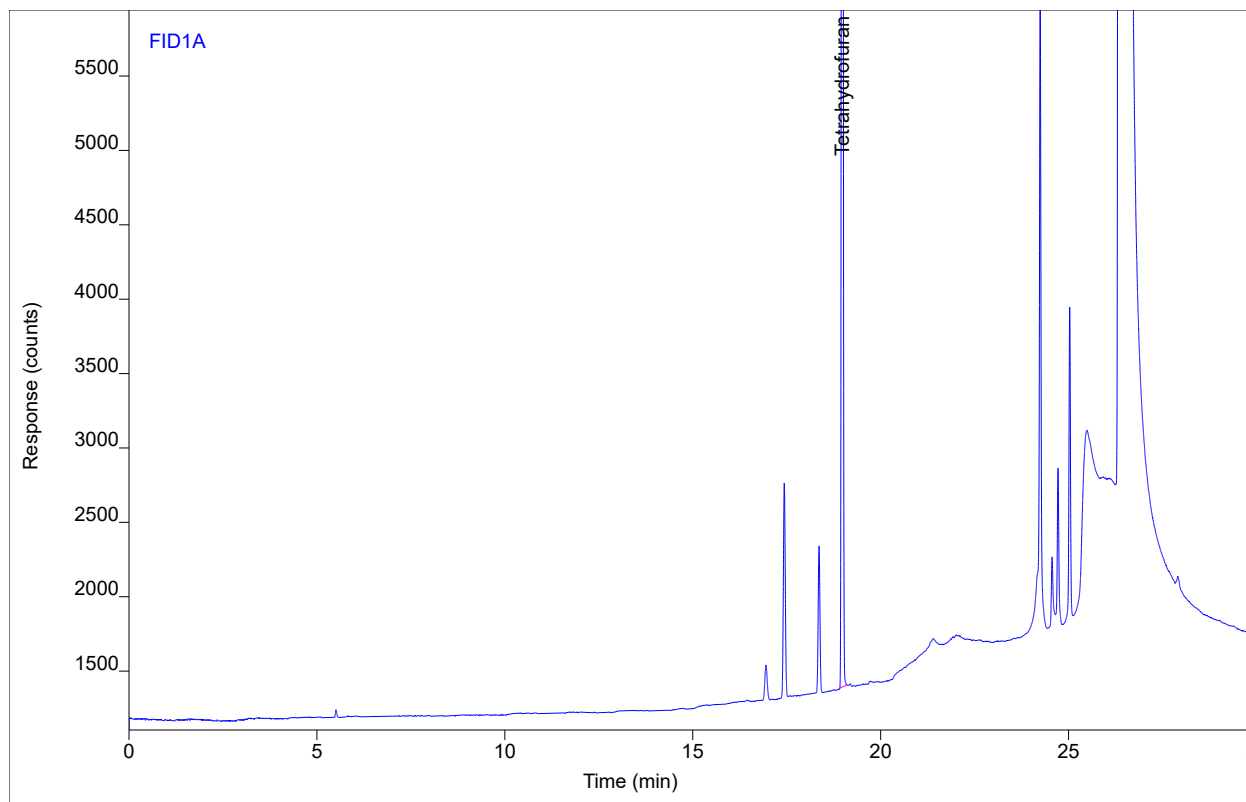
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Methanol	VB	11.72	1662.62	230.041	6.08398	1	6.08398	ug/mL
Tetrahydrofuran	I BB	18.97	57769.9	22570.9	149.190			ug/mL
Phenol	VV	24.83	143.766	48.5387	0.30964	1	0.30964	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R1-DUP.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 002F0301.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 4:23 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 2  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



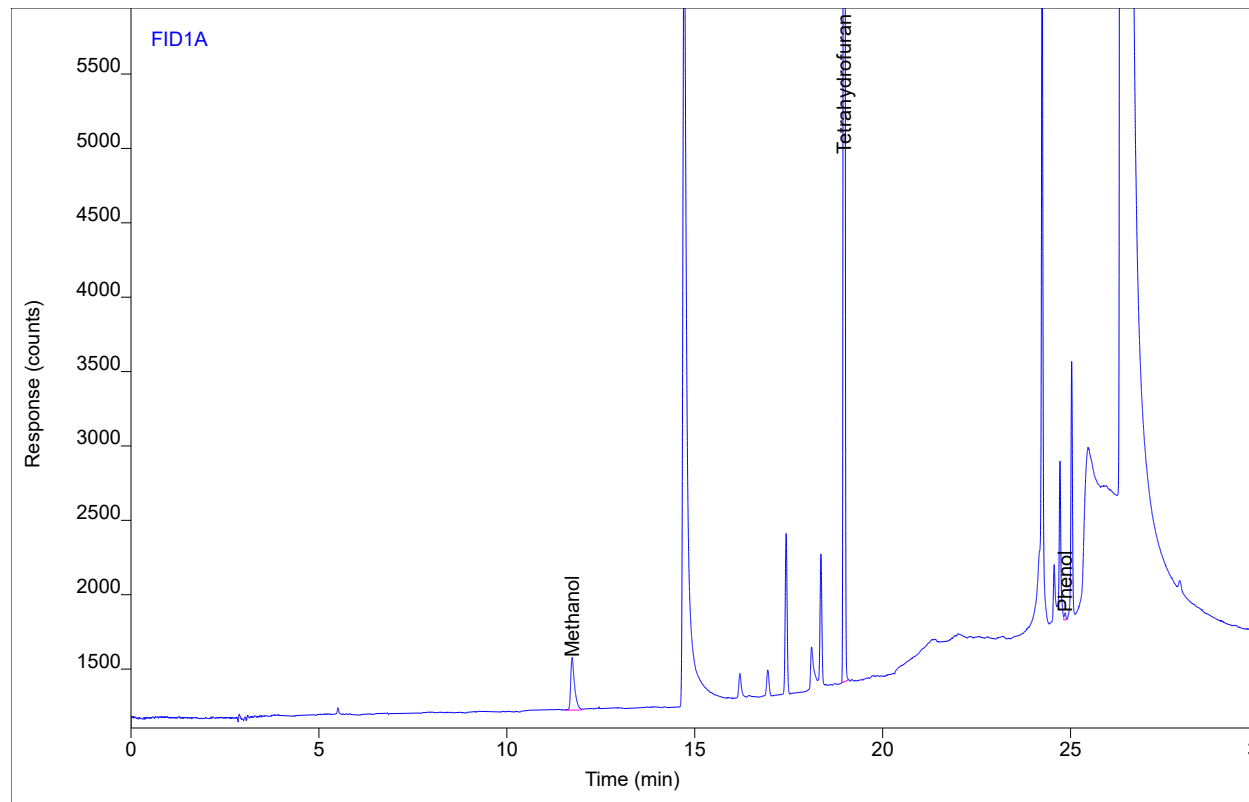
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol		(11.74)				1		ug/mL
Tetrahydrofuran	I BB	18.98	54734.1	21330.7	149.190			ug/mL
Phenol		(24.86)				1		ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R2.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 003F0401.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 4:58 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 3  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



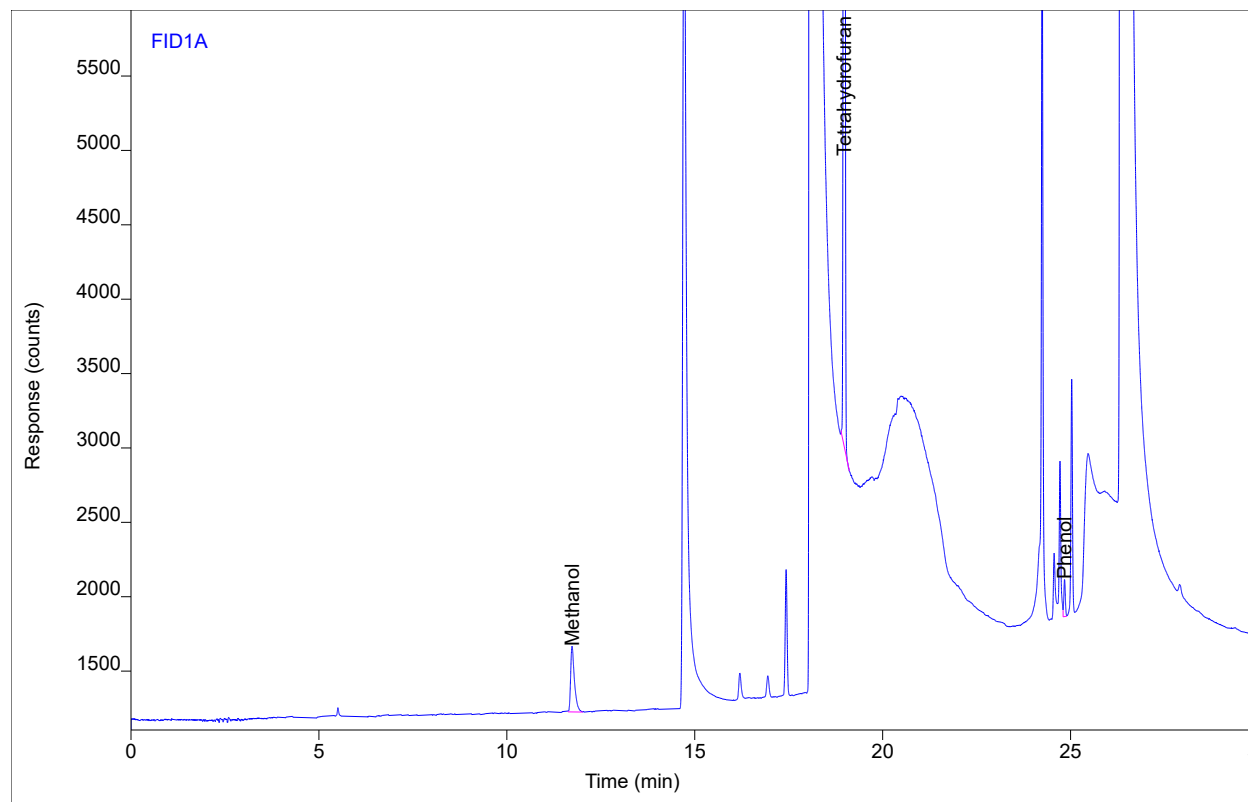
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.74	2533.74	352.876	9.85870	1	9.85870	ug/mL
Tetrahydrofuran	I BB	18.98	54329.8	21159.7	149.190			ug/mL
Phenol	VV	24.86	133.503	50.0549	0.30574	1	0.30574	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R2-L-SPK.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 004F0501.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 5:34 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 4  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BV	11.74	3111.19	442.125	12.1495	1	12.1495	ug/mL
Tetrahydrofuran	l BB	18.98	54133.6	21310.1	149.190			ug/mL
Phenol	VV	24.84	694.468	251.438	1.59621	1	1.59621	ug/mL

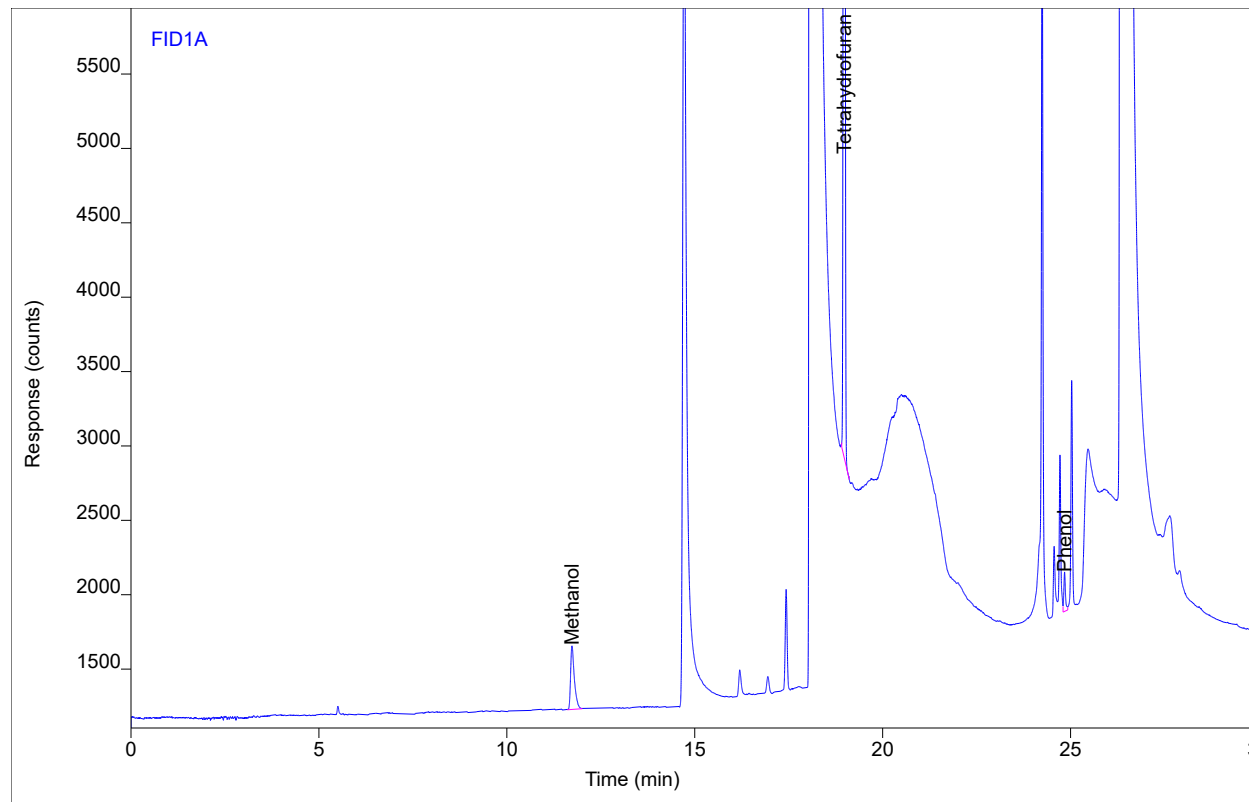


# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R2-L-SPK-LD.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 005F0601.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 6:10 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 5  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



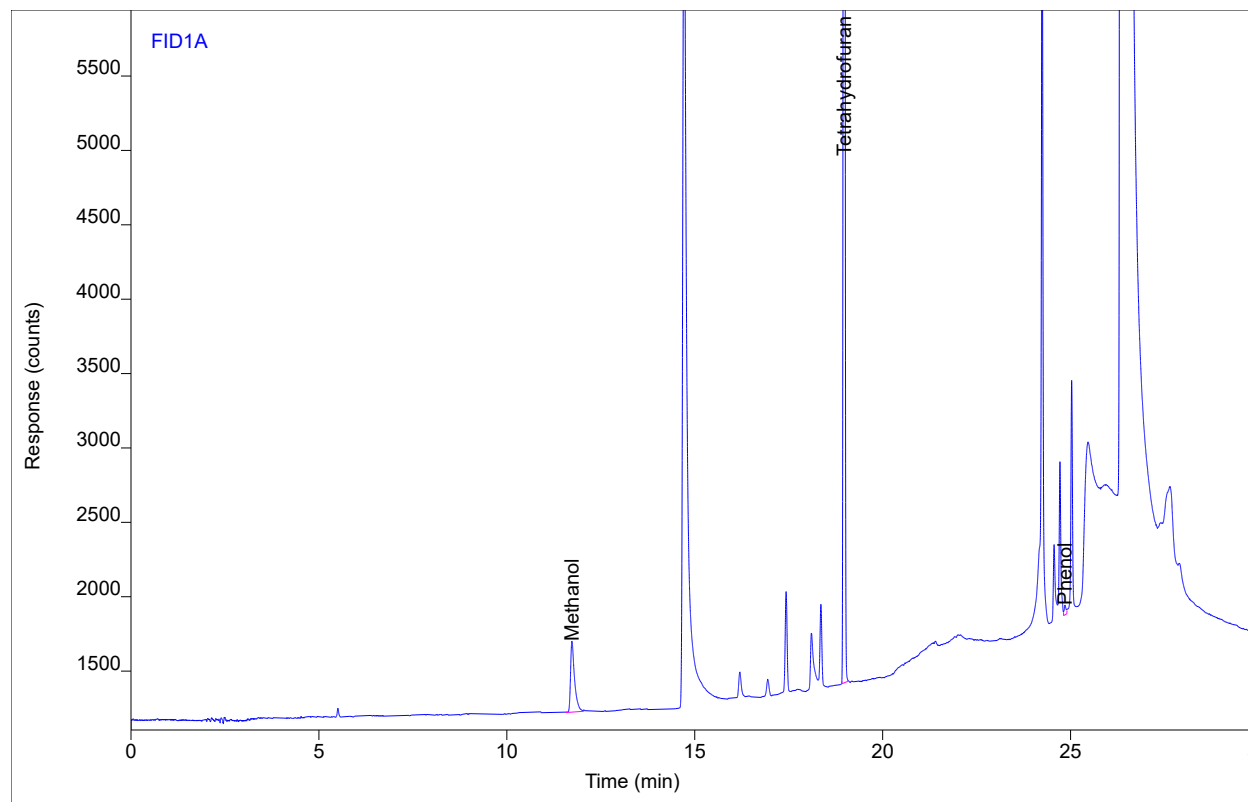
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.73	2986.35	430.231	11.4701	1	11.4701	ug/mL
Tetrahydrofuran	I BB	18.98	55038.7	21674.5	149.190			ug/mL
Phenol	VV	24.84	797.270	265.926	1.80235	1	1.80235	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R3.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 006F0701.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 6:45 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 6  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



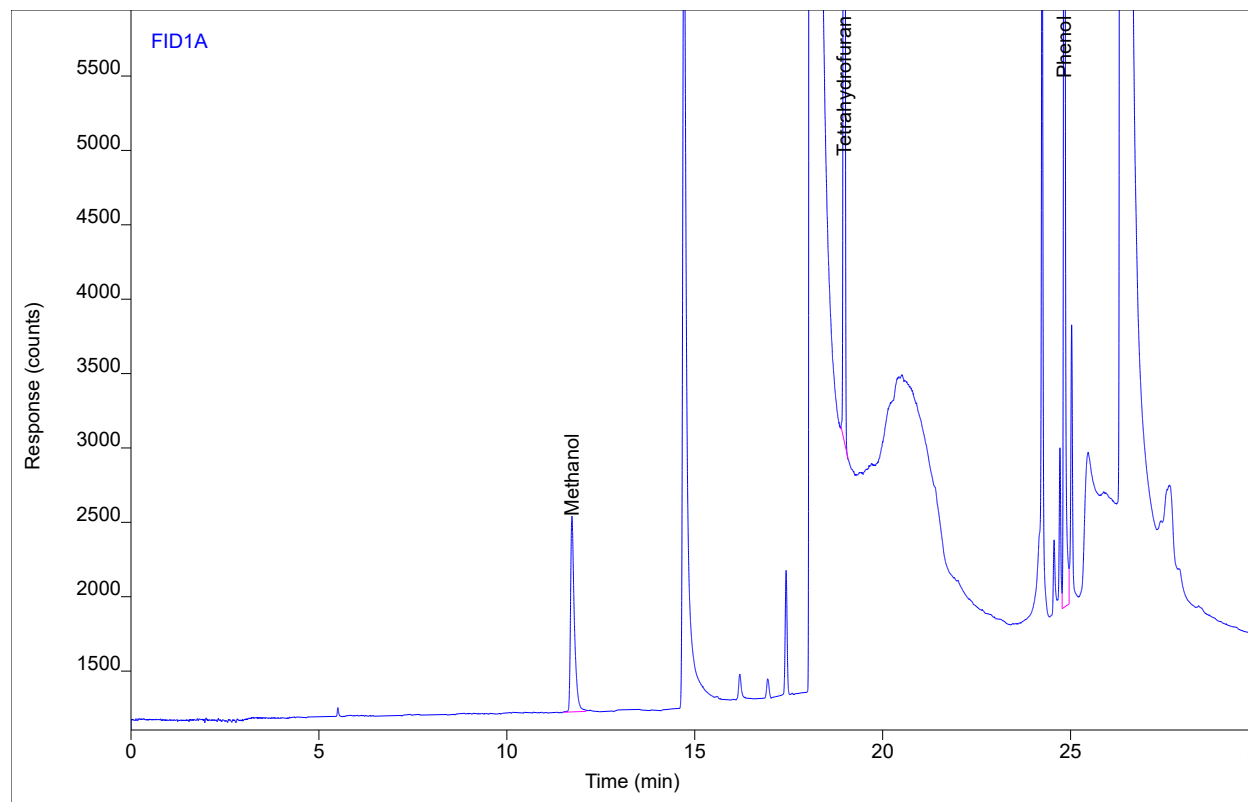
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BV	11.73	3533.14	478.652	13.8668	1	13.8668	ug/mL
Tetrahydrofuran	I BB	18.97	53861.9	20974.0	149.190			ug/mL
Phenol	VV	24.85	225.267	67.5792	0.52038	1	0.52038	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R3-H-SPK.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 007F0801.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 7:21 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 7  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



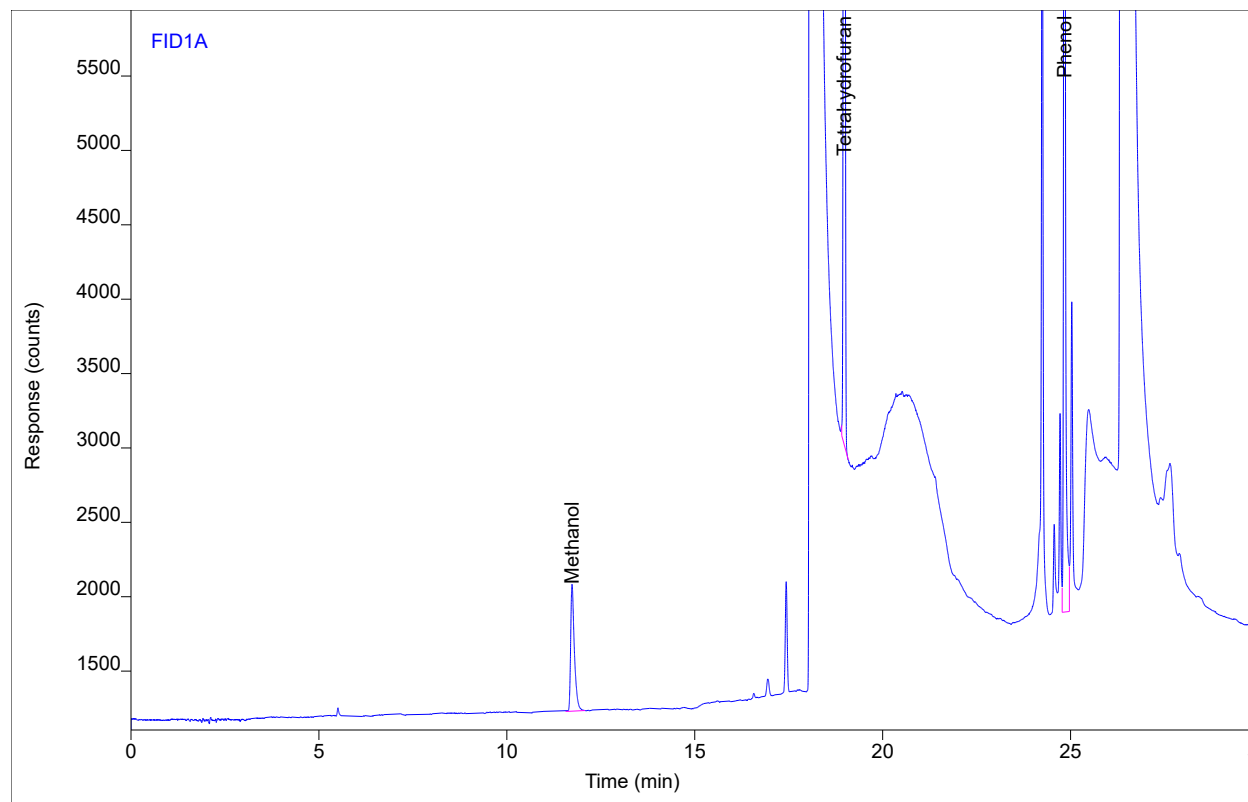
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.73	9318.96	1316.00	36.6038	1	36.6038	ug/mL
Tetrahydrofuran	I BB	18.98	53819.3	21264.0	149.190			ug/mL
Phenol	VV	24.83	32285.4	11524.6	74.6399	1	74.6399	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.TS.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 008F0901.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 7:57 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 8  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



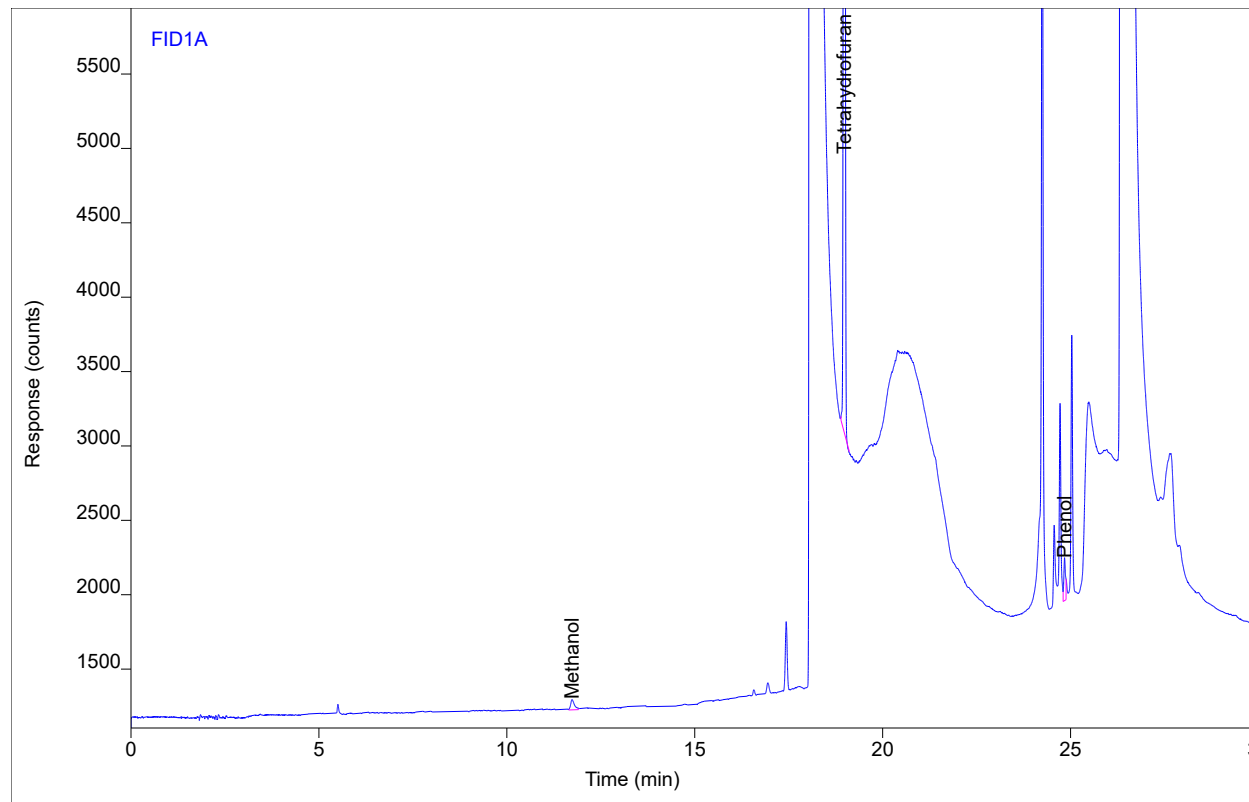
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.74	5866.22	857.295	22.5168	1	22.5168	ug/mL
Tetrahydrofuran	I BB	18.98	55074.2	21665.4	149.190			ug/mL
Phenol	VV	24.84	33203.6	11415.8	75.0136	1	75.0136	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.F-L-SPK.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 009F1001.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 8:33 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 9  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VV	11.73	486.655	69.9263	1.93778	1	1.93778	ug/mL
Tetrahydrofuran	I BB	18.98	53090.2	20972.2	149.190			ug/mL
Phenol	MF	24.84	866.109	285.959	2.02984	1	2.02984	ug/mL

### Analyst Peak Integration Comments

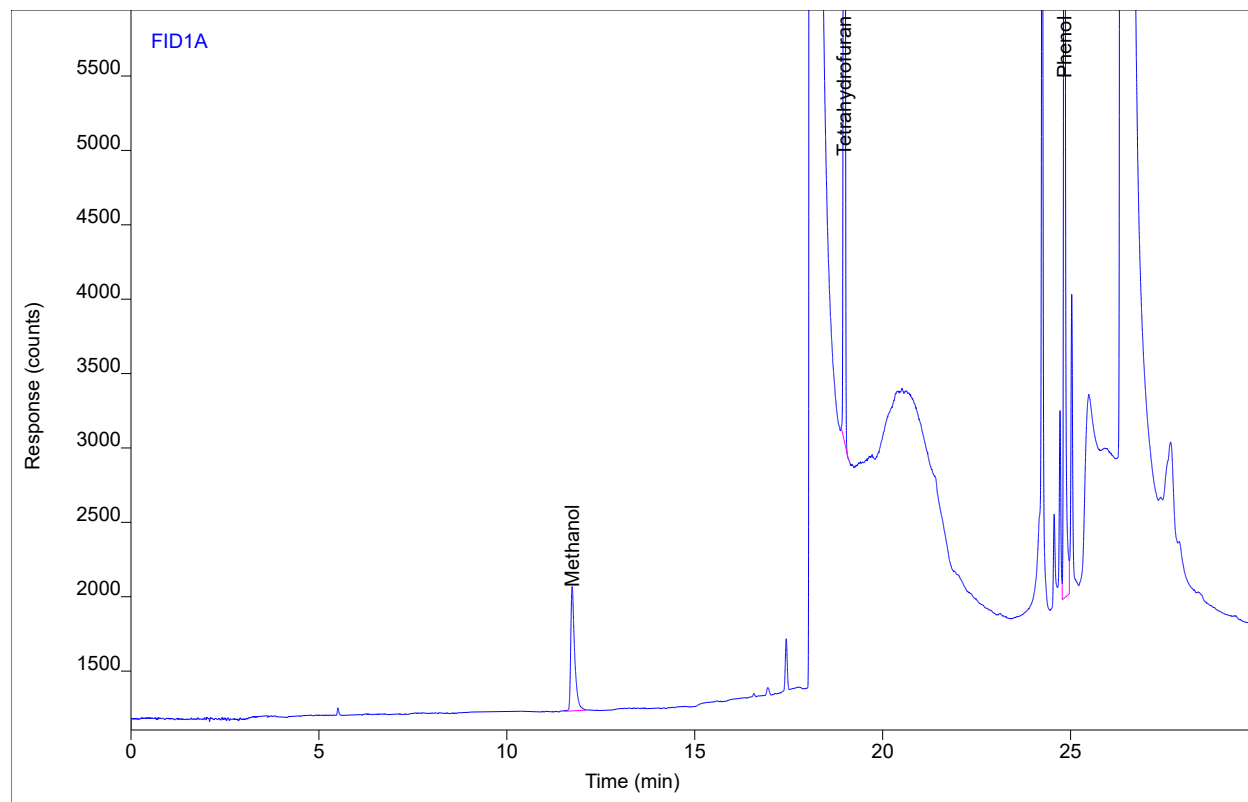
13:58:52 07/26/23 Remington Heathcoat ii

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.F-H-SPK.BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 011F1101.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 9:09 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 11  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



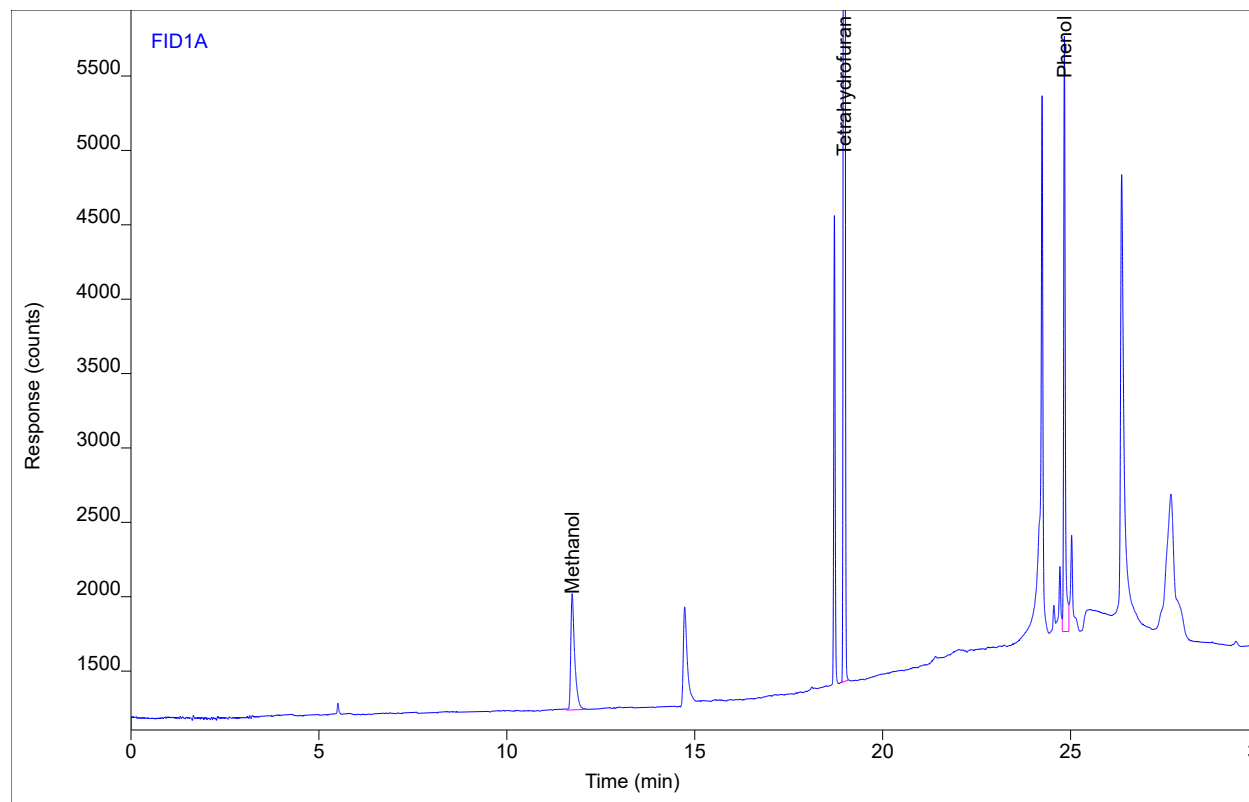
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BV	11.74	6051.69	835.597	22.5884	1	22.5884	ug/mL
Tetrahydrofuran	I BB	18.98	56635.4	22344.2	149.190			ug/mL
Phenol	VV	24.84	32219.6	11399.1	70.7840	1	70.7840	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #4  
Sequence Name FESTER0836A ver.7  
Inj Data File 010F1301.D  
File Location GC/2023/Fester/Quarter 3  
Injection Date 7/18/2023 10:21 PM  
File Modified 7/26/2023 2:09 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number 10  
Injection Volume 1  
Injection 1 of 1  
Acquisition Method FESTER0258.M  
Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
Method Modified 7/19/2023 10:01 AM  
Printed 7/26/2023 3:40 PM



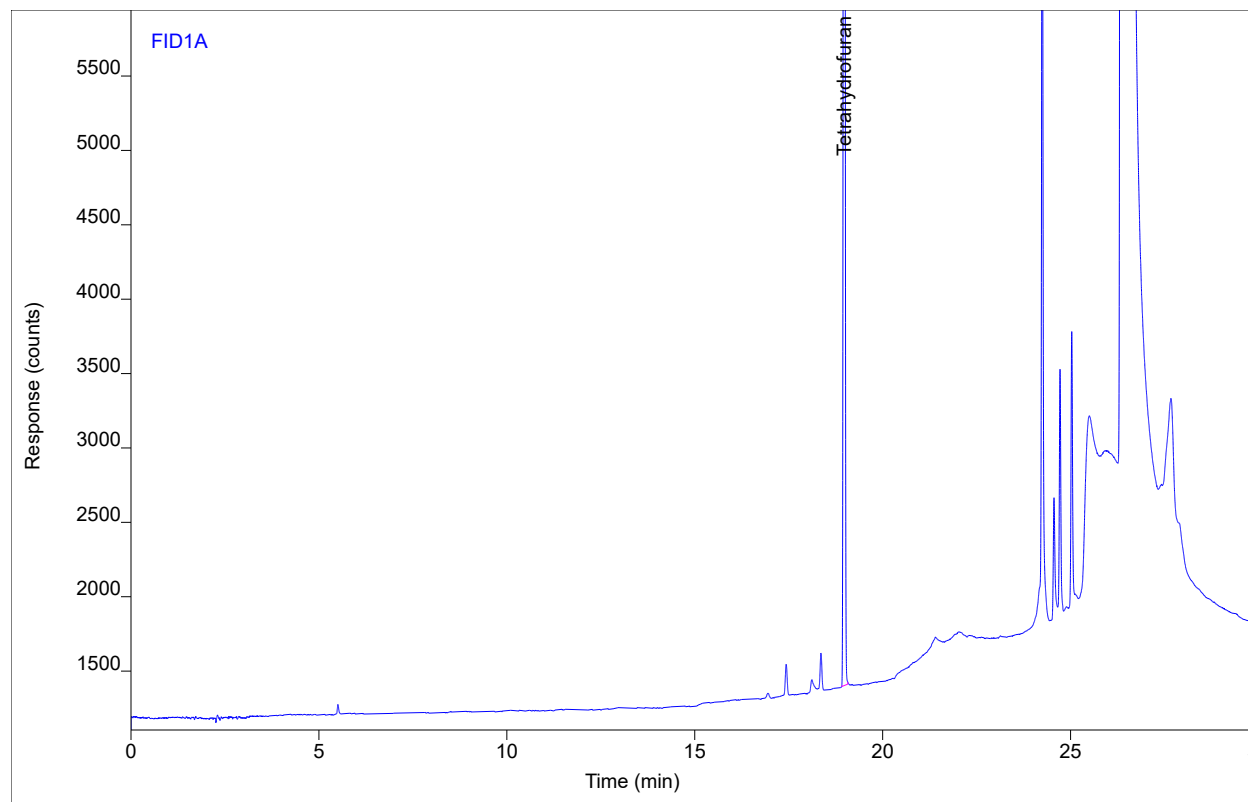
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VB	11.74	5660.89	782.540	22.6671	1	22.6671	ug/mL
Tetrahydrofuran	I BB	18.98	52794.0	20502.1	149.190			ug/mL
Phenol	VV	24.84	11698.8	3995.01	27.5716	1	27.5716	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcprep5570 #MB-BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 013F1401.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 10:57 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 13  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol		(11.74)				1		ug/mL
Tetrahydrofuran	I BB	18.98	55273.1	21626.8	149.190			ug/mL
Phenol		(24.86)				1		ug/mL

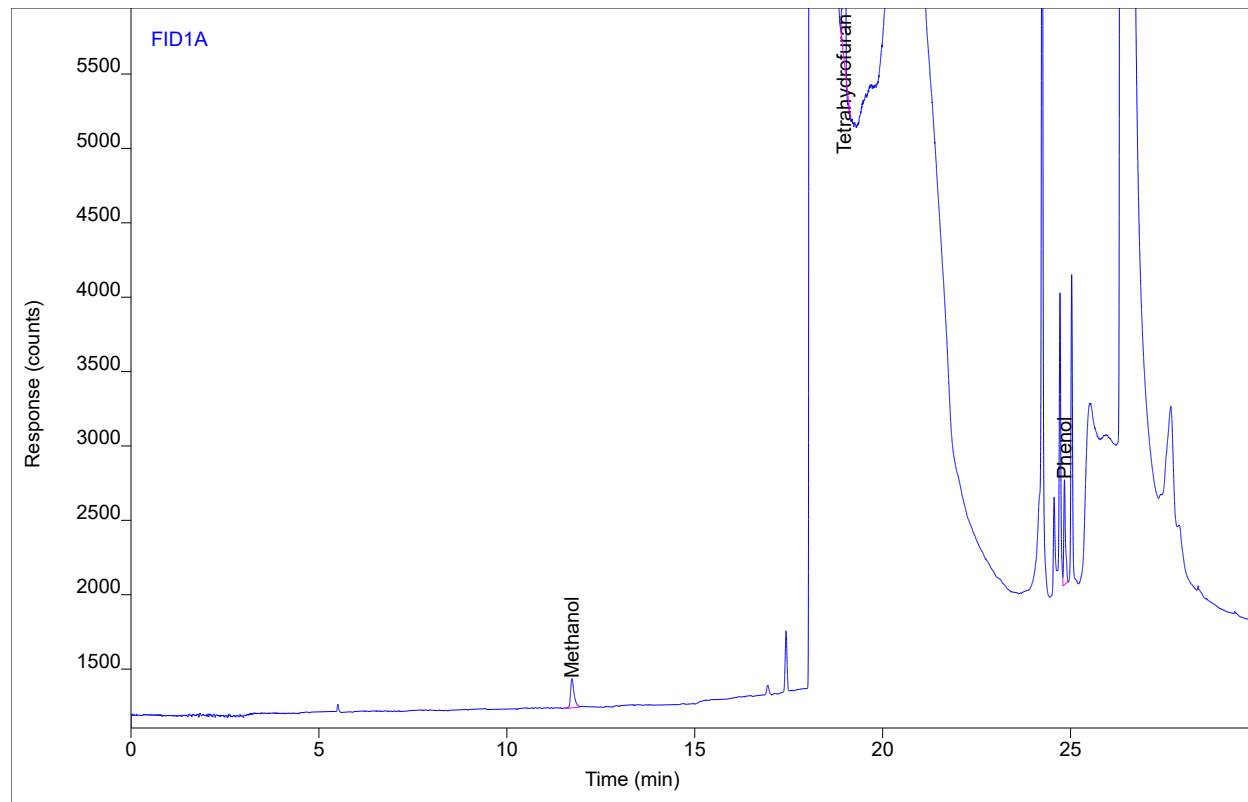


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcprep5570 #LCS-L-BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 014F1501.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/18/2023 11:33 PM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 14  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VV	11.73	1296.53	196.489	5.24125	1	5.24125	ug/mL
Tetrahydrofuran	I BB	18.98	52293.2	20558.2	149.190			ug/mL
Phenol	FM	24.84	2209.82	712.517	5.25793	1	5.25793	ug/mL

### Analyst Peak Integration Comments

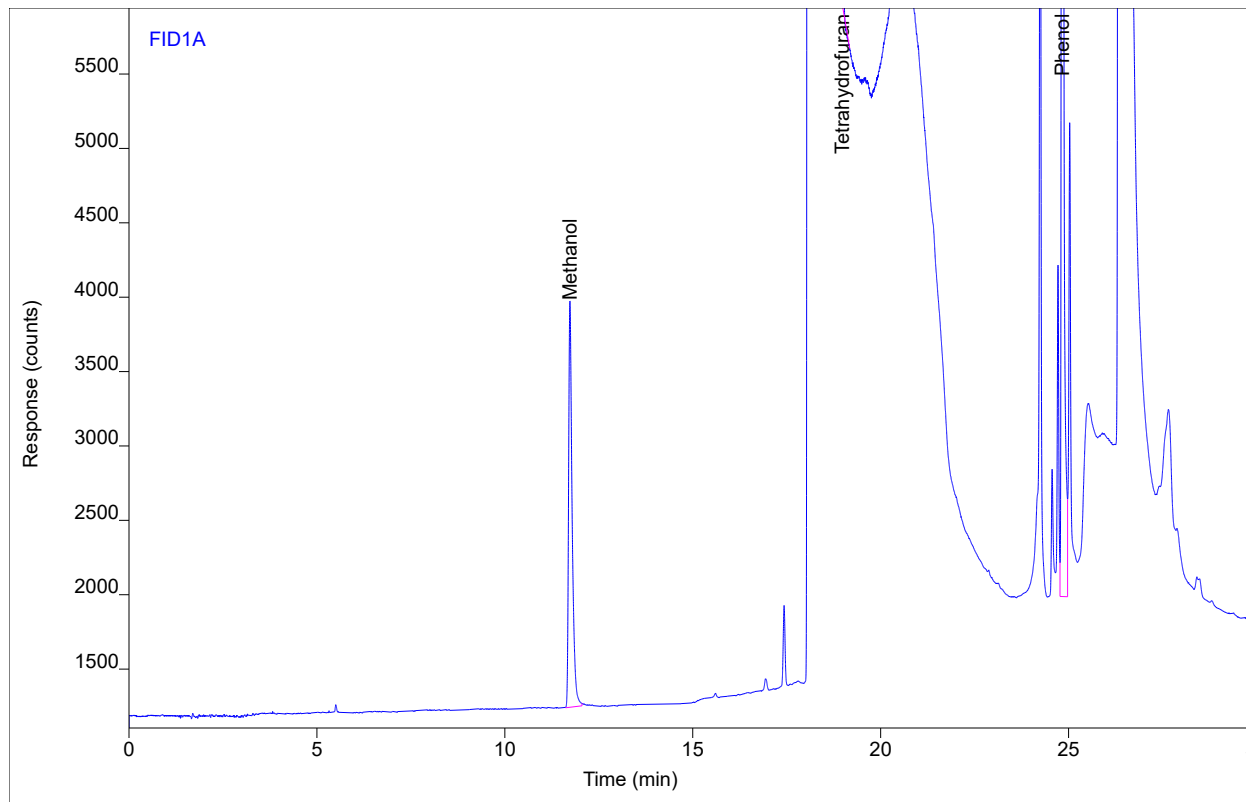
11:26:19 07/19/23 Remington Heathcoat ii

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcprep5570 #LCS-H-BHA  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 015F1601.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/19/2023 12:09 AM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 15  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



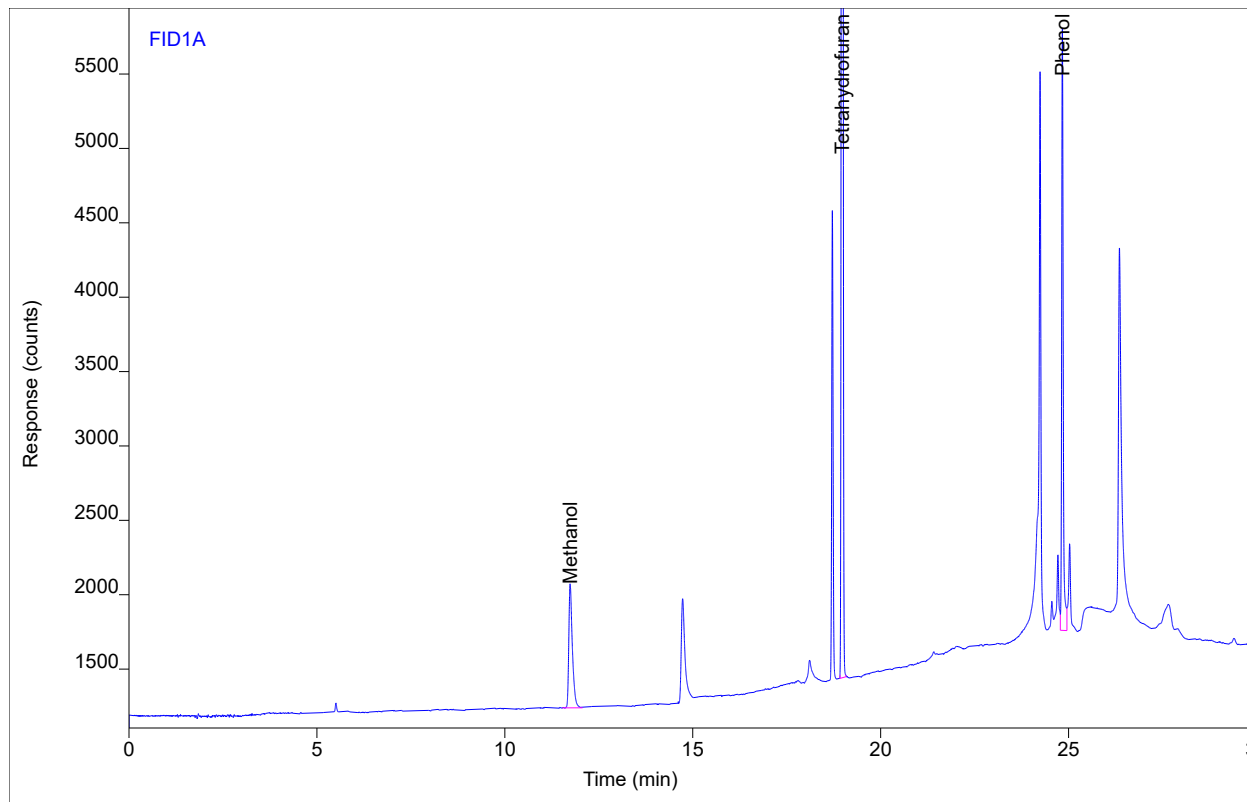
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BV	11.73	17999.6	2733.63	71.5369	1	71.5369	ug/mL
Tetrahydrofuran	l BB	18.98	53190.0	20770.6	149.190			ug/mL
Phenol	VV	24.84	98008.5	34610.3	229.265	1	229.265	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #4  
 Sequence Name FESTER0836A ver.7  
 Inj Data File 010F1701.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/19/2023 12:45 AM  
 File Modified 7/26/2023 2:09 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type  
 Vial Number 10  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/19/2023 10:01 AM  
 Printed 7/26/2023 3:40 PM



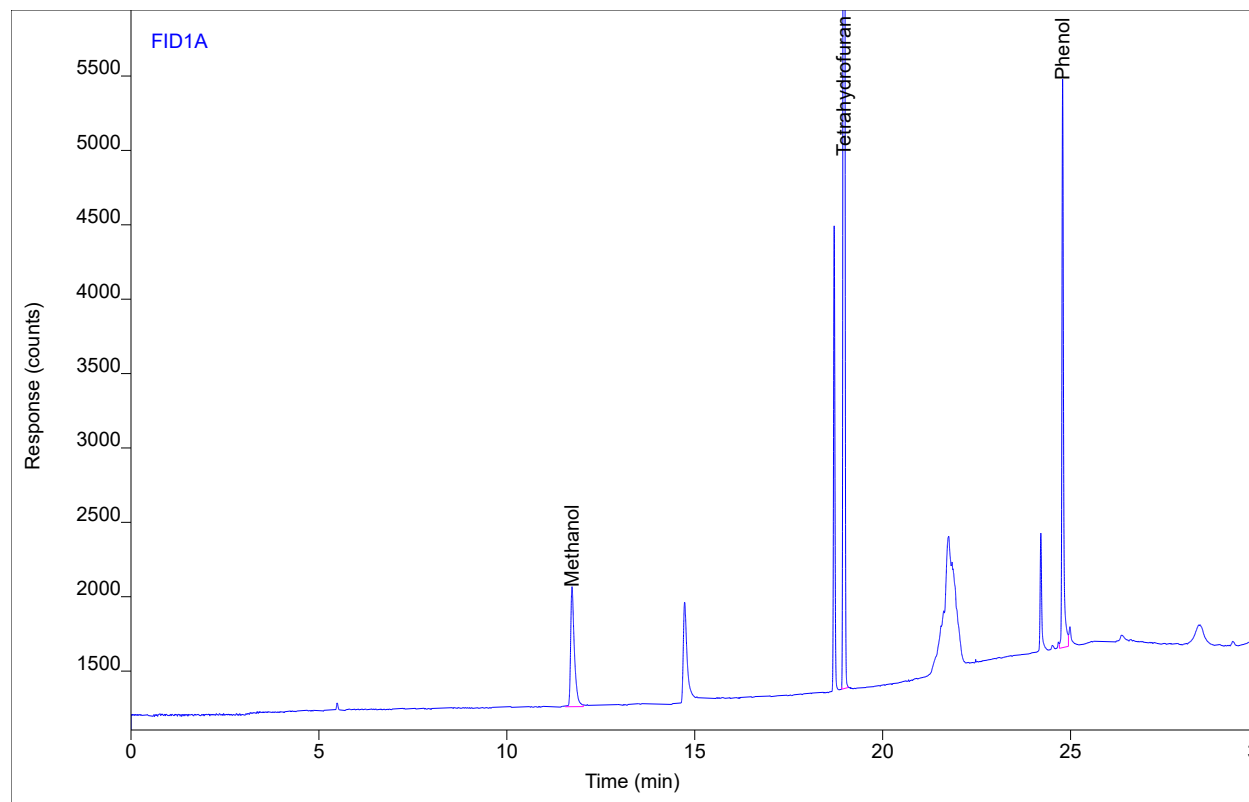
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BV	11.74	5507.70	834.015	22.1294	1	22.1294	ug/mL
Tetrahydrofuran	l BB	18.98	52613.4	20666.8	149.190			ug/mL
Phenol	VV	24.84	11643.8	4042.38	27.5361	1	27.5361	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #4  
Sequence Name FESTER0842 ver.3  
Inj Data File 010F0101.D  
File Location GC/2023/Fester/Quarter 3  
Injection Date 7/26/2023 8:25 AM  
File Modified 7/26/2023 2:12 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number 10  
Injection Volume 1  
Injection 1 of 1  
Acquisition Method FESTER0258.M  
Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
Method Modified 7/26/2023 2:11 PM  
Printed 7/26/2023 3:40 PM



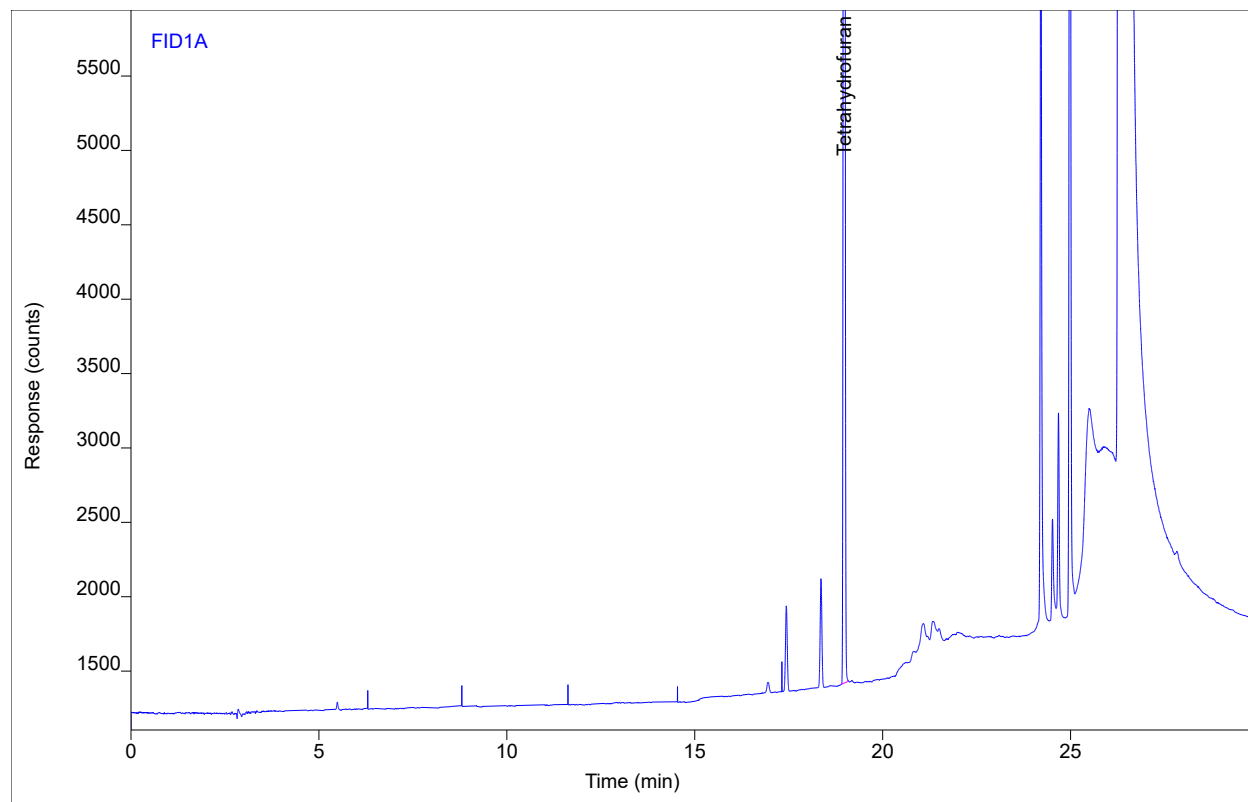
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VB	11.74	5604.43	807.275	22.5995	1	22.5995	ug/mL
Tetrahydrofuran	I BB	18.97	52424.0	20666.1	149.190			ug/mL
Phenol	VV	24.79	11174.2	3812.86	26.5209	1	26.5209	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.BLK.BHA  
 Sequence Name FESTER0842 ver.3  
 Inj Data File 097F0401.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/26/2023 10:12 AM  
 File Modified 7/26/2023 2:12 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Sample  
 Vial Number 97  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/26/2023 2:11 PM  
 Printed 7/26/2023 3:40 PM



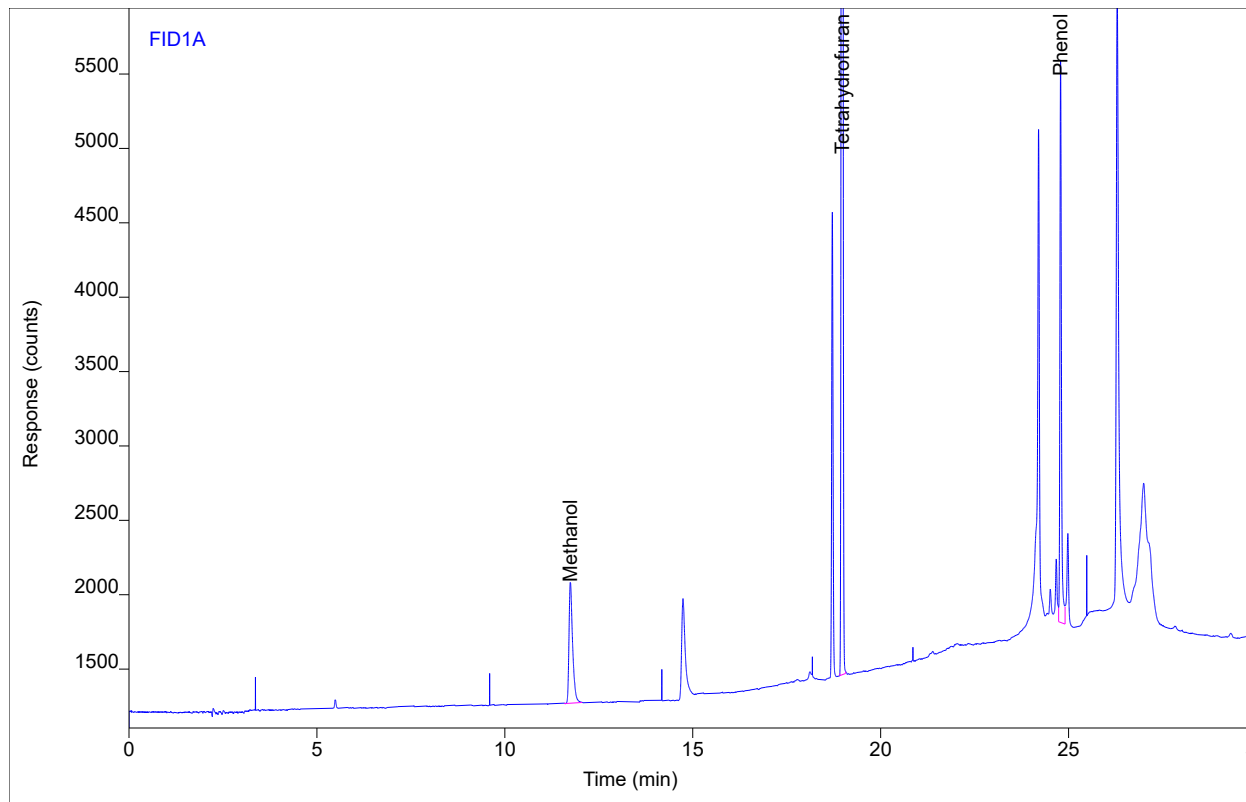
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol		(11.74)				1		ug/mL
Tetrahydrofuran	I BB	18.98	56315.8	22119.7	149.190			ug/mL
Phenol		(24.86)				1		ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #4  
 Sequence Name FESTER0842 ver.3  
 Inj Data File 010F0801.D  
 File Location GC/2023/Fester/Quarter 3  
 Injection Date 7/26/2023 12:34 PM  
 File Modified 7/26/2023 2:12 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type  
 Vial Number 10  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 7/26/2023 2:11 PM  
 Printed 7/26/2023 3:40 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.74	5432.44	816.672	21.9151	1	21.9151	ug/mL
Tetrahydrofuran	I BB	18.97	52401.9	20549.2	149.190			ug/mL
Phenol	VV	24.79	10738.9	3773.09	25.4986	1	25.4986	ug/mL

=====  
 Calibration Table  
 =====

Calib. Data Modified : Monday, June 26, 2023 12:23:39 PM

Rel. Reference Window : 0.000 %  
 Abs. Reference Window : 0.400 min  
 Rel. Non-ref. Window : 0.000 %  
 Abs. Non-ref. Window : 0.150 min  
 Uncalibrated Peaks : not reported  
 Partial Calibration : Yes, identified peaks are recalibrated  
 Correct All Ret. Times: No, only for identified peaks

Curve Type : Average Response/Amount  
 Origin : Ignored  
 Weight : Equal

Recalibration Settings:  
 Average Response : Average all calibrations  
 Average Retention Time: Floating Average New 75%

Calibration Report Options :  
 Printout of recalibrations within a sequence:  
     Calibration Table after Recalibration  
     Normal Report after Recalibration  
 If the sequence is done with bracketing:  
     Results of first cycle (ending previous bracket)

Sample ISTD Information:

ISTD #	ISTD Amount [ug/mL]	Name
1	149.19000	Tetrahydrofuran

Signal 1: FID2 B,  
 Signal 2: FID1 A,

RetTime [min]	Lvl Sig	Amount [ug/mL]	Area	Amt/Area	Ref Grp	Name
11.735	2 1	3.79528e-1	110.87212	3.42311e-3	1	Methanol
	2	9.48252e-1	254.05077	3.73253e-3		
	3	4.72239	1246.11243	3.78970e-3		
	4	23.15122	5708.50684	4.05556e-3		
	5	45.20000	1.15769e4	3.90433e-3		
	6	105.46667	2.65565e4	3.97141e-3		
	7	949.20000	2.32222e5	4.08746e-3		
14.747	2 1	3.76676e-1	82.70997	4.55418e-3	1	Ethanol
	2	9.41125e-1	204.73123	4.59688e-3		
	3	4.68690	1143.99426	4.09696e-3		
	4	22.97722	5178.28320	4.43723e-3		
	5	44.86029	1.07985e4	4.15431e-3		
	6	104.67400	2.58476e4	4.04966e-3		
	7	942.06600	2.54901e5	3.69582e-3		

RetTime [min]	Lvl Sig	Amount [ug/mL]	Area	Amt/Area	Ref	Grp Name
18.731	2 1	3.85110e-1	138.62234	2.77812e-3	1	2-Butanone
	2	9.62198e-1	346.38651	2.77782e-3		
	3	4.79184	1763.44043	2.71732e-3		
	4	23.49170	8539.21289	2.75104e-3		
	5	45.86475	1.72049e4	2.66580e-3		
	6	107.01776	3.93543e4	2.71934e-3		
	7	963.15984	3.36939e5	2.85856e-3		
18.985	2 1	149.19000	5.60711e4	2.66073e-3	I1	Tetrahydrofuran
	2	149.19000	5.56343e4	2.68162e-3		
	3	149.19000	5.46498e4	2.72993e-3		
	4	149.19000	5.44407e4	2.74041e-3		
	5	149.19000	5.55217e4	2.68706e-3		
	6	149.19000	5.42298e4	2.75107e-3		
	7	149.19000	5.46873e4	2.72806e-3		
24.859	2 1	4.18613e-1	166.87405	2.50856e-3	1	Phenol
	2	1.04591	420.31168	2.48841e-3		
	3	5.20872	2216.61182	2.34986e-3		
	4	25.53541	1.12283e4	2.27420e-3		
	5	49.85486	2.27546e4	2.19098e-3		
	6	116.32800	5.66135e4	2.05477e-3		
	7	1046.95200	5.07730e5	2.06202e-3		

More compound-specific settings:

Compound: Methanol

Time Window : From 11.518 min To 11.960 min

Compound: Ethanol

Time Window : From 14.542 min To 14.978 min

Compound: 2-Butanone

Time Window : From 18.611 min To 18.857 min

Compound: Tetrahydrofuran

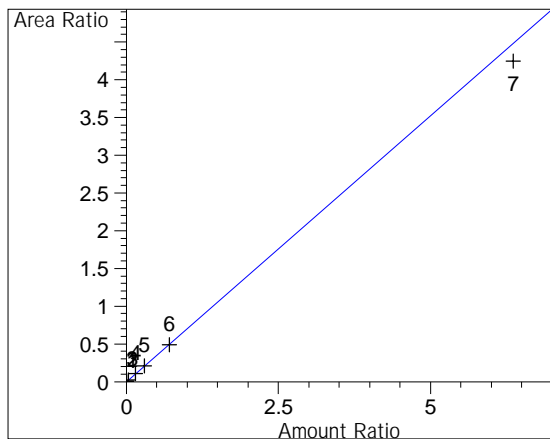
Time Window : From 18.872 min To 19.101 min

=====  
Peak Sum Table  
=====

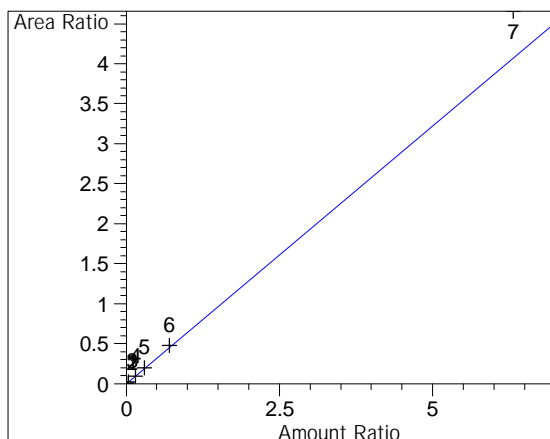
\*\*\*No Entries in table\*\*\*  
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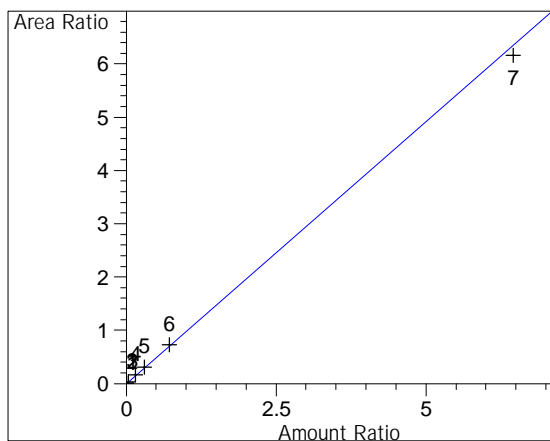
=====  
 Calibration Curves  
 =====



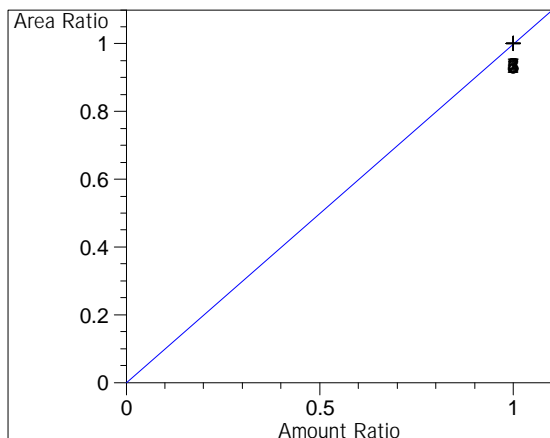
Methanol at exp. RT: 11.735  
 FID1 A,  
 Correlation: 0.99999  
 Residual Std. Dev.: 0.10915  
 Formula:  $y = mx$   
 m: 7.05738e-1  
 x: Amount  
 y: Area



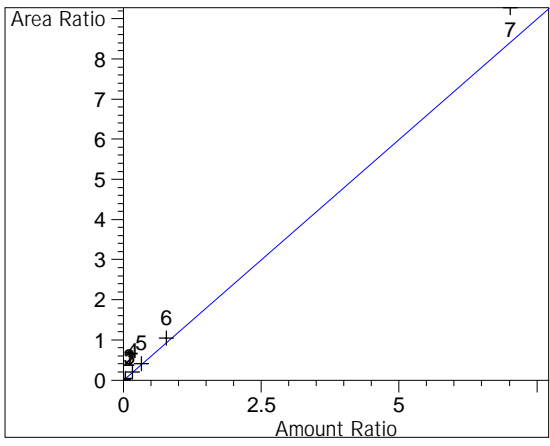
Ethanol at exp. RT: 14.747  
 FID1 A,  
 Correlation: 0.99996  
 Residual Std. Dev.: 0.26294  
 Formula:  $y = mx$   
 m: 6.45116e-1  
 x: Amount  
 y: Area



2-Butanone at exp. RT: 18.731  
 FID1 A,  
 Correlation: 0.99998  
 Residual Std. Dev.: 0.09014  
 Formula:  $y = mx$   
 m: 9.85411e-1  
 x: Amount  
 y: Area



Tetrahydrofuran at exp. RT: 18.985  
 FID1 A,  
 Correlation: 1.00000  
 Residual Std. Dev.: 0.00000  
 Formula:  $y = mx$   
 m: 1.00000  
 x: Amount  
 y: Area



Phenol at exp. RT: 24.859  
FID1 A,  
Correlation: 0.99999  
Residual Std. Dev.: 0.39207  
Formula:  $y = mx$   
m: 1.19905  
x: Amount  
y: Area

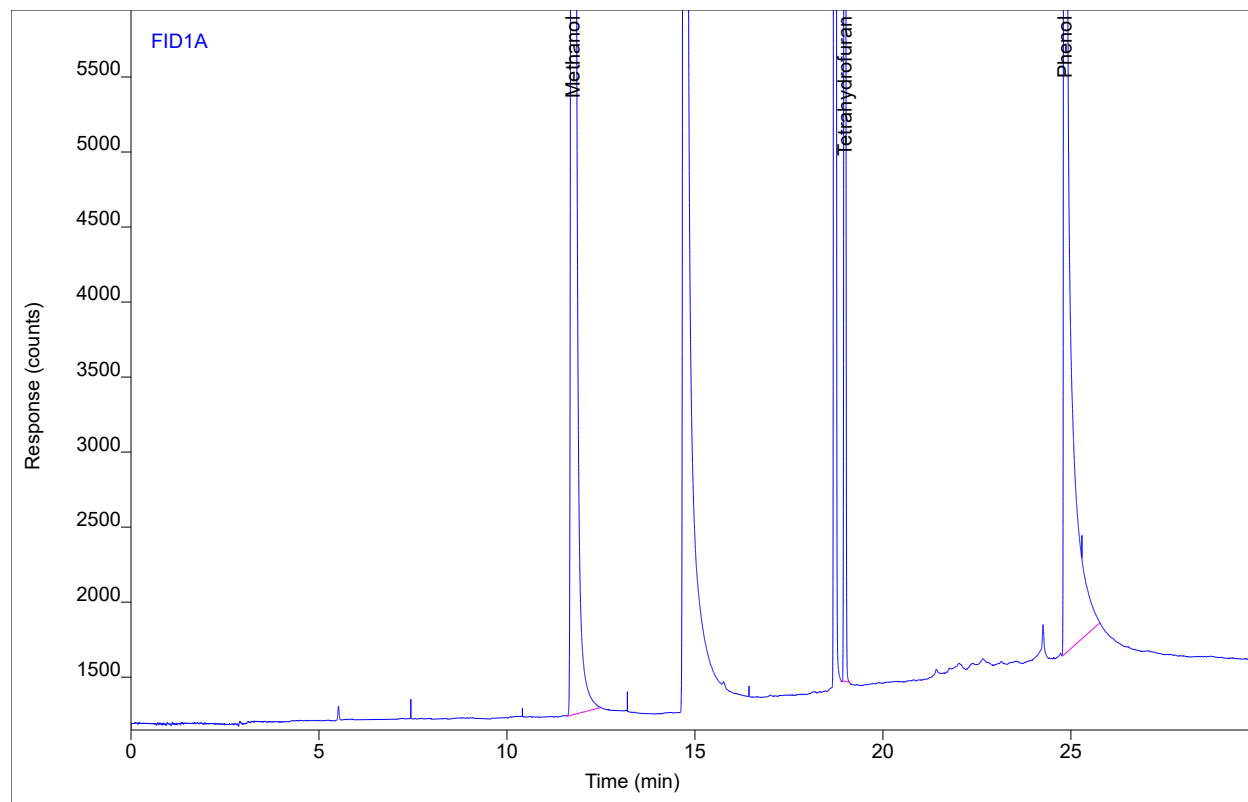
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# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #7  
Sequence Name FESTER0821 1 ver.1  
Inj Data File 034F0601.D  
File Location GC/2023/Fester/Quarter 2  
Injection Date 6/23/2023 1:28 PM  
File Modified 6/26/2023 12:52 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number  
Injection Volume  
Injection  
Acquisition Method  
Analysis Method  
Method Modified  
Printed  
Calibration  
Vial 34  
1  
1 of 1  
FESTER0258.M  
FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
6/26/2023 12:49 PM  
6/26/2023 2:04 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	MM	11.75	232222	39819.2	897.664	1	897.664	ug/mL
Tetrahydrofuran	BB	18.99	54687.3	21452.1	149.190	1	149.190	ug/mL
Phenol	MM	24.84	507730	179279	1155.18	1	1155.18	ug/mL

## Analyst Peak Integration Comments

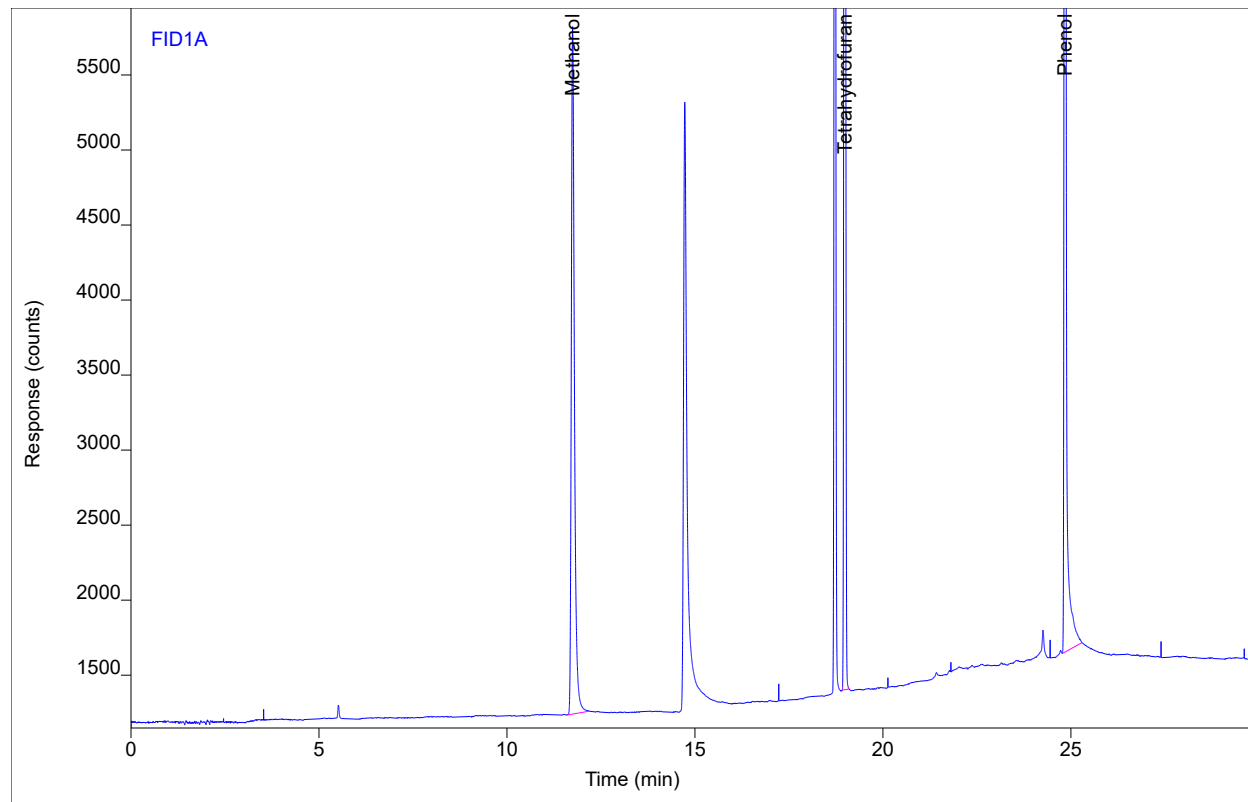
07:29:20 06/26/23 Remington Heathcoat ii

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #6  
 Sequence Name FESTER0821 1 ver.1  
 Inj Data File 035F0701.D  
 File Location GC/2023/Fester/Quarter 2  
 Injection Date 6/23/2023 2:04 PM  
 File Modified 6/26/2023 12:52 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type  
 Vial Number Vial 35  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 6/26/2023 12:49 PM  
 Printed 6/26/2023 2:04 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VB	11.75	26556.5	4577.77	103.521	1	103.521	ug/mL
Tetrahydrofuran	BB	18.99	54229.8	21440.9	149.190	1	149.190	ug/mL
Phenol	MM	24.84	56613.5	19705.7	129.893	1	129.893	ug/mL

### Analyst Peak Integration Comments

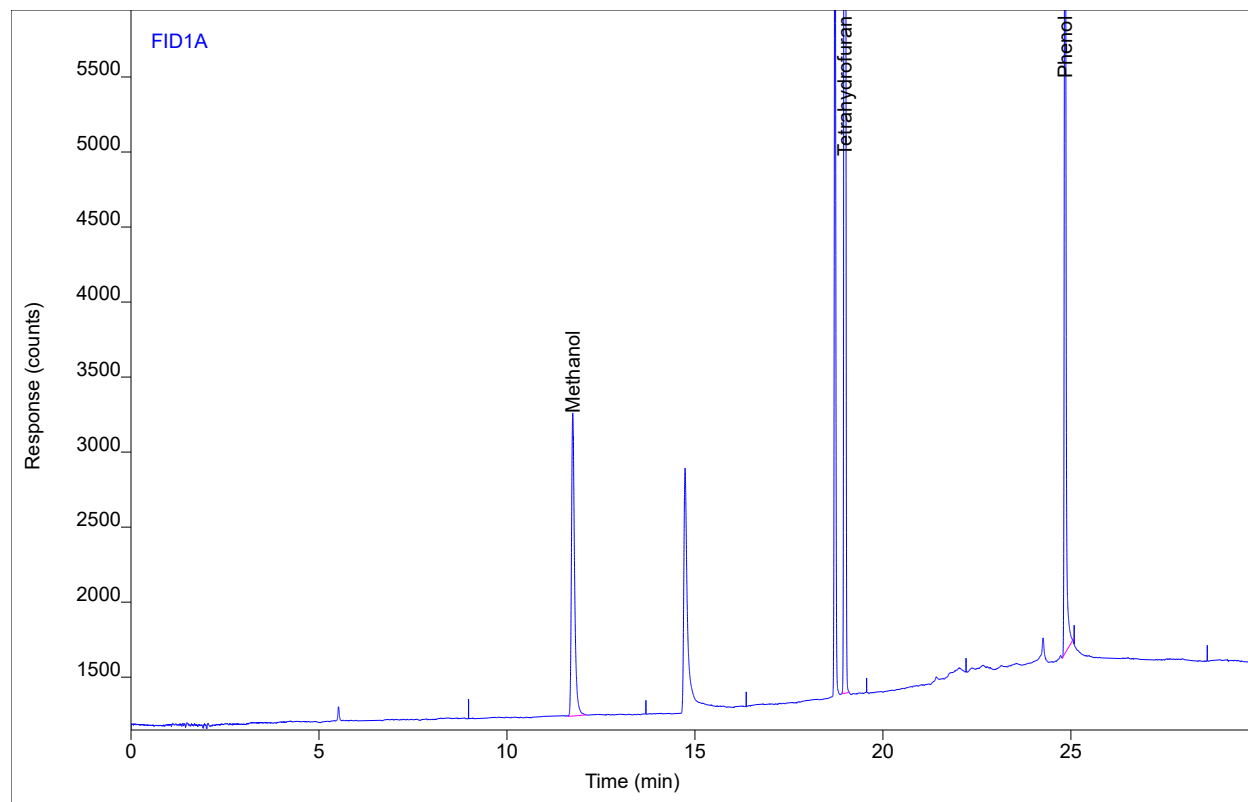
08:35:53 06/26/23 Remington Heathcoat ii

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #5  
Sequence Name FESTER0821 1 ver.1  
Inj Data File 036F0801.D  
File Location GC/2023/Fester/Quarter 2  
Injection Date 6/23/2023 2:40 PM  
File Modified 6/26/2023 12:52 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number  
Injection Volume  
Injection  
Acquisition Method  
Analysis Method  
Method Modified  
Printed  
Calibration  
Vial 36  
1  
1 of 1  
FESTER0258.M  
FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
6/26/2023 12:49 PM  
6/26/2023 2:04 PM



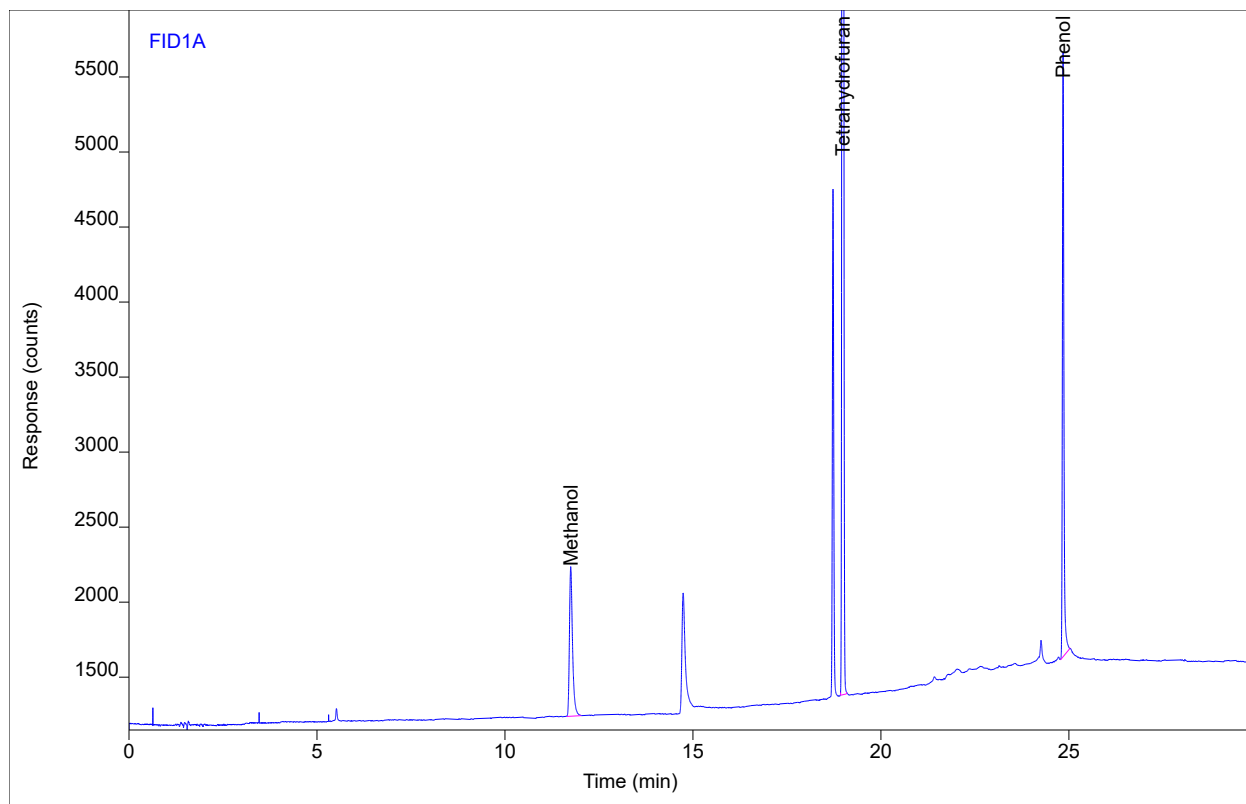
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VB	11.75	11576.9	2018.21	44.0784	1	44.0784	ug/mL
Tetrahydrofuran	BB	18.99	55521.7	21731.7	149.190	1	149.190	ug/mL
Phenol	VB	24.85	22754.6	8206.78	50.9929	1	50.9929	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #4  
Sequence Name FESTER0821 1 ver.1  
Inj Data File 037F0901.D  
File Location GC/2023/Fester/Quarter 2  
Injection Date 6/23/2023 3:16 PM  
File Modified 6/26/2023 12:52 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number 37  
Injection Volume 1  
Injection 1 of 1  
Acquisition Method FESTER0258.M  
Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
Method Modified 6/26/2023 12:49 PM  
Printed 6/26/2023 2:04 PM



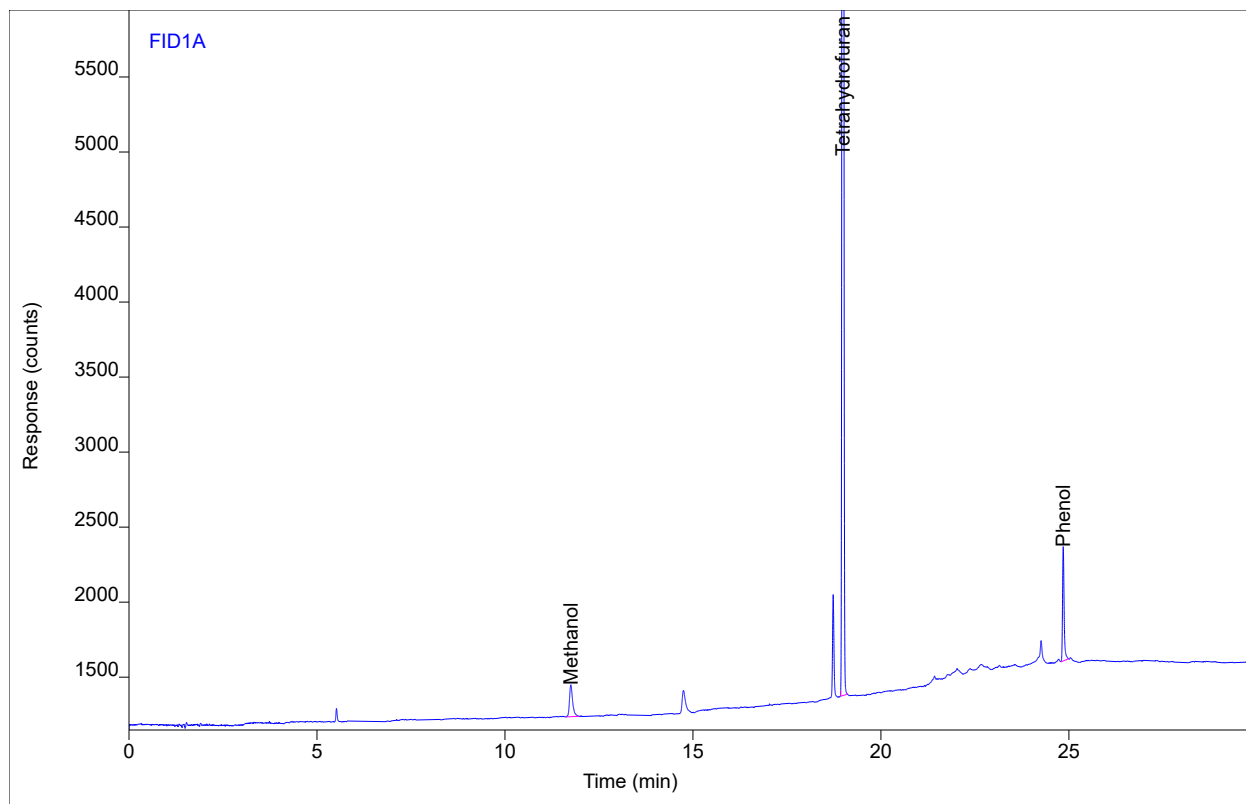
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.75	5708.51	998.001	22.1664	1	22.1664	ug/mL
Tetrahydrofuran	BB	18.99	54440.7	21499.0	149.190	1	149.190	ug/mL
Phenol	VB	24.85	11228.3	3999.46	25.6622	1	25.6622	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #3  
Sequence Name FESTER0821 1 ver.1  
Inj Data File 038F1001.D  
File Location GC/2023/Fester/Quarter 2  
Injection Date 6/23/2023 3:52 PM  
File Modified 6/26/2023 12:52 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number  
Injection Volume  
Injection  
Acquisition Method  
Analysis Method  
Method Modified  
Printed  
Calibration  
Vial 38  
1  
1 of 1  
FESTER0258.M  
FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
6/26/2023 12:49 PM  
6/26/2023 2:04 PM



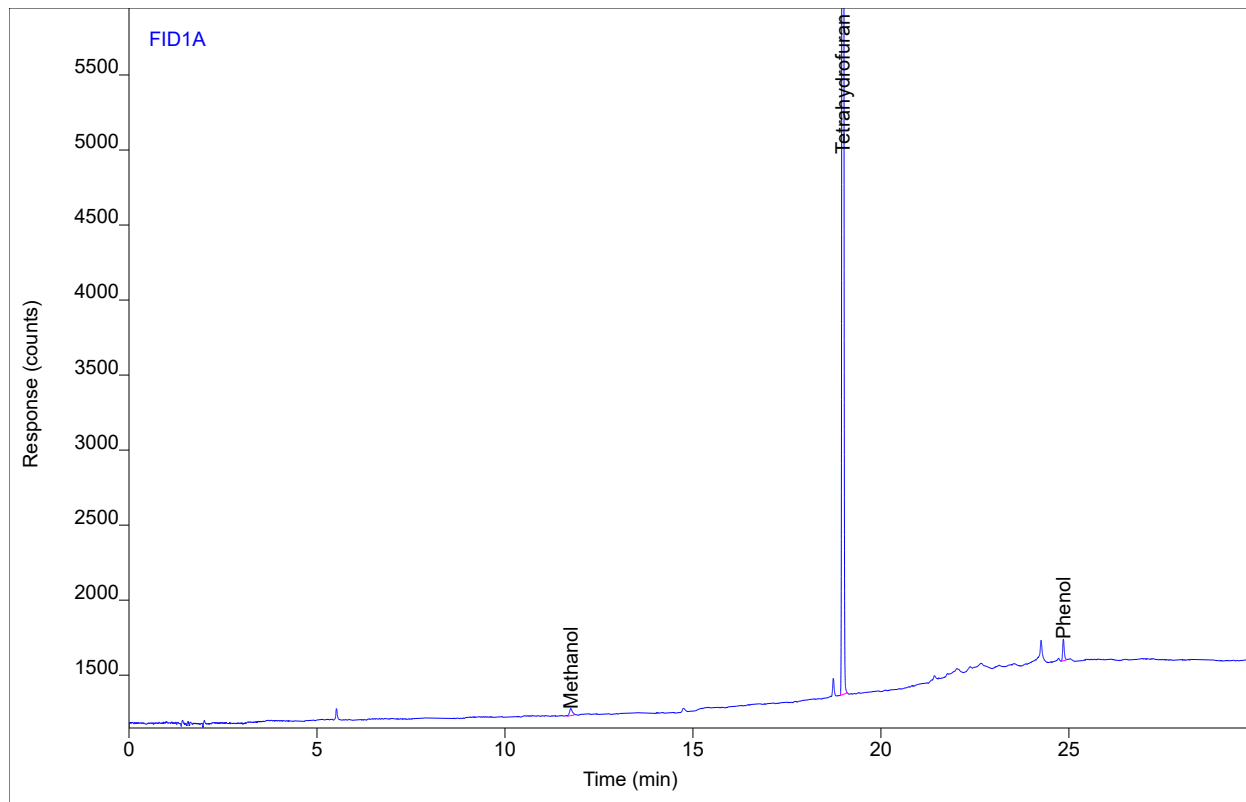
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VB	11.75	1246.11	213.589	4.82020	1	4.82020	ug/mL
Tetrahydrofuran	BB	18.99	54649.8	21602.6	149.190	1	149.190	ug/mL
Phenol	VB	24.85	2216.61	761.902	5.04666	1	5.04666	ug/mL

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #2  
Sequence Name FESTER0821 1 ver.1  
Inj Data File 039F1101.D  
File Location GC/2023/Fester/Quarter 2  
Injection Date 6/23/2023 4:28 PM  
File Modified 6/26/2023 12:52 PM  
Instrument Fester  
Operator Remington Heathcoat

Sample Type  
Vial Number  
Injection Volume  
Injection  
Acquisition Method  
Analysis Method  
Method Modified  
Printed  
Calibration  
Vial 39  
1  
1 of 1  
FESTER0258.M  
FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
6/26/2023 12:49 PM  
6/26/2023 2:04 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	VV	11.75	254.051	47.8732	0.96533	1	0.96533	ug/mL
Tetrahydrofuran	BB	18.99	55634.3	22000.8	149.190	1	149.190	ug/mL
Phenol	BB	24.85	420.312	145.379	0.94001	1	0.94001	ug/mL

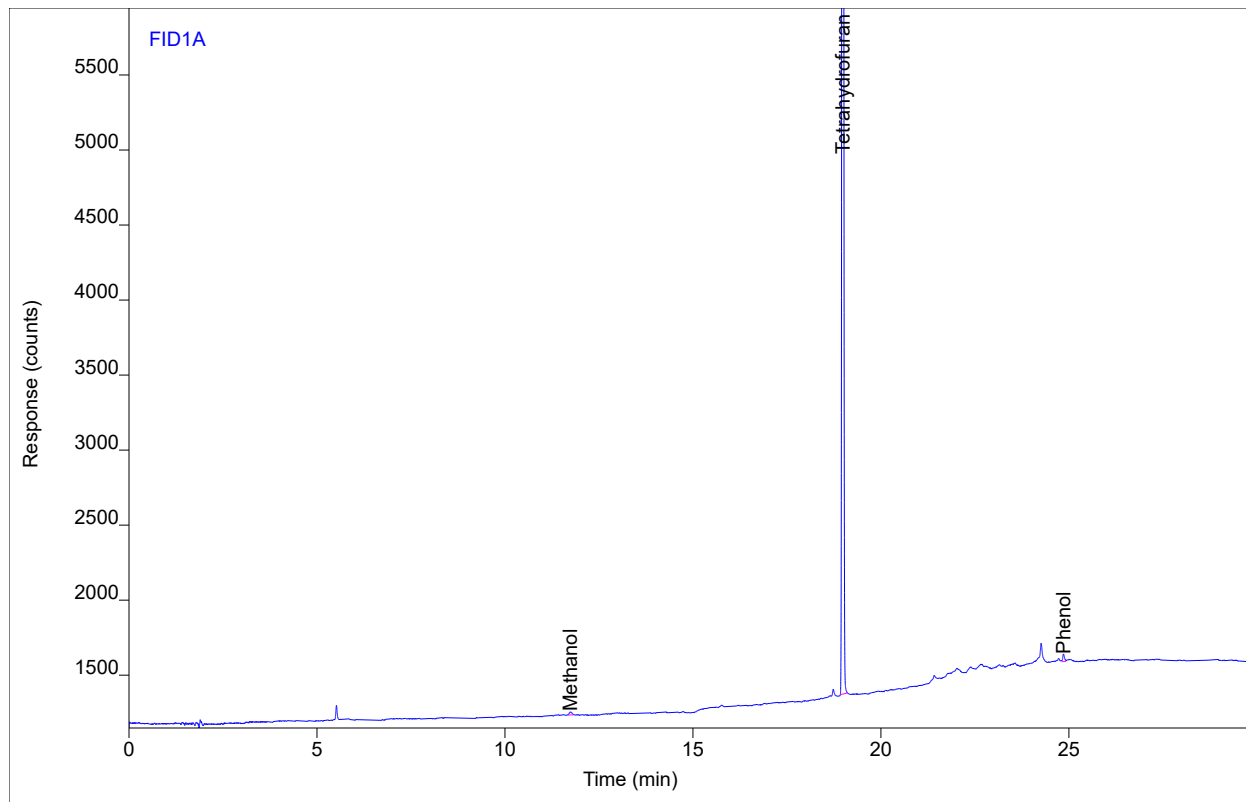


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #1  
 Sequence Name FESTER0821 1 ver.1  
 Inj Data File 040F1201.D  
 File Location GC/2023/Fester/Quarter 2  
 Injection Date 6/23/2023 5:04 PM  
 File Modified 6/26/2023 12:52 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type  
 Vial Number 1  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 6/26/2023 12:49 PM  
 Printed 6/26/2023 2:04 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	MM	11.74	110.872	25.5369	0.41800	1	0.41800	ug/mL
Tetrahydrofuran	BB	18.99	56071.1	22009.1	149.190	1	149.190	ug/mL
Phenol	MM	24.86	166.874	53.9441	0.37030	1	0.37030	ug/mL

### Analyst Peak Integration Comments

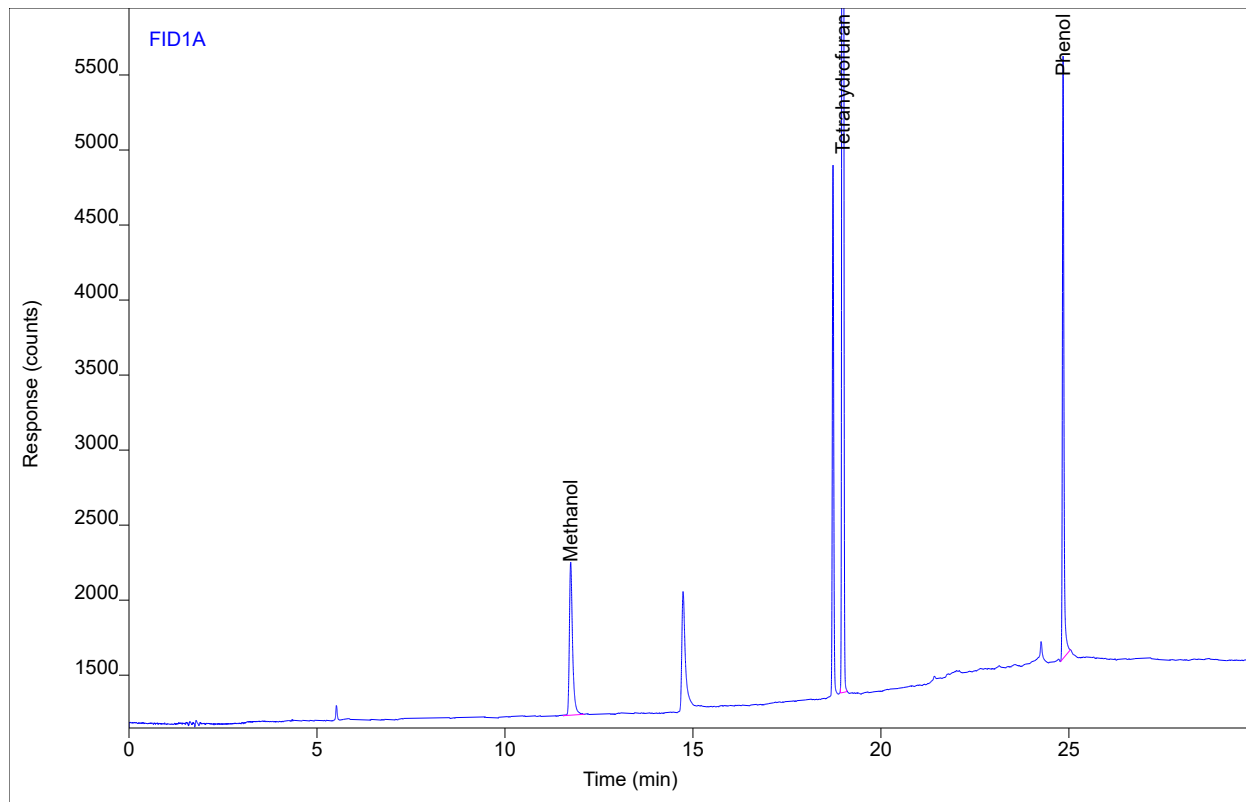
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 08:22:51 06/25/23 Remington Heathcoat i  
 08:30:43 06/26/23 Remington Heathcoat ii  
 08:32:23 06/26/23 Remington Heathcoat ii  
 08:56:18 06/26/23 Remington Heathcoat ni-2-butanone  
 08:57:52 06/26/23 Remington Heathcoat ni-ethanol  
 08:58:44 06/26/23 Remington Heathcoat ii

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1855 #3ss  
 Sequence Name FESTER0821 1 ver.1  
 Inj Data File 041F1301.D  
 File Location GC/2023/Fester/Quarter 2  
 Injection Date 6/23/2023 5:40 PM  
 File Modified 6/26/2023 12:52 PM  
 Instrument Fester  
 Operator Remington Heathcoat

Sample Type Control  
 Vial Number Vial 41  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method FESTER0258.M  
 Analysis Method FESTER0821\_MEOH\_PHENOL\_THF-IS.M  
 Method Modified 6/26/2023 12:49 PM  
 Printed 6/26/2023 2:04 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Methanol	BB	11.75	6008.68	1021.39	22.0546	1	22.0546	ug/mL
Tetrahydrofuran	BB	18.99	57593.9	22565.9	149.190	1	149.190	ug/mL
Phenol	VB	24.85	11243.2	4002.76	24.2894	1	24.2894	ug/mL

# Raw Data

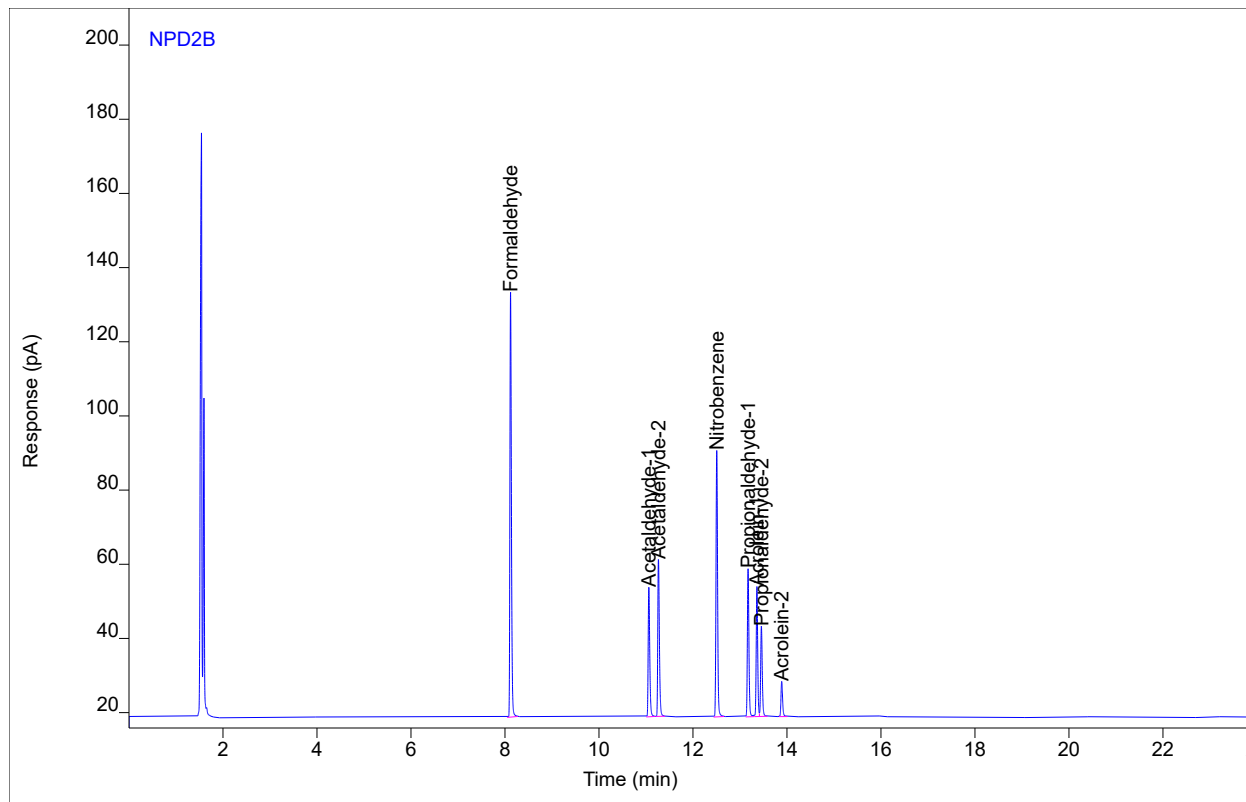


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #3  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 040B0601.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 12:54 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type  
 Vial Number Vial 40  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



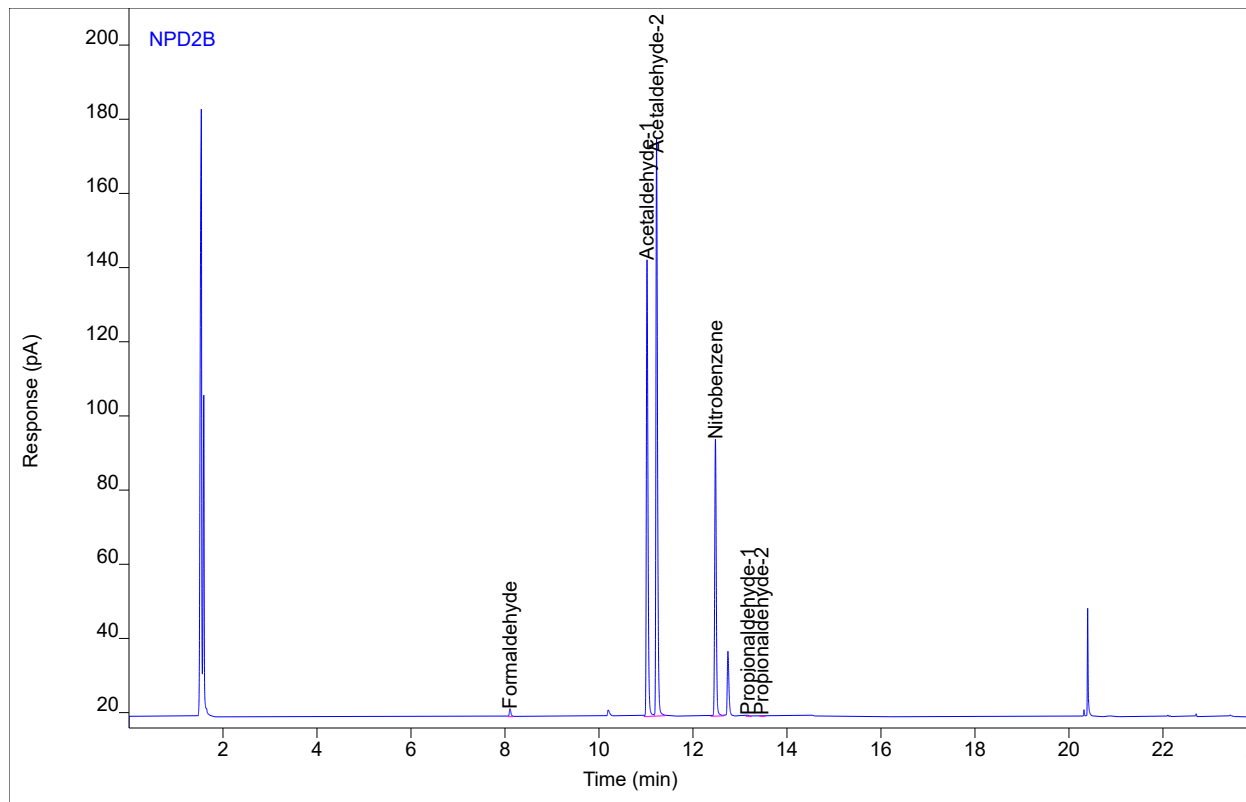
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				5.96350	1	5.96350	
Acrolein	Group				6.33704	1	6.33704	
Propionaldehyde	Group				6.17200	1	6.17200	
Formaldehyde	BB	8.12	250.199	114.615	6.24373	1	6.24373	ug/ml
Acetaldehyde-1	VB	11.06	81.0862	35.0615	2.67094	1	2.67094	ug/ml
Acetaldehyde-2	BB	11.27	99.9577	42.4888	3.29256	1	3.29256	ug/ml
Nitrobenzene	BB	12.51	168.037	71.9717	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.17	90.4789	40.0494	3.76910	1	3.76910	ug/ml
Acrolein-1	BV	13.36	76.4540	35.1811	4.88171	1	4.88171	ug/ml
Propionaldehyde-2	VB	13.46	57.6826	24.4373	2.40290	1	2.40290	ug/ml
Acrolein-2	BB	13.89	22.7923	9.62280	1.45533	1	1.45533	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R1.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 026B0801.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 2:44 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 26  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



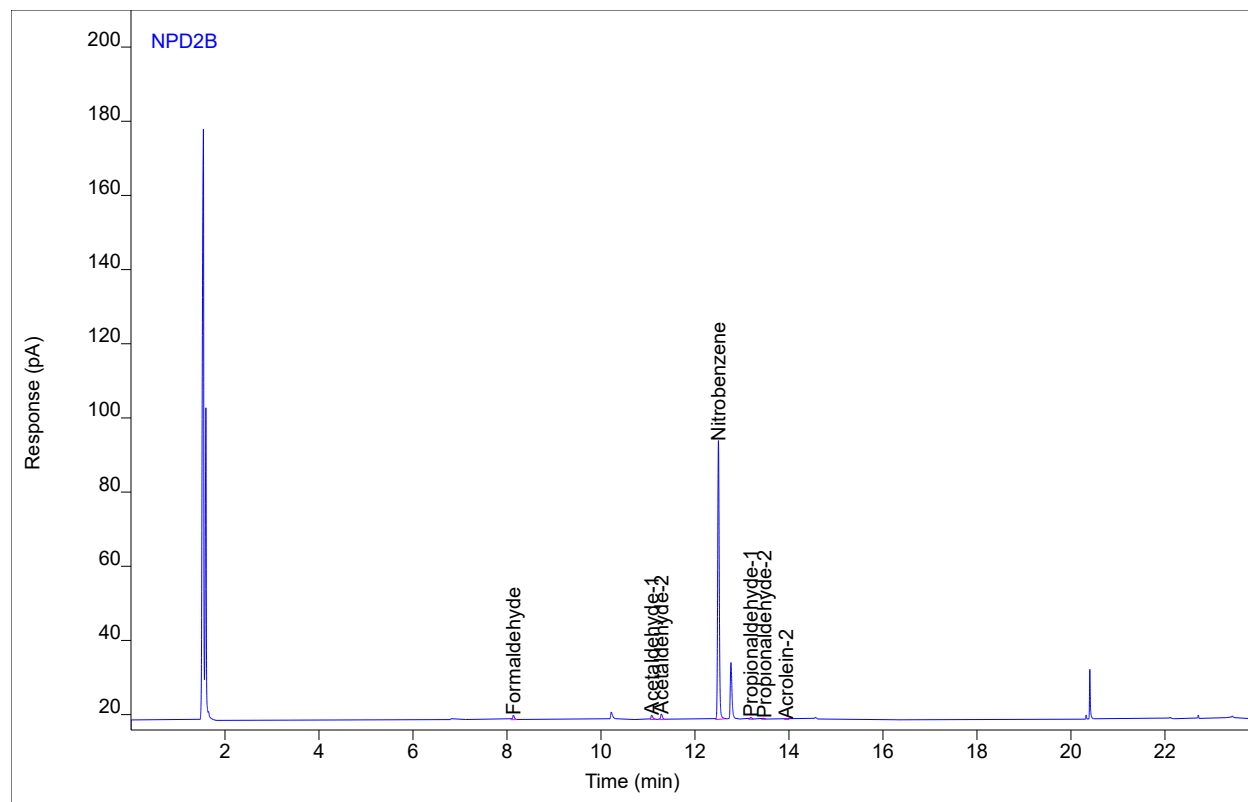
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				20.6013	1	20.6013	
Acrolein	Group					1		
Propionaldehyde	Group				0.08722	1	0.08722	
Formaldehyde	VV	8.11	5.22688	2.19716	0.12567	1	0.12567	ug/ml
Acetaldehyde-1	VV	11.02	285.956	123.351	9.07530	1	9.07530	ug/ml
Acetaldehyde-2	VV	11.23	363.176	155.756	11.5260	1	11.5260	ug/ml
Nitrobenzene	BB	12.48	174.405	74.7600	100.000	1	100.000	ug/ml
Propionaldehyde-1	VB	13.17	1.26757	0.46807	0.05088	1	0.05088	ug/ml
Acrolein-1		(13.38)				1		
Propionaldehyde-2	BB	13.46	0.90556	0.29702	0.03635	1	0.03635	ug/ml
Acrolein-2		(13.91)				1		

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R1-DUP.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 027B0901.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 3:13 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 27  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



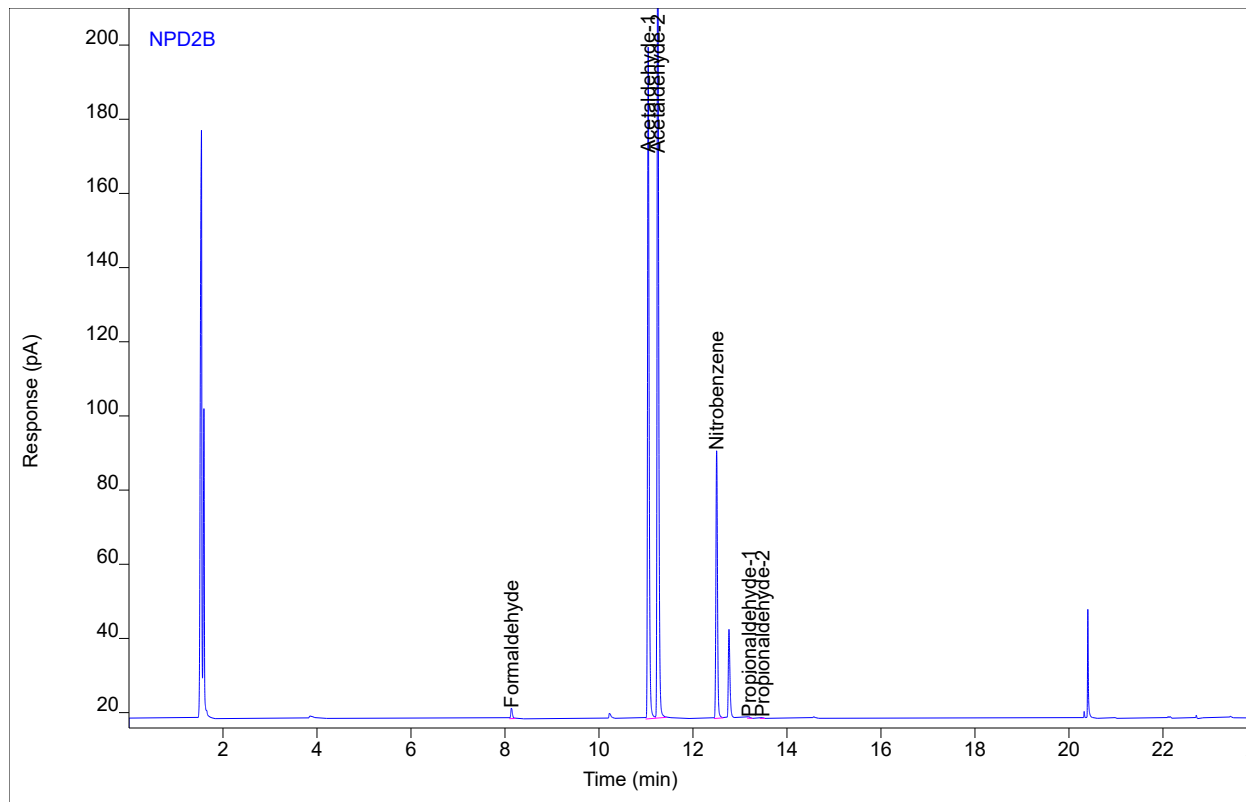
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				0.23573	1	0.23573	
Acrolein	Group				0.02396	1	0.02396	
Propionaldehyde	Group				0.09179	1	0.09179	
Formaldehyde	BV	8.14	3.15037	1.29794	0.07600	1	0.07600	ug/ml
Acetaldehyde-1	VV	11.08	3.31094	1.33344	0.10542	1	0.10542	ug/ml
Acetaldehyde-2	BB	11.29	4.09238	1.63369	0.13031	1	0.13031	ug/ml
Nitrobenzene	VB	12.50	173.833	75.1955	100.000	1	100.000	ug/ml
Propionaldehyde-1	VV	13.19	1.41075	0.55793	0.05681	1	0.05681	ug/ml
Acrolein-1		(13.38)				1		
Propionaldehyde-2	VV	13.48	0.86862	0.33514	0.03498	1	0.03498	ug/ml
Acrolein-2	VV	13.94	0.38827	0.10141	0.02396	1	0.02396	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R2.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 028B1001.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 3:42 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 28  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



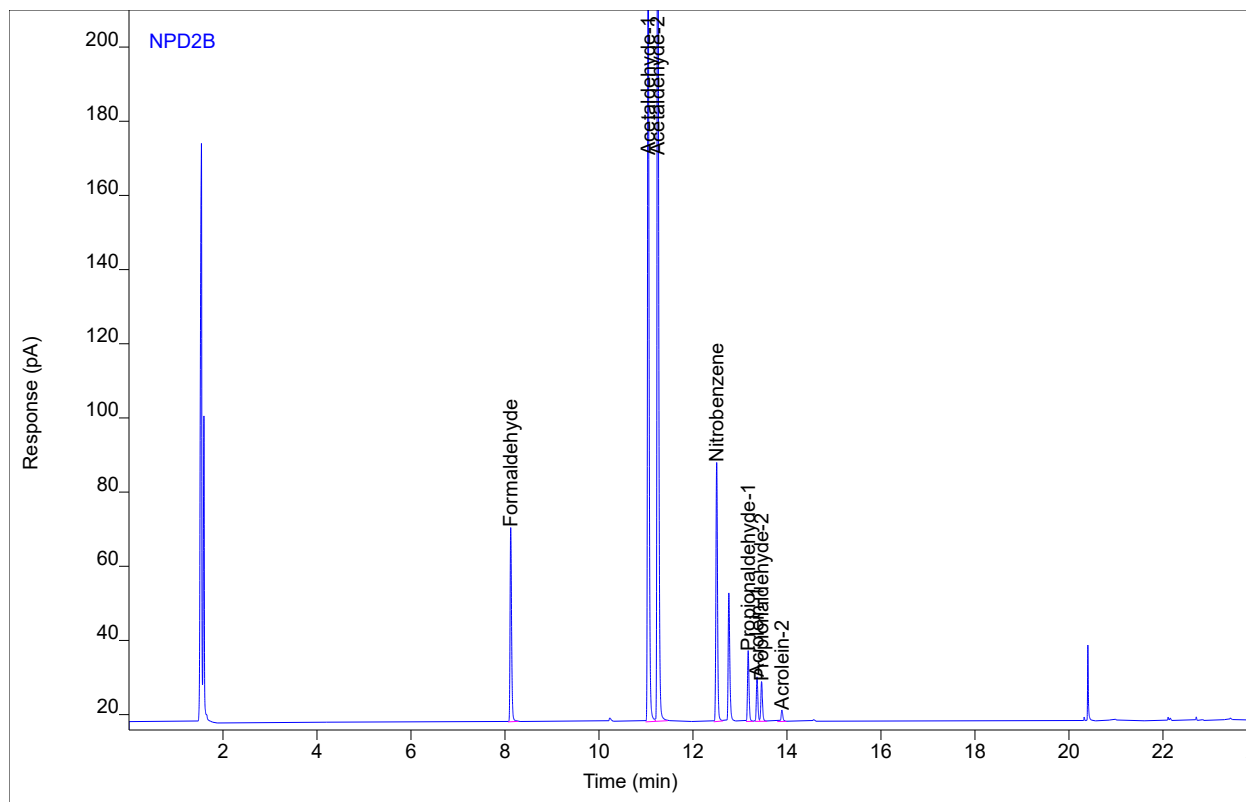
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				30.9041	1	30.9041	
Acrolein	Group					1		
Propionaldehyde	Group				0.07801	1	0.07801	
Formaldehyde	VB	8.14	6.86512	2.99437	0.16979	1	0.16979	ug/ml
Acetaldehyde-1	VV	11.05	416.280	181.146	13.5900	1	13.5900	ug/ml
Acetaldehyde-2	VV	11.25	530.351	231.127	17.3141	1	17.3141	ug/ml
Nitrobenzene	VB	12.50	169.545	72.3709	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.20	1.19454	0.47629	0.04932	1	0.04932	ug/ml
Acrolein-1		(13.38)				1		
Propionaldehyde-2	BV	13.48	0.69485	0.27842	0.02869	1	0.02869	ug/ml
Acrolein-2		(13.91)				1		

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R2-L-SPK.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 029B1101.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 4:11 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 29  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				38.1971	1	38.1971	
Acrolein	Group				2.24043	1	2.24043	
Propionaldehyde	Group				2.88491	1	2.88491	
Formaldehyde	VB	8.12	116.474	52.5166	2.95316	1	2.95316	ug/ml
Acetaldehyde-1	BV	11.05	499.042	218.244	16.7015	1	16.7015	ug/ml
Acetaldehyde-2	VB	11.25	642.292	278.266	21.4956	1	21.4956	ug/ml
Nitrobenzene	VB	12.50	165.388	70.0596	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.18	42.4269	19.1411	1.79569	1	1.79569	ug/ml
Acrolein-1	BV	13.36	26.9356	12.0700	1.74743	1	1.74743	ug/ml
Propionaldehyde-2	VB	13.46	25.7350	10.8695	1.08922	1	1.08922	ug/ml
Acrolein-2	BB	13.89	7.59933	3.15124	0.49300	1	0.49300	ug/ml

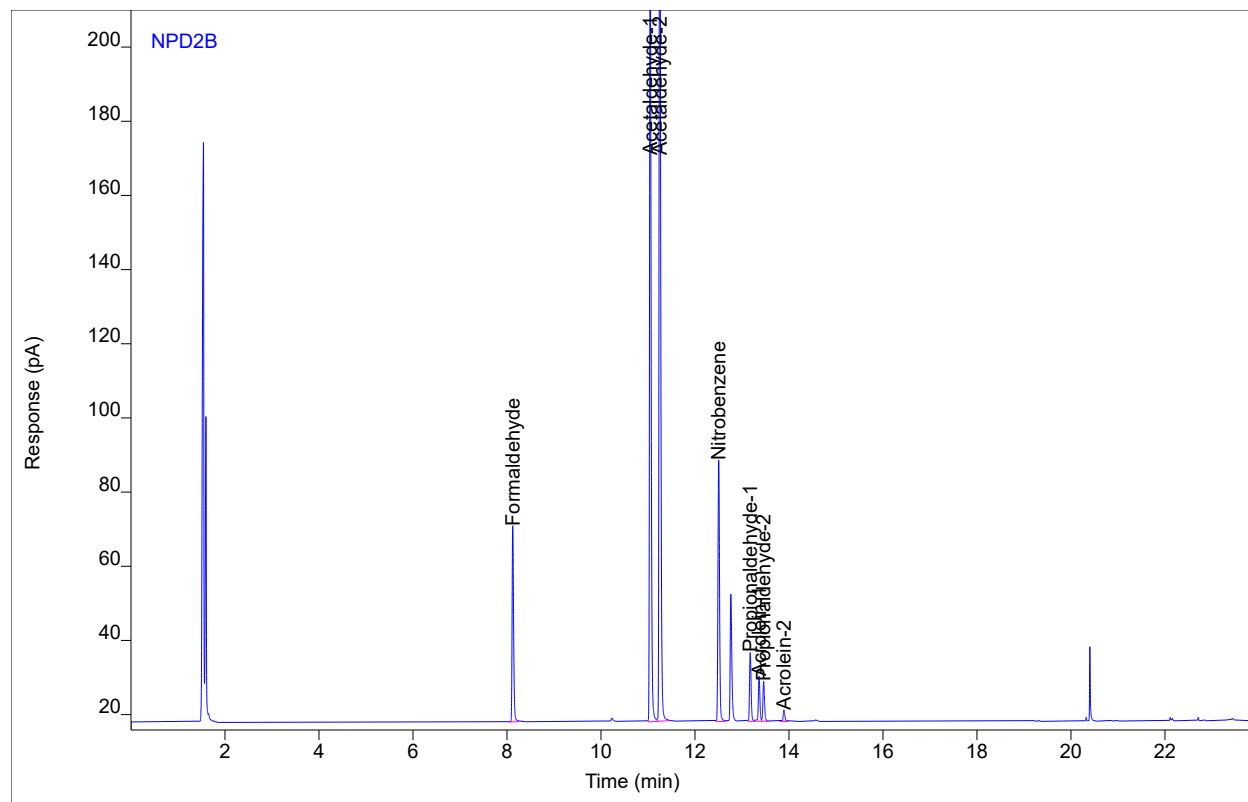


# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R2-L-SPK-LD.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 030B1201.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 4:40 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 30  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



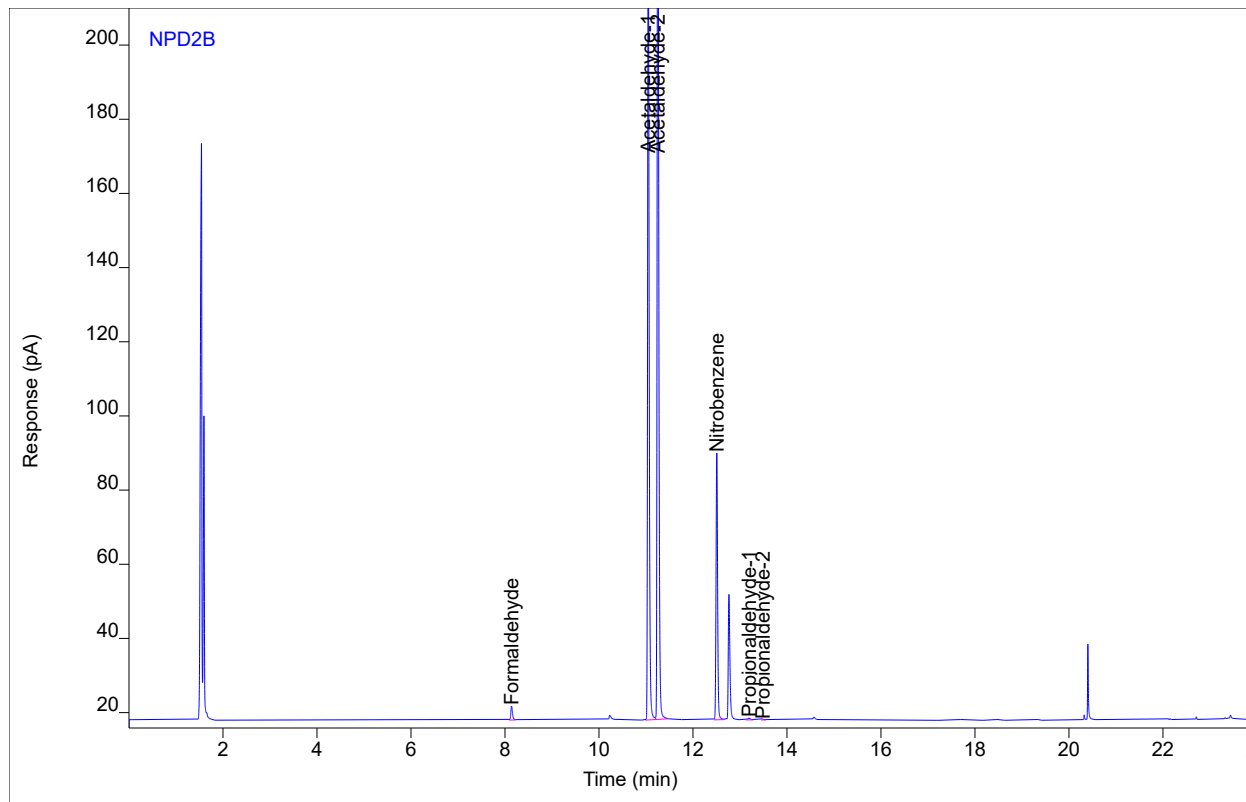
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				37.9078	1	37.9078	
Acrolein	Group				2.23273	1	2.23273	
Propionaldehyde	Group				2.89395	1	2.89395	
Formaldehyde	VB	8.12	116.744	52.9339	2.93437	1	2.93437	ug/ml
Acetaldehyde-1	BV	11.05	500.234	219.679	16.5964	1	16.5964	ug/ml
Acetaldehyde-2	VB	11.25	642.351	282.808	21.3114	1	21.3114	ug/ml
Nitrobenzene	VB	12.51	166.833	70.5321	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.18	42.9941	18.6832	1.80394	1	1.80394	ug/ml
Acrolein-1	BV	13.36	27.0082	12.1983	1.73696	1	1.73696	ug/ml
Propionaldehyde-2	VB	13.46	25.9787	10.7754	1.09001	1	1.09001	ug/ml
Acrolein-2	BB	13.89	7.70883	3.20779	0.49577	1	0.49577	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R3.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 031B1301.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 5:09 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 31  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



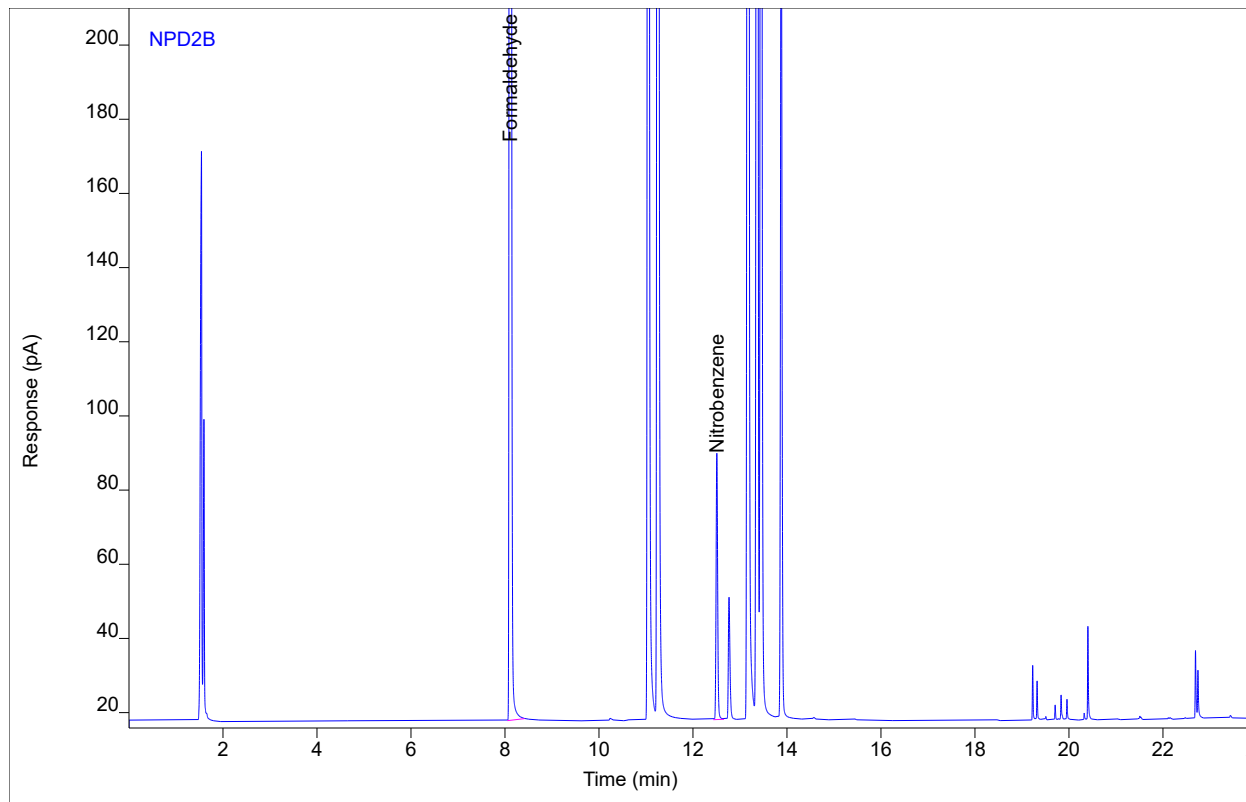
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				37.4589	1	37.4589	
Acrolein	Group					1		
Propionaldehyde	Group				0.11769	1	0.11769	
Formaldehyde	VV	8.14	9.26319	3.94808	0.23344	1	0.23344	ug/ml
Acetaldehyde-1	VV	11.05	494.768	216.995	16.4582	1	16.4582	ug/ml
Acetaldehyde-2	VV	11.25	631.325	271.387	21.0007	1	21.0007	ug/ml
Nitrobenzene	BV	12.51	166.395	72.1766	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.20	1.94769	0.69703	0.08194	1	0.08194	ug/ml
Acrolein-1		(13.38)				1		
Propionaldehyde-2	BB	13.48	0.84996	0.37418	0.03576	1	0.03576	ug/ml
Acrolein-2		(13.91)				1		

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R3-H-SPK.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 032B1401.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 5:38 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 32  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



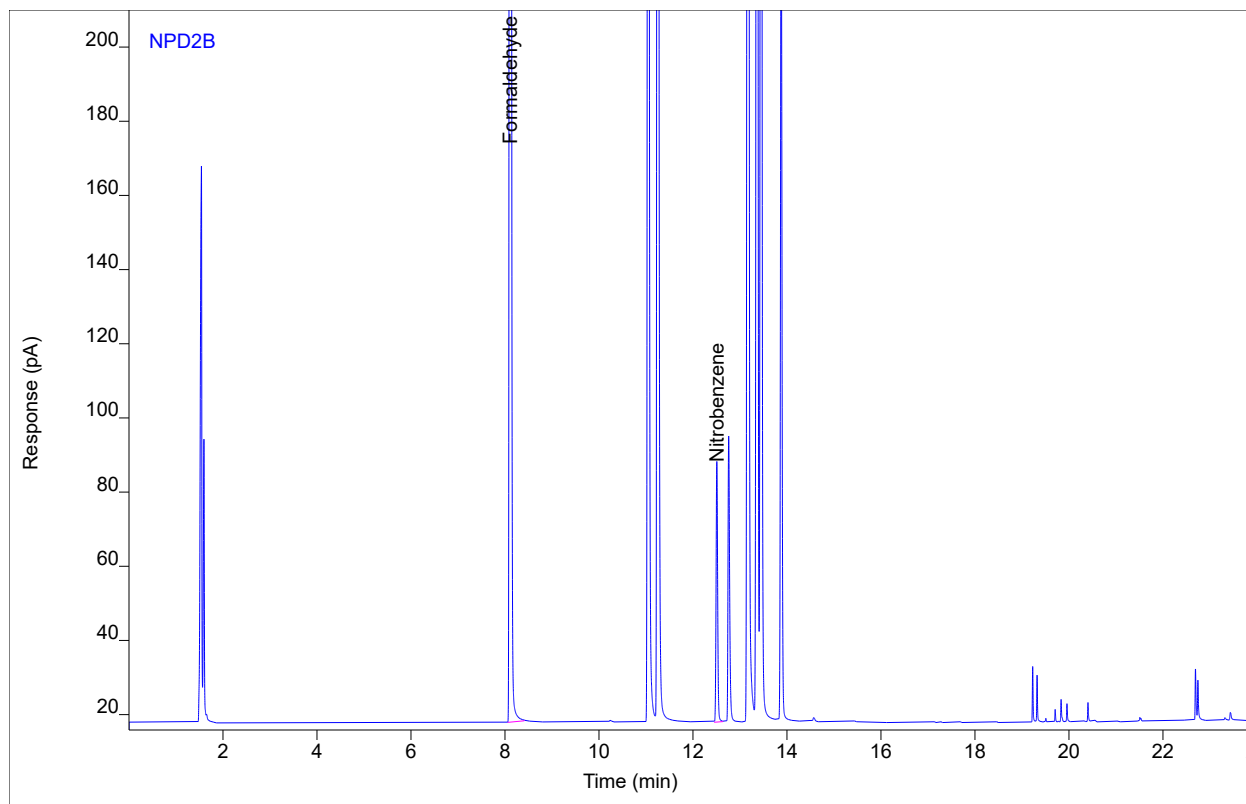
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Formaldehyde	BB	8.11	3723.18	1705.33	93.6695	1	93.6695	ug/ml
Nitrobenzene	VB	12.51	166.678	71.9550	100.000	1	100.000	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.TS.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 033B1501.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 6:07 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 33  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



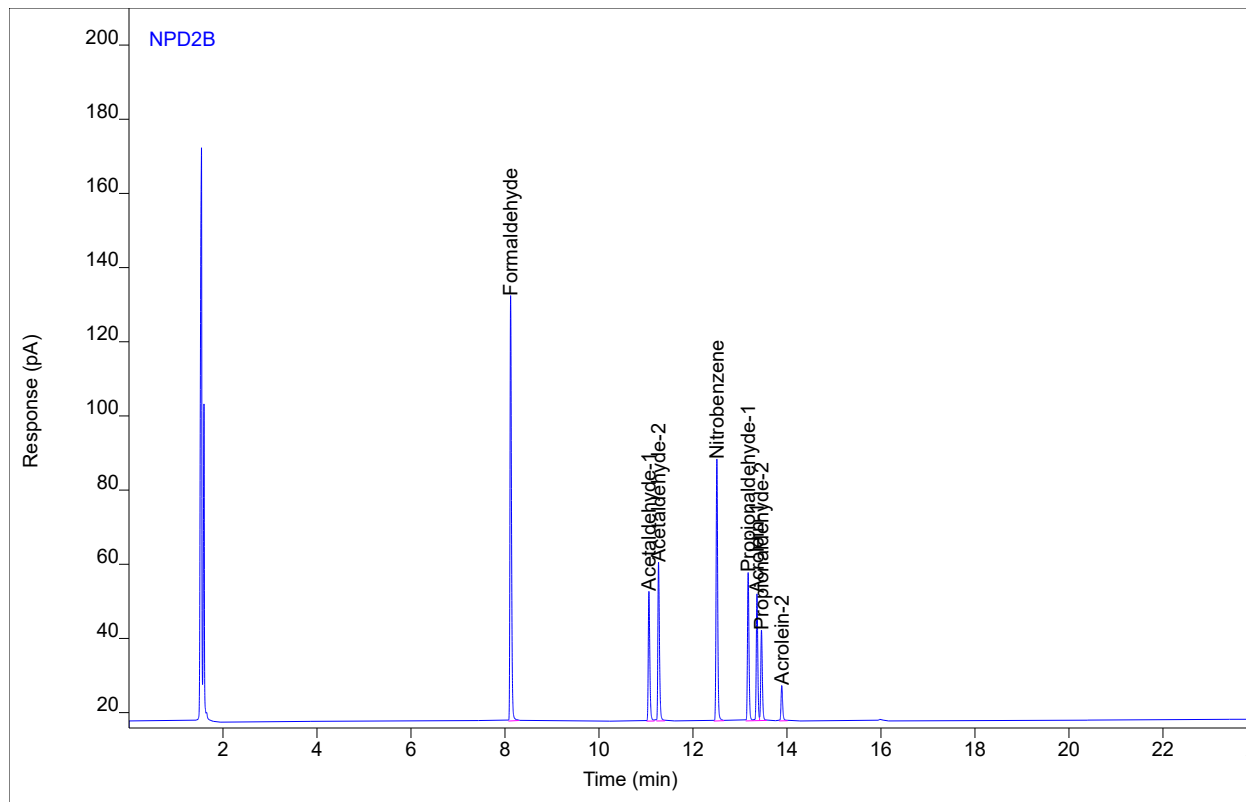
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Formaldehyde	VV	8.11	3363.71	1553.69	86.7490	1	86.7490	ug/ml
Nitrobenzene	BB	12.51	162.598	70.2877	100.000	1	100.000	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #3  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 040B1601.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 6:36 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type  
 Vial Number Vial 40  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



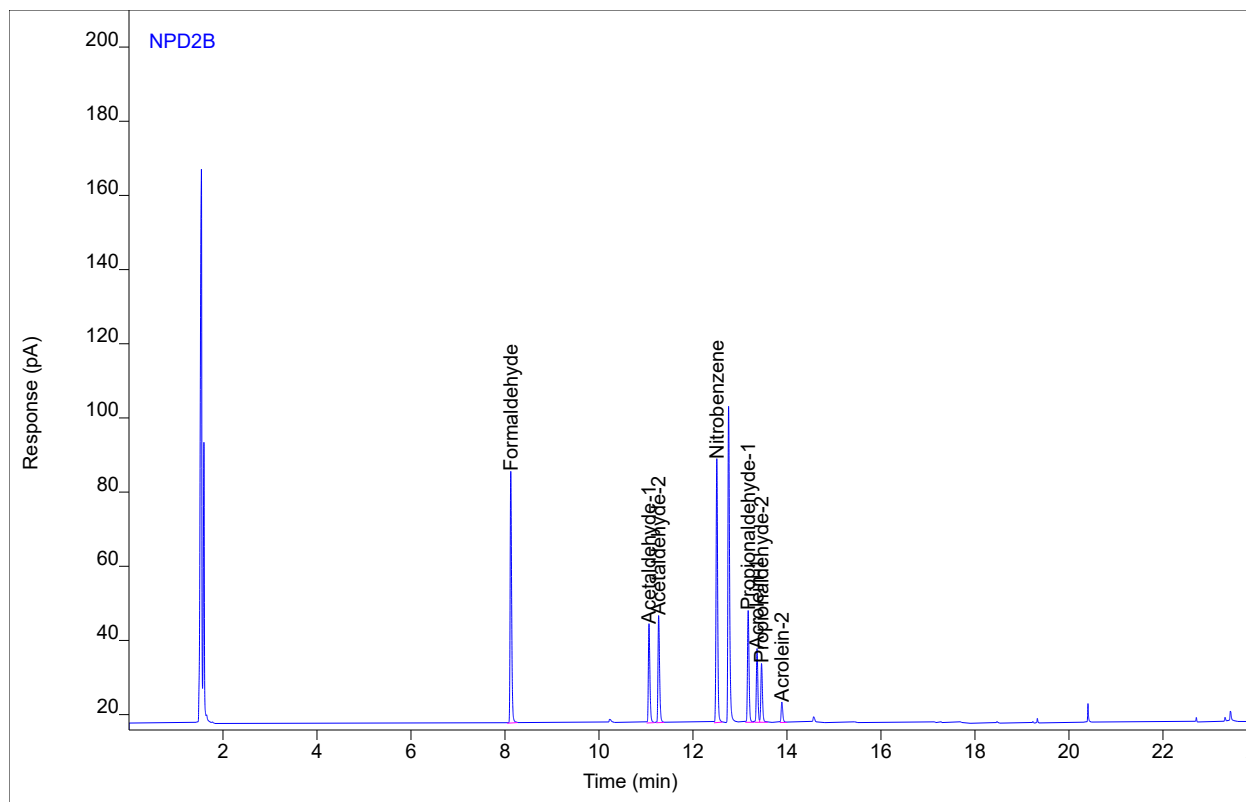
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				6.05708	1	6.05708	
Acrolein	Group				6.41330	1	6.41330	
Propionaldehyde	Group				6.22292	1	6.22292	
Formaldehyde	BB	8.12	250.599	114.709	6.34328	1	6.34328	ug/ml
Acetaldehyde-1	VV	11.06	80.5560	35.1768	2.69149	1	2.69149	ug/ml
Acetaldehyde-2	BV	11.27	100.732	42.8235	3.36559	1	3.36559	ug/ml
Nitrobenzene	BB	12.51	165.664	70.7003	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.17	90.1259	40.1408	3.80817	1	3.80817	ug/ml
Acrolein-1	VV	13.36	76.0256	34.3654	4.92389	1	4.92389	ug/ml
Propionaldehyde-2	VB	13.46	57.1484	24.4163	2.41474	1	2.41474	ug/ml
Acrolein-2	VB	13.89	22.9967	9.71206	1.48941	1	1.48941	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.F-L-SPK.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 034B1701.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 7:05 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 34  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



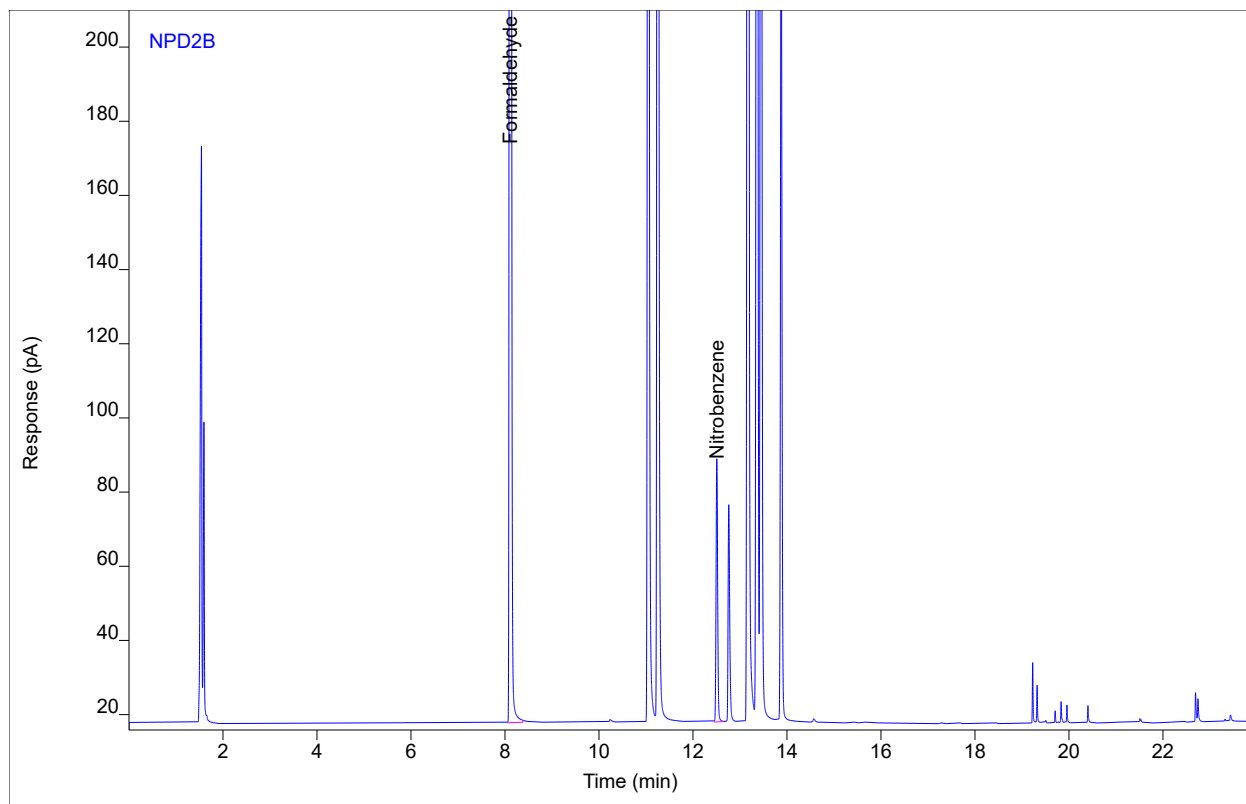
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				4.32593	1	4.32593	
Acrolein	Group				3.74452	1	3.74452	
Propionaldehyde	Group				4.51644	1	4.51644	
Formaldehyde	VB	8.12	148.204	67.9874	3.76551	1	3.76551	ug/ml
Acetaldehyde-1	VB	11.06	60.6724	26.7617	2.03477	1	2.03477	ug/ml
Acetaldehyde-2	VB	11.27	68.3178	29.0436	2.29117	1	2.29117	ug/ml
Nitrobenzene	VV	12.51	165.044	71.1774	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.17	68.8080	30.3282	2.91834	1	2.91834	ug/ml
Acrolein-1	BV	13.36	44.2742	19.8792	2.87825	1	2.87825	ug/ml
Propionaldehyde-2	VB	13.46	37.6799	15.9286	1.59811	1	1.59811	ug/ml
Acrolein-2	BB	13.89	13.3252	5.58137	0.86627	1	0.86627	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.F-H-SPK.HEX  
Sequence Name LOLITA0463 ver.1  
Inj Data File 035B1801.D  
File Location GC/2023/Lolita/Quarter 2  
Injection Date 7/19/2023 7:34 PM  
File Modified 7/19/2023 11:27 PM  
Instrument Lolita  
Operator Aaron Petersen

Sample Type Sample  
Vial Number Vial 35  
Injection Volume 1  
Injection 1 of 1  
Acquisition Method LOLITA0349X.M  
Analysis Method LOLITA0458\_NPD.M  
Method Modified 6/26/2023 12:20 PM  
Printed 7/25/2023 12:44 PM



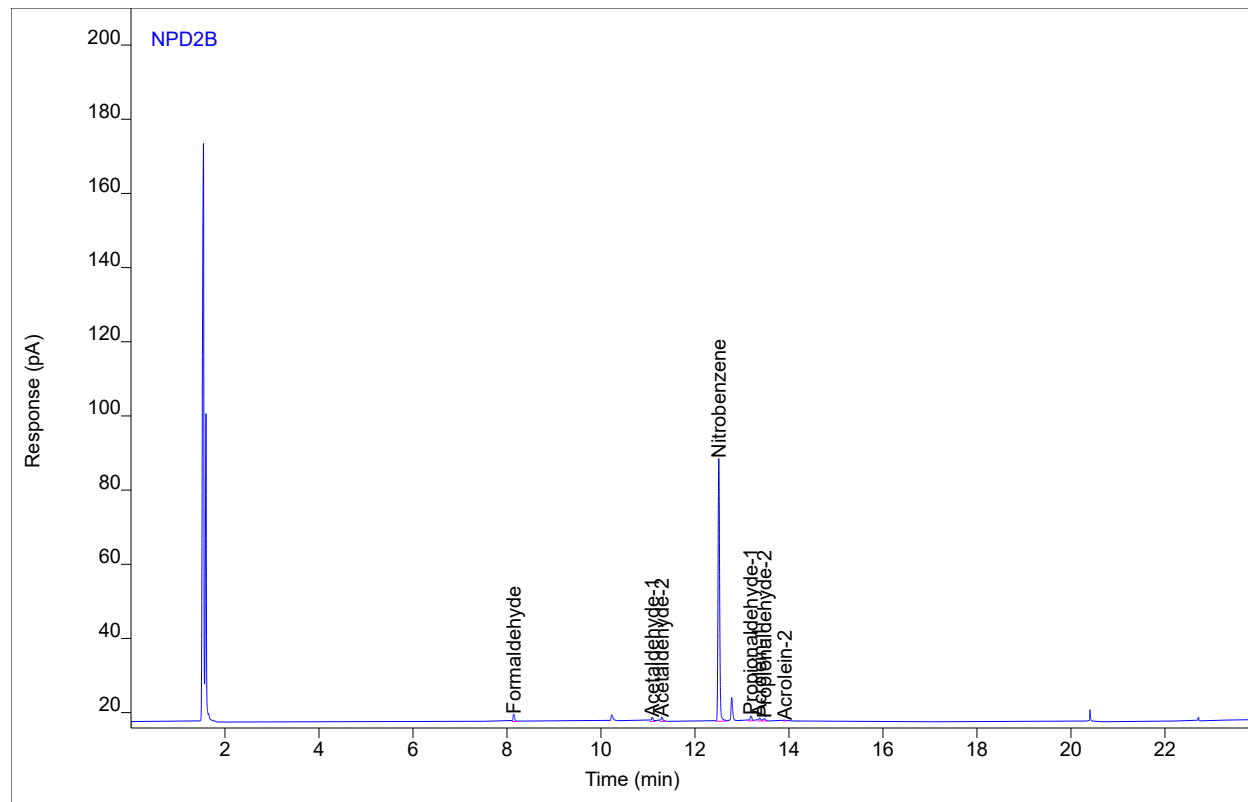
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Formaldehyde	BV	8.11	3322.22	1523.74	83.4589	1	83.4589	ug/ml
Nitrobenzene	BB	12.51	166.924	71.0069	100.000	1	100.000	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.BLK.HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 036B1901.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 8:03 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 36  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				0.20818	1	0.20818	
Acrolein	Group				0.20582	1	0.20582	
Propionaldehyde	Group				0.24093	1	0.24093	
Formaldehyde	VB	8.14	4.90878	2.11868	0.12312	1	0.12312	ug/ml
Acetaldehyde-1	VV	11.09	3.06644	1.19891	0.10152	1	0.10152	ug/ml
Acetaldehyde-2	VV	11.30	3.22196	1.26525	0.10666	1	0.10666	ug/ml
Nitrobenzene	VV	12.51	167.195	71.0612	100.000	1	100.000	ug/ml
Propionaldehyde-1	VB	13.19	3.63264	1.50512	0.15209	1	0.15209	ug/ml
Acrolein-1	BV	13.38	2.44576	0.96332	0.15695	1	0.15695	ug/ml
Propionaldehyde-2	VV	13.48	2.12198	0.82926	0.08884	1	0.08884	ug/ml
Acrolein-2	VV	13.91	0.76153	0.29639	0.04887	1	0.04887	ug/ml

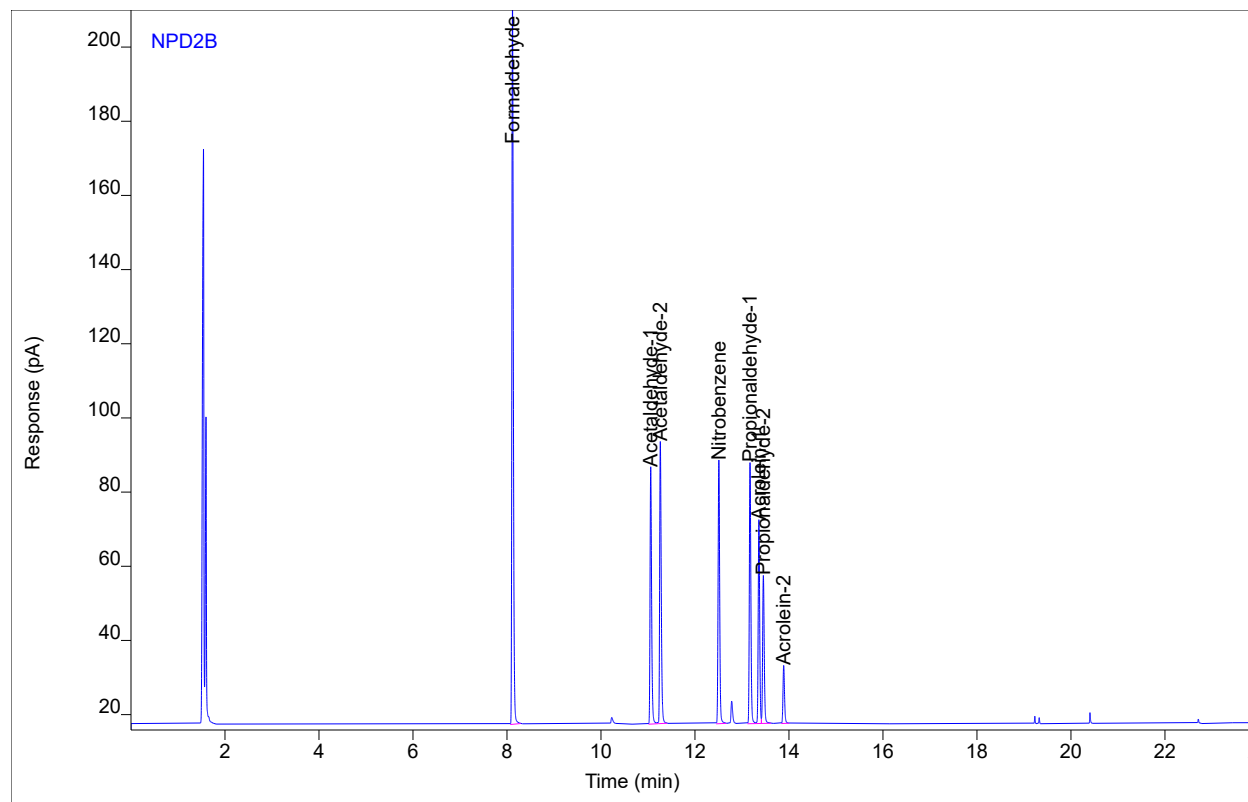


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcprep5570 #LCS-L-HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 037B2001.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 8:32 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 37  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



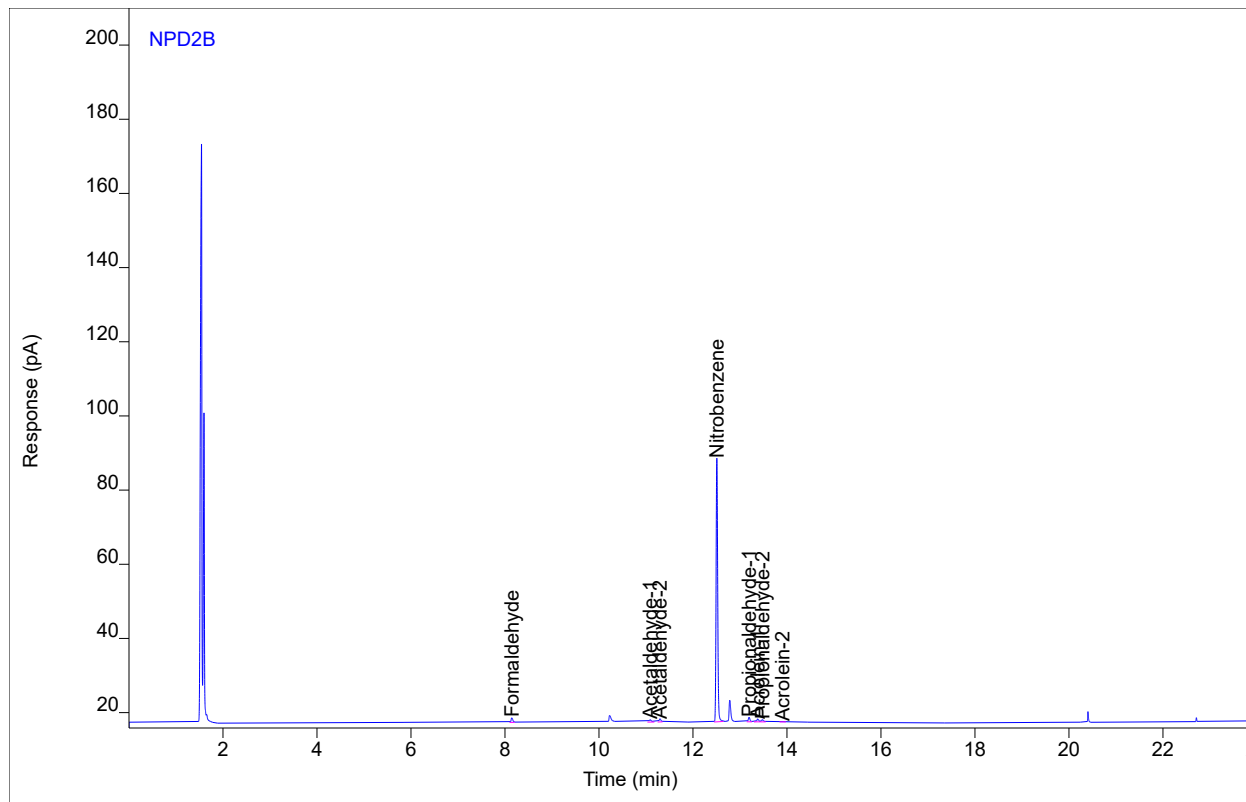
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				11.1795	1	11.1795	
Acrolein	Group				10.0527	1	10.0527	
Propionaldehyde	Group				10.7903	1	10.7903	
Formaldehyde	BB	8.12	420.595	194.055	10.6561	1	10.6561	ug/ml
Acetaldehyde-1	BB	11.06	158.148	69.4181	5.28879	1	5.28879	ug/ml
Acetaldehyde-2	BB	11.26	176.147	76.2163	5.89070	1	5.89070	ug/ml
Nitrobenzene	BB	12.51	165.512	71.1057	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.17	160.183	70.5275	6.77458	1	6.77458	ug/ml
Acrolein-1	VV	13.36	119.257	55.0100	7.73092	1	7.73092	ug/ml
Propionaldehyde-2	VB	13.46	94.9502	39.8956	4.01570	1	4.01570	ug/ml
Acrolein-2	BB	13.89	35.8165	15.7399	2.32183	1	2.32183	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcprep5570 #MB-HEX  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 039B2201.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 9:30 PM  
 File Modified 7/19/2023 11:27 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 39  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



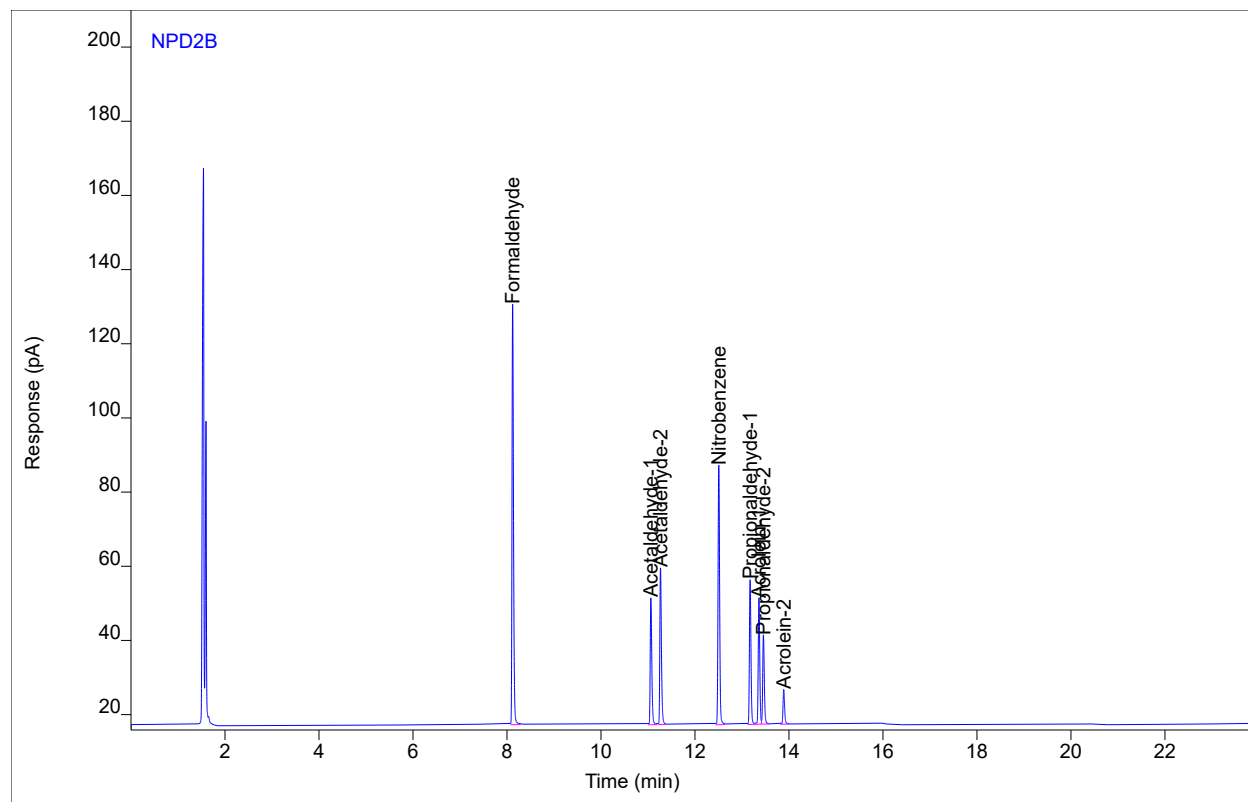
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				0.13225	1	0.13225	
Acrolein	Group				0.20360	1	0.20360	
Propionaldehyde	Group				0.21107	1	0.21107	
Formaldehyde	VV	8.15	3.27343	1.38335	0.08202	1	0.08202	ug/ml
Acetaldehyde-1	VV	11.09	1.88645	0.74385	0.06239	1	0.06239	ug/ml
Acetaldehyde-2	VV	11.30	2.11245	0.88448	0.06986	1	0.06986	ug/ml
Nitrobenzene	BV	12.51	167.360	71.1932	100.000	1	100.000	ug/ml
Propionaldehyde-1	VV	13.19	3.06467	1.24071	0.12818	1	0.12818	ug/ml
Acrolein-1	VV	13.38	2.25956	0.88862	0.14486	1	0.14486	ug/ml
Propionaldehyde-2	VV	13.48	1.98187	0.74292	0.08289	1	0.08289	ug/ml
Acrolein-2	BV	13.91	0.91629	0.27471	0.05874	1	0.05874	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #3  
 Sequence Name LOLITA0463 ver.1  
 Inj Data File 040B2301.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/19/2023 9:59 PM  
 File Modified 7/19/2023 11:28 PM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type  
 Vial Number 40  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



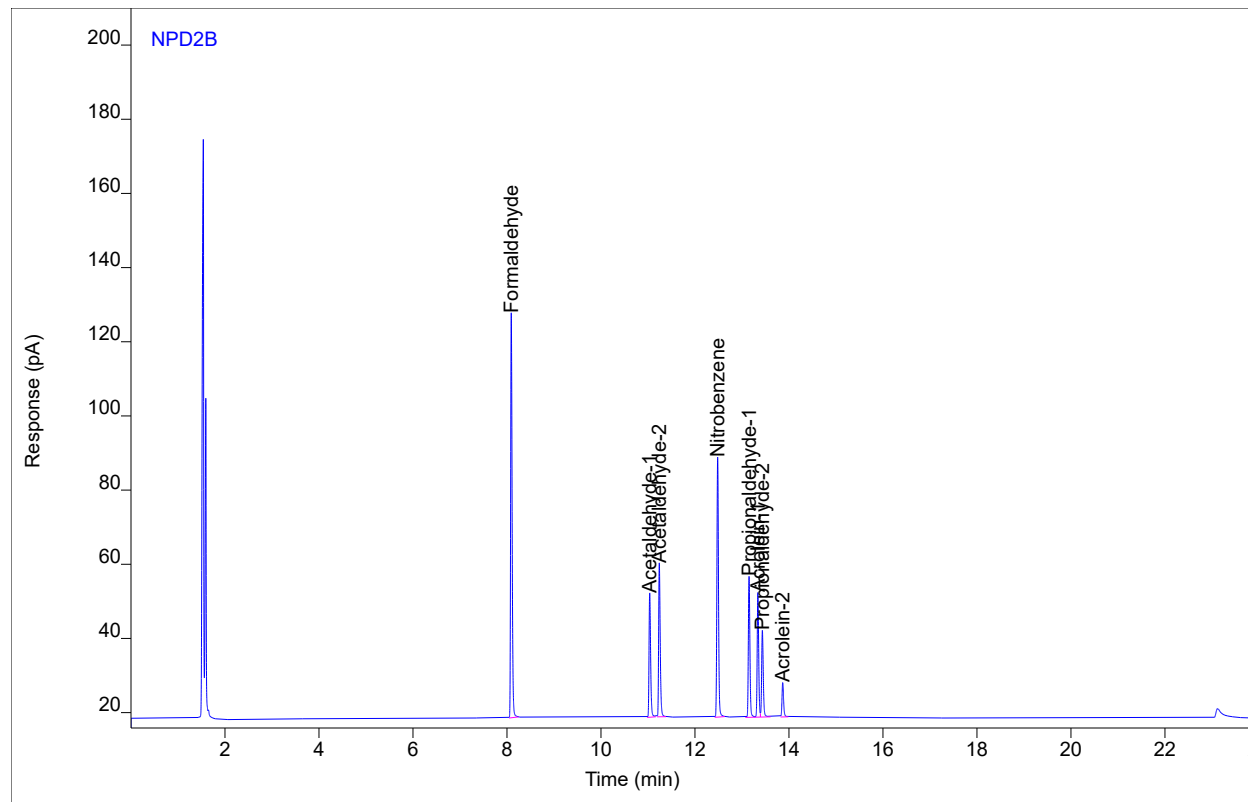
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				5.98543	1	5.98543	
Acrolein	Group				6.36738	1	6.36738	
Propionaldehyde	Group				6.20758	1	6.20758	
Formaldehyde	VB	8.12	248.887	113.390	6.33888	1	6.33888	ug/ml
Acetaldehyde-1	VV	11.06	79.6042	34.4210	2.67612	1	2.67612	ug/ml
Acetaldehyde-2	VV	11.27	98.4393	42.3530	3.30931	1	3.30931	ug/ml
Nitrobenzene	VV	12.51	164.646	70.1012	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.17	89.0694	39.2094	3.78679	1	3.78679	ug/ml
Acrolein-1	VV	13.36	75.5398	34.0534	4.92266	1	4.92266	ug/ml
Propionaldehyde-2	VB	13.46	56.9396	24.1098	2.42079	1	2.42079	ug/ml
Acrolein-2	BB	13.89	22.1698	9.53922	1.44472	1	1.44472	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #3  
 Sequence Name LOLITA0464 ver.1  
 Inj Data File 040B0201.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/24/2023 12:02 PM  
 File Modified 7/25/2023 9:25 AM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type  
 Vial Number 40  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



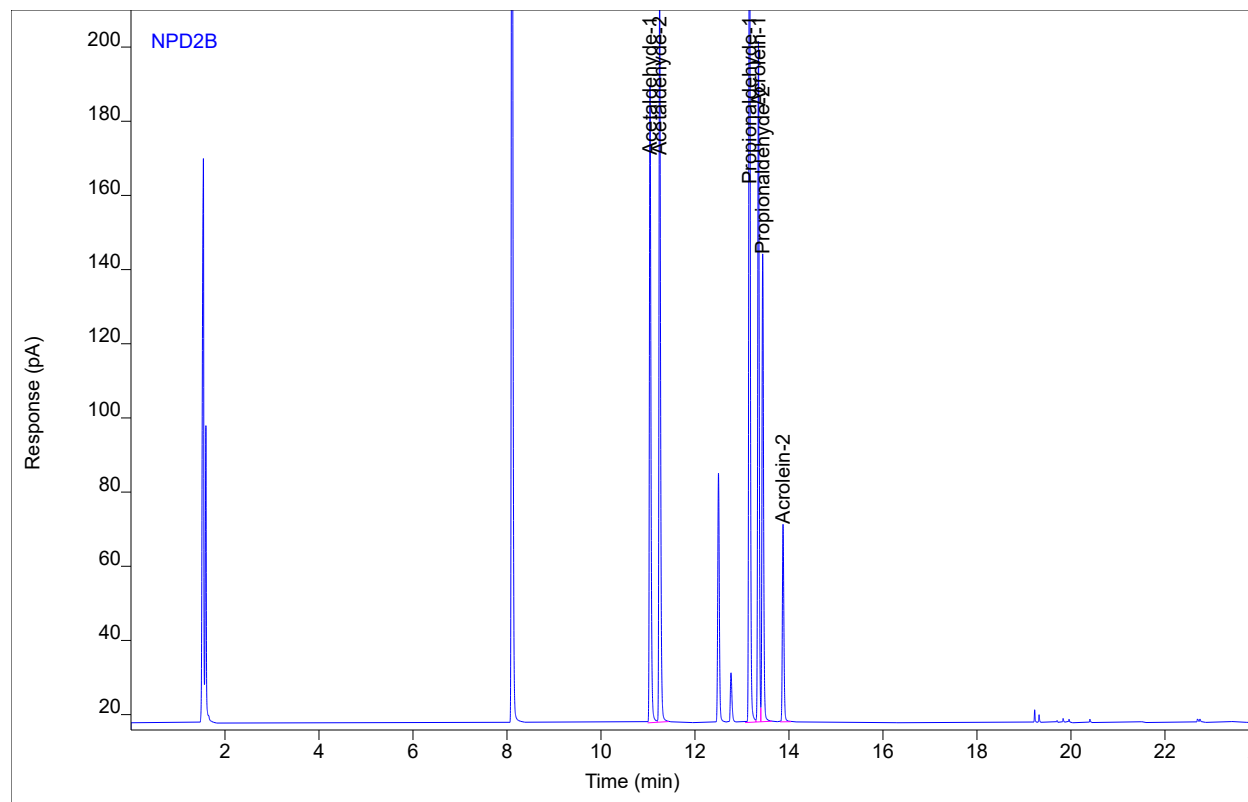
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				5.81766	1	5.81766	
Acrolein	Group				6.23955	1	6.23955	
Propionaldehyde	Group				6.08547	1	6.08547	
Formaldehyde	BB	8.09	238.780	109.203	6.05415	1	6.05415	ug/ml
Acetaldehyde-1	VB	11.04	77.9648	33.5368	2.60924	1	2.60924	ug/ml
Acetaldehyde-2	VB	11.24	95.8689	41.6011	3.20843	1	3.20843	ug/ml
Nitrobenzene	VB	12.48	165.389	70.2024	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.15	87.7750	38.2141	3.71500	1	3.71500	ug/ml
Acrolein-1	VV	13.34	74.3461	33.7667	4.82312	1	4.82312	ug/ml
Propionaldehyde-2	VB	13.43	56.0075	23.3963	2.37047	1	2.37047	ug/ml
Acrolein-2	BB	13.87	21.8336	9.40288	1.41643	1	1.41643	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.F-H-SPK.HEX  
 Sequence Name LOLITA0464 ver.1  
 Inj Data File 042B0401.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/24/2023 1:00 PM  
 File Modified 7/25/2023 9:25 AM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 42  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



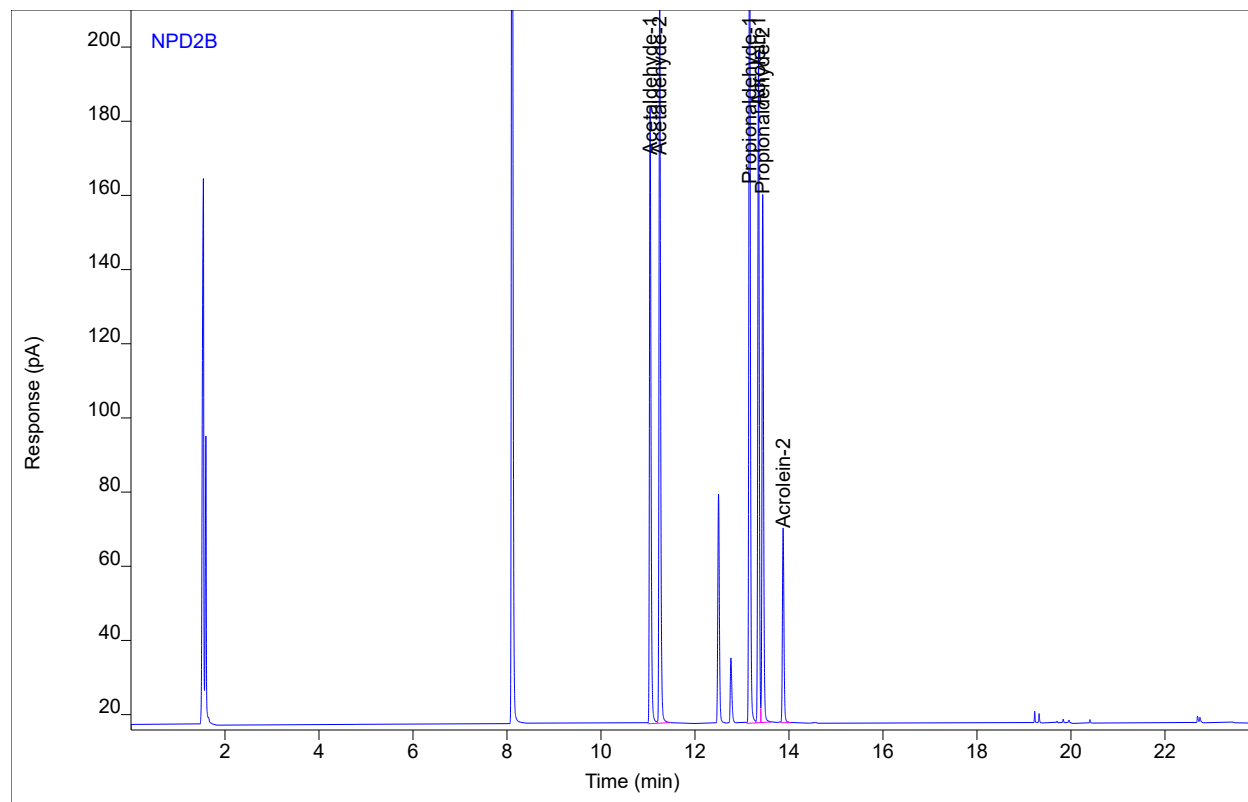
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				30.1567	4	120.627	
Acrolein	Group				35.4572	4	141.829	
Propionaldehyde	Group				38.7969	4	155.188	
Acetaldehyde-1	VV	11.04	393.969	171.993	13.9376	4	55.7506	ug/ml
Acetaldehyde-2	VB	11.25	458.458	198.013	16.2191	4	64.8764	ug/ml
Propionaldehyde-1	BV	13.16	572.396	250.112	25.6093	4	102.437	ug/ml
Acrolein-1	VV	13.35	396.779	183.568	27.2101	4	108.840	ug/ml
Propionaldehyde-2	VB	13.44	294.759	126.153	13.1877	4	52.7506	ug/ml
Acrolein-2	BB	13.87	120.259	53.4011	8.24710	4	32.9884	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.TS.HEX  
 Sequence Name LOLITA0464 ver.1  
 Inj Data File 043B0501.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/24/2023 1:29 PM  
 File Modified 7/25/2023 9:25 AM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 43  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



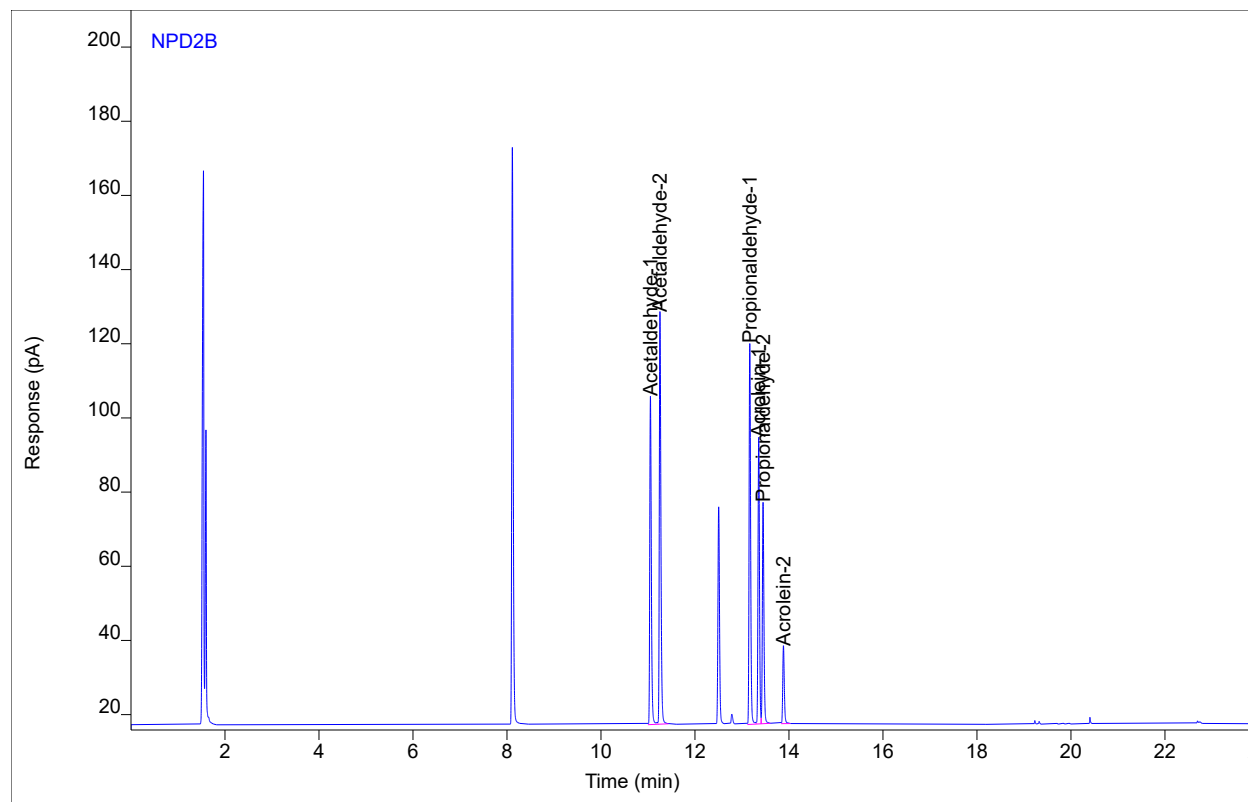
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				32.7481	4	130.993	
Acrolein	Group				38.2834	4	153.134	
Propionaldehyde	Group				42.2666	4	169.066	
Acetaldehyde-1	VV	11.05	382.473	166.512	14.7332	4	58.9327	ug/ml
Acetaldehyde-2	VB	11.25	467.667	202.981	18.0150	4	72.0598	ug/ml
Propionaldehyde-1	BV	13.16	540.329	242.030	26.3225	4	105.290	ug/ml
Acrolein-1	VV	13.35	393.199	180.772	29.3605	4	117.442	ug/ml
Propionaldehyde-2	VB	13.44	327.288	142.391	15.9441	4	63.7762	ug/ml
Acrolein-2	BB	13.88	119.497	52.5564	8.92296	4	35.6919	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name 0623-263.R3-H-SPK.HEX  
 Sequence Name LOLITA0464 ver.1  
 Inj Data File 044B0601.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/24/2023 1:58 PM  
 File Modified 7/25/2023 9:25 AM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 44  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



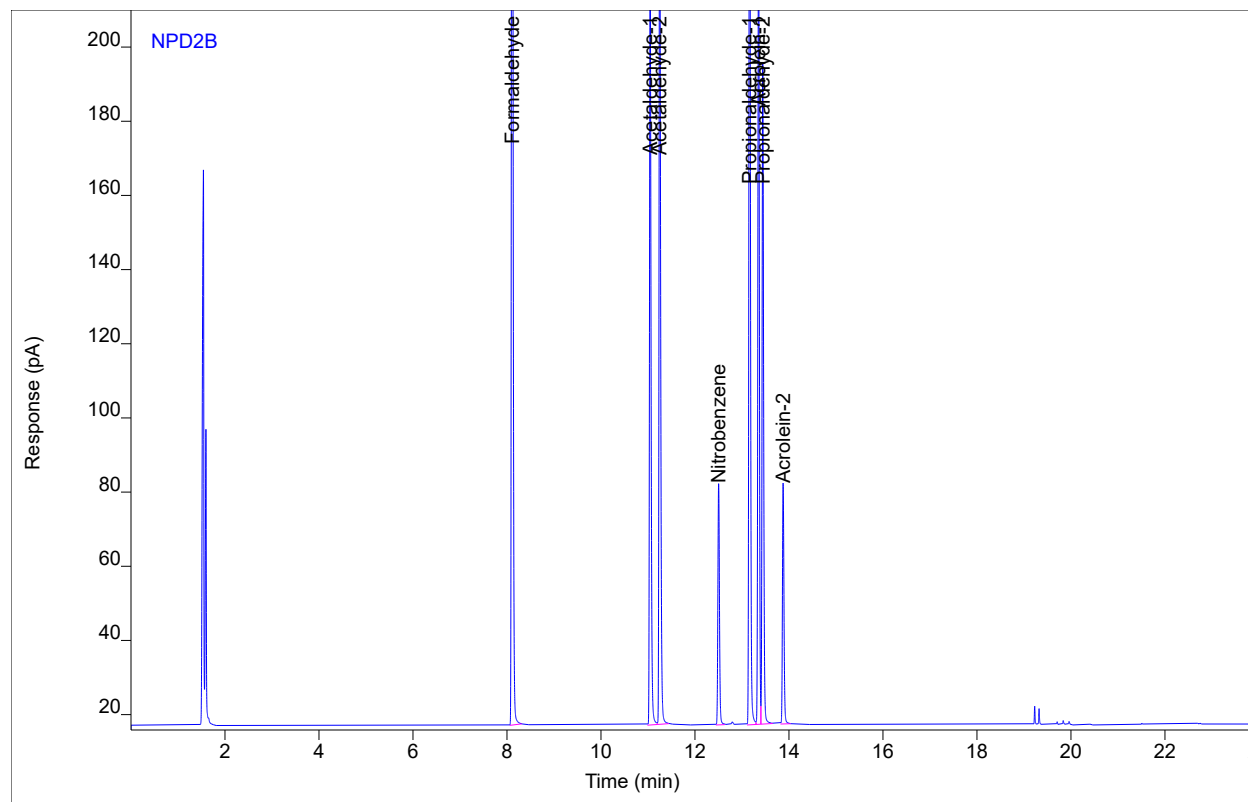
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				18.7448	10	187.448	
Acrolein	Group				16.9553	10	169.553	
Propionaldehyde	Group				18.9087	10	189.087	
Acetaldehyde-1	VB	11.05	204.084	88.5547	8.25613	10	82.5613	ug/ml
Acetaldehyde-2	BB	11.26	259.269	111.393	10.4886	10	104.886	ug/ml
Propionaldehyde-1	BV	13.17	232.856	102.884	11.9132	10	119.132	ug/ml
Acrolein-1	VV	13.36	168.011	77.3233	13.1753	10	131.753	ug/ml
Propionaldehyde-2	VB	13.45	136.734	59.9312	6.99549	10	69.9549	ug/ml
Acrolein-2	BB	13.88	48.2026	21.0482	3.78002	10	37.8002	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcprep5570 #LCS-H-HEX  
 Sequence Name LOLITA0464 ver.1  
 Inj Data File 045B0701.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/24/2023 2:27 PM  
 File Modified 7/25/2023 9:25 AM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type Sample  
 Vial Number Vial 45  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				37.8618	10	378.618	
Acrolein	Group				45.0686	10	450.686	
Propionaldehyde	Group				48.9565	10	489.565	
Formaldehyde	BB	8.11	947.649	438.202	26.3258	10	263.258	ug/ml
Acetaldehyde-1	VV	11.05	468.455	205.772	17.1776	10	171.776	ug/ml
Acetaldehyde-2	VB	11.25	564.087	246.798	20.6842	10	206.842	ug/ml
Nitrobenzene	BV	12.50	150.948	65.2179	10.0000	10	100.000	ug/ml
Propionaldehyde-1	BV	13.16	648.220	290.959	30.0600	10	300.600	ug/ml
Acrolein-1	VV	13.35	487.919	224.075	34.6814	10	346.814	ug/ml
Propionaldehyde-2	VB	13.44	407.488	178.466	18.8965	10	188.965	ug/ml
Acrolein-2	VB	13.88	146.134	65.0541	10.3873	10	103.873	ug/ml

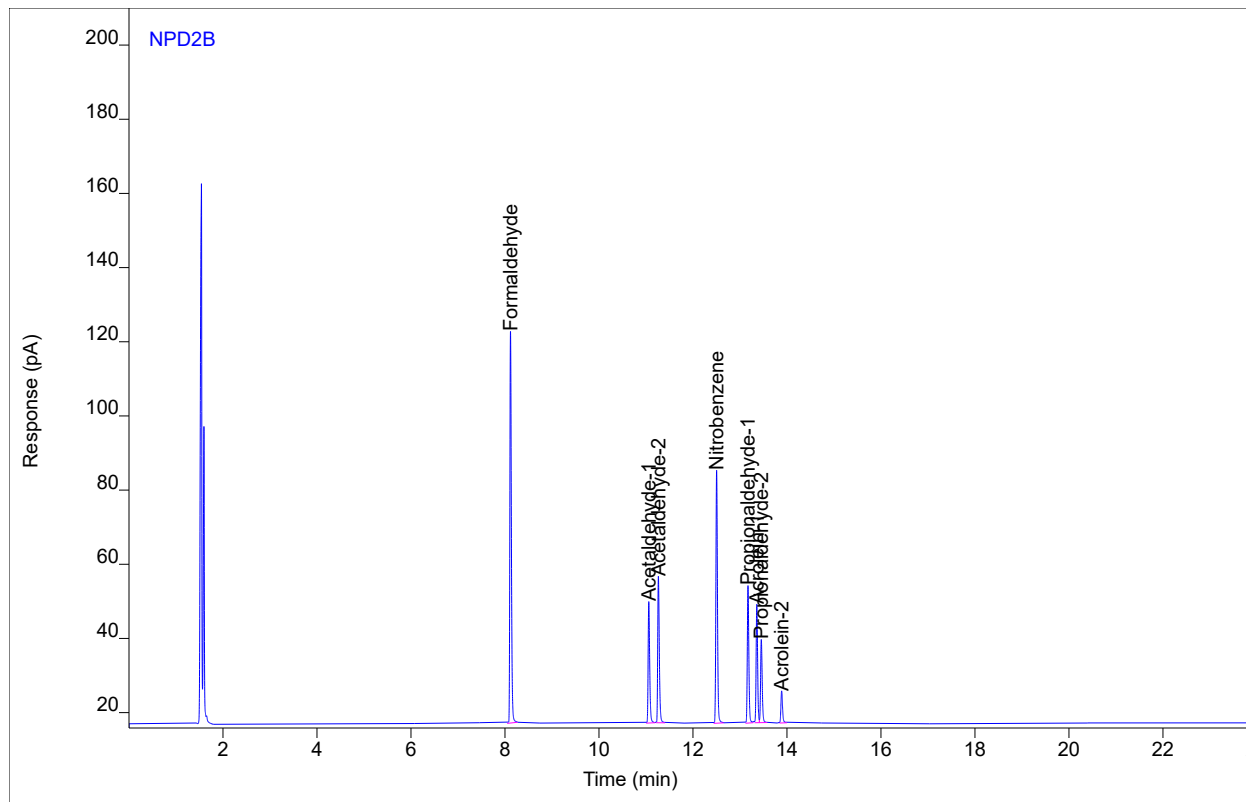


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #3  
 Sequence Name LOLITA0464 ver.1  
 Inj Data File 040B0801.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 7/24/2023 2:56 PM  
 File Modified 7/25/2023 9:26 AM  
 Instrument Lolita  
 Operator Aaron Petersen

Sample Type  
 Vial Number 40  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 7/25/2023 12:44 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				5.85760	1	5.85760	
Acrolein	Group				6.19050	1	6.19050	
Propionaldehyde	Group				6.04048	1	6.04048	
Formaldehyde	VB	8.12	232.166	105.637	6.17116	1	6.17116	ug/ml
Acetaldehyde-1	VB	11.06	74.6896	32.8949	2.62052	1	2.62052	ug/ml
Acetaldehyde-2	BV	11.26	92.2625	39.5139	3.23707	1	3.23707	ug/ml
Nitrobenzene	VB	12.50	157.759	68.3392	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.17	83.2462	37.1908	3.69373	1	3.69373	ug/ml
Acrolein-1	BV	13.36	70.3059	31.9619	4.78161	1	4.78161	ug/ml
Propionaldehyde-2	VB	13.45	52.8890	22.4813	2.34675	1	2.34675	ug/ml
Acrolein-2	BB	13.89	20.7154	8.69140	1.40889	1	1.40889	ug/ml

=====  
 Calibration Table  
 =====

Calib. Data Modified : Monday, June 26, 2023 12:20:37 PM

Rel. Reference Window : 0.000 %  
 Abs. Reference Window : 0.200 min  
 Rel. Non-ref. Window : 0.000 %  
 Abs. Non-ref. Window : 0.200 min  
 Uncalibrated Peaks : not reported  
 Partial Calibration : Yes, identified peaks are recalibrated  
 Correct All Ret. Times: No, only for identified peaks

Curve Type : Average Response/Amount  
 Origin : Ignored  
 Weight : Equal

Recalibration Settings:  
 Average Response : Average all calibrations  
 Average Retention Time: Floating Average New 75%

Calibration Report Options :  
 Printout of recalibrations within a sequence:  
     Calibration Table after Recalibration  
     Normal Report after Recalibration  
 If the sequence is done with bracketing:  
     Results of first cycle (ending previous bracket)

Default Sample ISTD Information (if not set in sample table):

ISTD #	ISTD Amount [ug/ml]	Name
1	100.00000	Nitrobenzene

Signal 1: NPD2 B,

RetTime [min]	Lvl Sig	Amount [ug/ml]	Area	Amt/Area	Ref	Grp	Name
8.138	1 1	4.85074e-1	16.36321	2.96442e-2	1		Formaldehyde
	2	2.52220	83.14323	3.03356e-2			
	3	6.03567	210.03967	2.87359e-2			
	4	12.01158	455.22662	2.63859e-2			
	5	29.58915	1042.53992	2.83818e-2			
	6	57.77000	2076.06104	2.78267e-2			
	7	110.28818	4080.39404	2.70288e-2			
11.085	1 1	2.05061e-1	5.61247	3.65367e-2	1	1	Acetaldehyde-1
	2	1.09480	27.99113	3.91125e-2			
	3	2.62140	68.14464	3.84681e-2			
	4	5.20328	148.62059	3.50105e-2			
	5	12.77683	333.11761	3.83553e-2			
	6	24.90202	661.56635	3.76410e-2			
	7	47.30046	1293.97083	3.65545e-2			
11.291	1 1	2.67939e-1	7.33343	3.65367e-2	1	1	Acetaldehyde-2

RetTime [min]	Lvl Sig	Amount [ug/ml]	Area	Amt/Area	Ref	Grp Name
	2	1.36720	34.95557	3.91125e-2		
	3	3.26960	84.99519	3.84681e-2		
	4	6.52072	186.25031	3.50105e-2		
	5	16.10417	419.86819	3.83553e-2		
	6	31.48498	836.45410	3.76410e-2		
	7	60.34954	1650.94678	3.65545e-2		
12.514	1	100.00000	144.90929	6.90087e-1	I1	Nitrobenzene
	2	100.00000	143.58173	6.96467e-1		
	3	100.00000	144.10732	6.93927e-1		
	4	100.00000	159.96103	6.25152e-1		
	5	100.00000	146.16470	6.84160e-1		
	6	100.00000	147.56770	6.77655e-1		
	7	100.00000	151.67018	6.59325e-1		
13.191	1	2.81412e-1	6.02810	4.66833e-2	1	2 Propionaldehyde-1
	2	1.52720	30.07953	5.07721e-2		
	3	3.65560	76.35092	4.78789e-2		
	4	7.23230	162.19019	4.45915e-2		
	5	17.77151	368.06042	4.82842e-2		
	6	34.59930	733.82892	4.71490e-2		
	7	65.51278	1435.39624	4.56409e-2		
13.377	1	3.88994e-1	5.12206	7.59449e-2	1	3 Acrolein-1
	2	1.97084	25.57232	7.70692e-2		
	3	4.79562	65.14576	7.36137e-2		
	4	9.49384	140.42151	6.76096e-2		
	5	23.40001	320.67676	7.29707e-2		
	6	45.64961	640.73010	7.12462e-2		
	7	86.85206	1258.95776	6.89873e-2		
13.476	1	2.00588e-1	4.29678	4.66833e-2	1	2 Propionaldehyde-2
	2	9.80800e-1	19.31771	5.07721e-2		
	3	2.34440	48.96522	4.78789e-2		
	4	4.71070	105.64125	4.45915e-2		
	5	11.65049	241.28981	4.82842e-2		
	6	22.84370	484.50018	4.71490e-2		
	7	44.14722	967.27332	4.56409e-2		
13.906	1	1.10006e-1	1.44849	7.59449e-2	1	3 Acrolein-2
	2	6.22161e-1	8.07276	7.70692e-2		
	3	1.41038	19.15918	7.36137e-2		
	4	2.85616	42.24499	6.76096e-2		
	5	7.02399	96.25770	7.29707e-2		
	6	13.75039	192.99820	7.12462e-2		
	7	26.54794	384.82370	6.89873e-2		

## Group summary :

## Group 1 ( Acetaldehyde ) :

## Group members:

Acetaldehyde-1 with retention time 11.085 min

Acetaldehyde-2 with retention time 11.291 min

## Group Amount Calculation:

Level 1 with amount 0.47300 ug/ml

Level 2 with amount 2.46200 ug/ml

Level 3 with amount 5.89100 ug/ml

Level 4 with amount 11.72400 ug/ml

Level 5 with amount 28.88100 ug/ml

Level 6 with amount 56.38700 ug/ml

Level 7 with amount 107.65000 ug/ml  
 Group 2 ( Propionaldehyde ) :  
 Group members:  
 Propionaldehyde-1 with retention time 13.191 min  
 Propionaldehyde-2 with retention time 13.476 min

Group Amount Calculation:  
 Level 1 with amount 0.48200 ug/ml  
 Level 2 with amount 2.50800 ug/ml  
 Level 3 with amount 6.00000 ug/ml  
 Level 4 with amount 11.94300 ug/ml  
 Level 5 with amount 29.42200 ug/ml  
 Level 6 with amount 57.44300 ug/ml  
 Level 7 with amount 109.66000 ug/ml

Group 3 ( Acrolein ) :  
 Group members:  
 Acrolein-1 with retention time 13.377 min  
 Acrolein-2 with retention time 13.906 min

Group Amount Calculation:  
 Level 1 with amount 0.49900 ug/ml  
 Level 2 with amount 2.59300 ug/ml  
 Level 3 with amount 6.20600 ug/ml  
 Level 4 with amount 12.35000 ug/ml  
 Level 5 with amount 30.42400 ug/ml  
 Level 6 with amount 59.40000 ug/ml  
 Level 7 with amount 113.40000 ug/ml

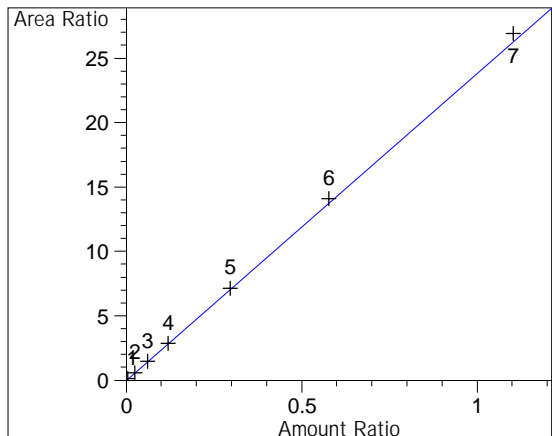
2 Warnings or Errors :

Warning : Overlapping peak time windows at 13.191 min, signal 1  
 Warning : Overlapping peak time windows at 13.377 min, signal 1

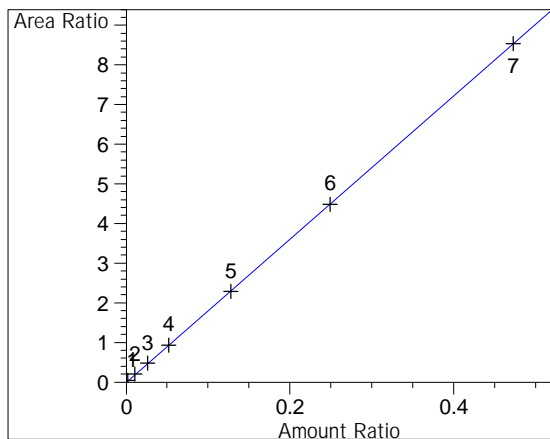
=====  
 Peak Sum Table  
 =====

\*\*\*No Entries in table\*\*\*

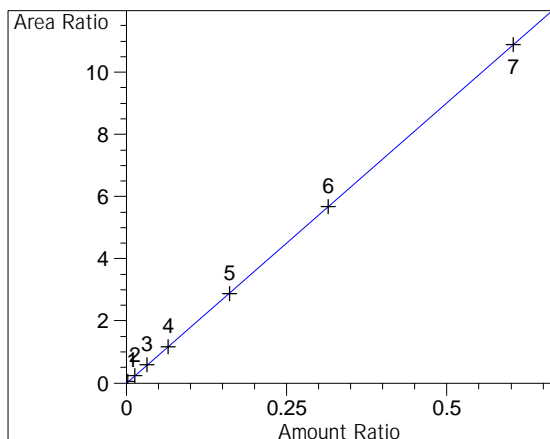
=====  
 Calibration Curves  
 =====



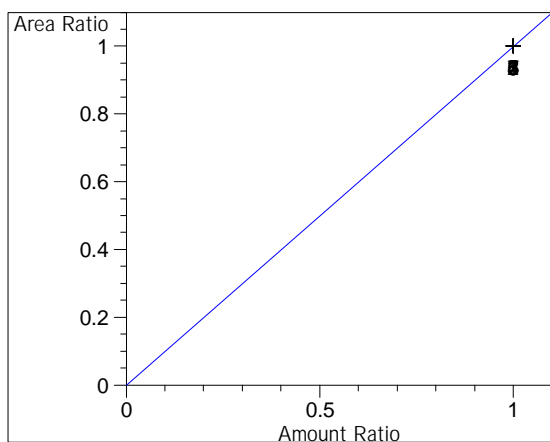
Formaldehyde at exp. RT: 8.138  
 NPD2 B,  
 Correlation: 0.99999  
 Residual Std. Dev.: 0.30172  
 Formula:  $y = mx$   
 m: 23.84722  
 x: Amount  
 y: Area



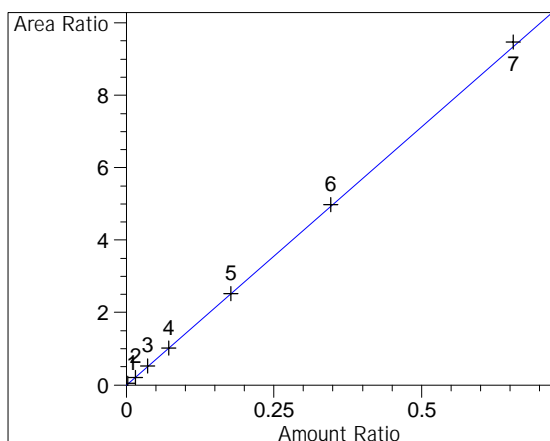
Acetaldehyde-1 at exp. RT: 11.085  
 NPD2 B,  
 Correlation: 1.00000  
 Residual Std. Dev.: 0.01697  
 Formula:  $y = mx$   
 m: 18.06668  
 x: Amount  
 y: Area



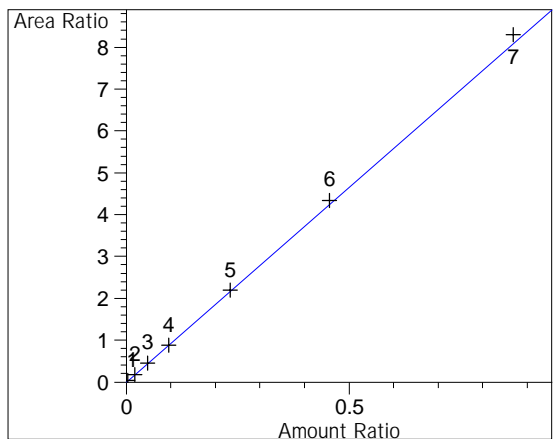
Acetaldehyde-2 at exp. RT: 11.291  
 NPD2 B,  
 Correlation: 1.00000  
 Residual Std. Dev.: 0.02143  
 Formula:  $y = mx$   
 m: 18.06668  
 x: Amount  
 y: Area



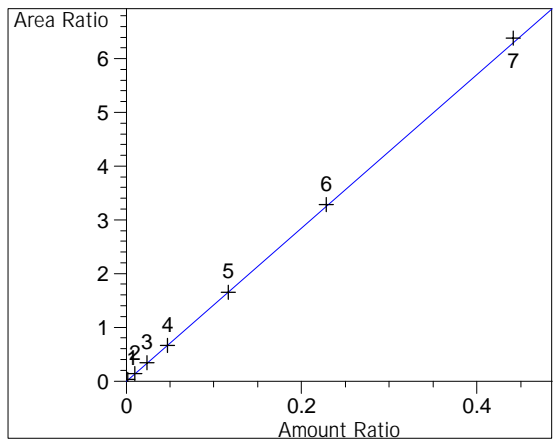
Nitrobenzene at exp. RT: 12.514  
 NPD2 B,  
 Correlation: 1.00000  
 Residual Std. Dev.: 0.00000  
 Formula:  $y = mx$   
 m: 1.00000  
 x: Amount  
 y: Area



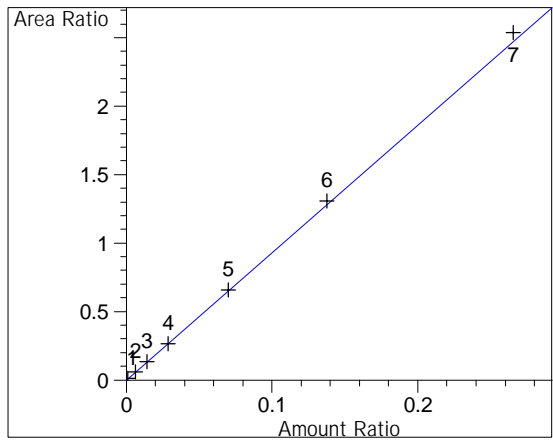
Propionaldehyde-1 at exp. RT: 13.191  
 NPD2 B,  
 Correlation: 0.99998  
 Residual Std. Dev.: 0.05067  
 Formula:  $y = mx$   
 m: 14.28582  
 x: Amount  
 y: Area



Acrolein-1 at exp. RT: 13.377  
NPD2 B,  
Correlation: 0.99999  
Residual Std. Dev.: 0.10028  
Formula:  $y = mx$   
m: 9.32017  
x: Amount  
y: Area



Propionaldehyde-2 at exp. RT: 13.476  
NPD2 B,  
Correlation: 0.99998  
Residual Std. Dev.: 0.03402  
Formula:  $y = mx$   
m: 14.28582  
x: Amount  
y: Area



Acrolein-2 at exp. RT: 13.906  
NPD2 B,  
Correlation: 0.99999  
Residual Std. Dev.: 0.03058  
Formula:  $y = mx$   
m: 9.32017  
x: Amount  
y: Area

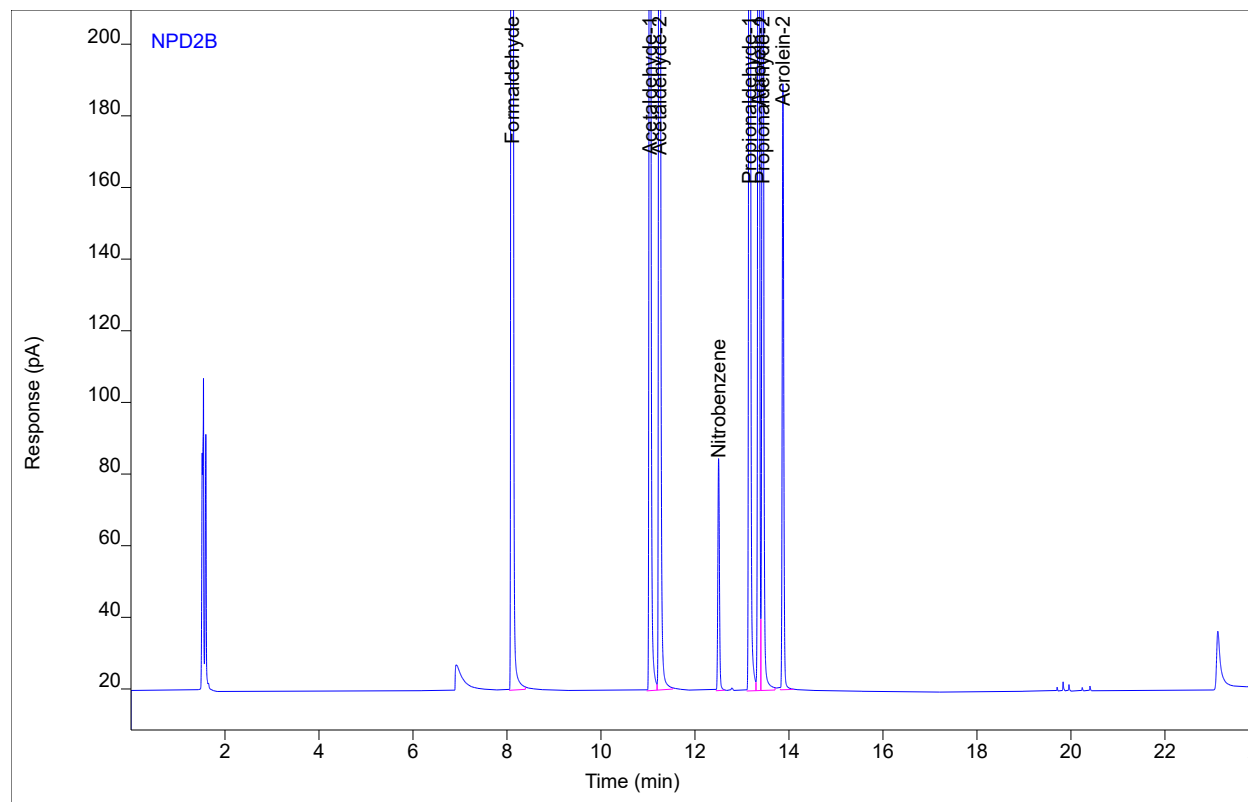
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# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #7  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 026B0201.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 10:22 AM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type  
 Vial Number Vial 26  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



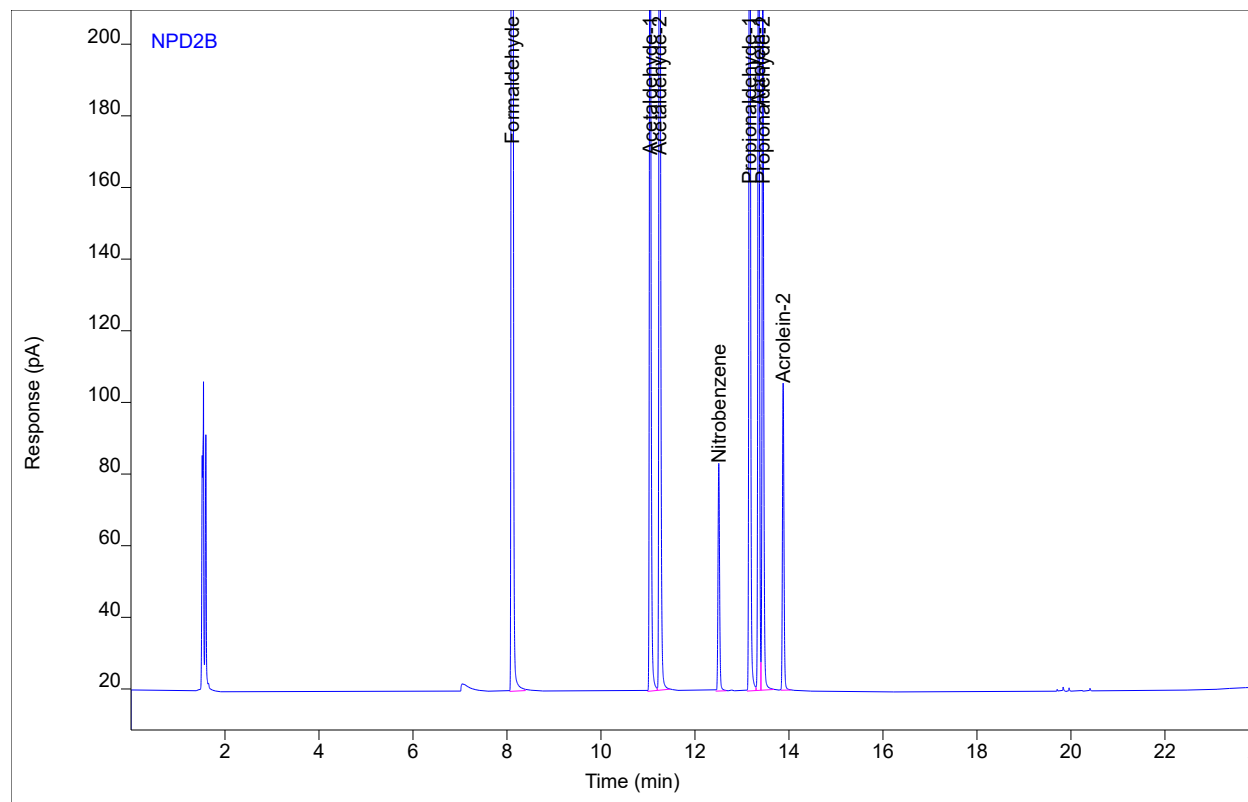
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				107.472	1	107.472	
Acrolein	Group				116.284	1	116.284	
Propionaldehyde	Group				110.889	1	110.889	
Formaldehyde	VV	8.11	4080.39	1843.91	112.814	1	112.814	ug/ml
Acetaldehyde-1	VV	11.04	1293.97	560.848	47.2222	1	47.2222	ug/ml
Acetaldehyde-2	VV	11.25	1650.95	720.260	60.2496	1	60.2496	ug/ml
Nitrobenzene	VV	12.50	151.670	64.9038	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.16	1435.40	623.964	66.2470	1	66.2470	ug/ml
Acrolein-1	VV	13.36	1258.96	566.521	89.0609	1	89.0609	ug/ml
Propionaldehyde-2	VV	13.44	967.273	414.382	44.6420	1	44.6420	ug/ml
Acrolein-2	BB	13.87	384.824	169.198	27.2231	1	27.2231	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #6  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 027B0301.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 10:51 AM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type  
 Vial Number Vial 27  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				56.1886	1	56.1886	
Acrolein	Group				60.6191	1	60.6191	
Propionaldehyde	Group				57.7921	1	57.7921	
Formaldehyde	BB	8.11	2076.06	959.118	58.9944	1	58.9944	ug/ml
Acetaldehyde-1	VV	11.05	661.566	291.454	24.8144	1	24.8144	ug/ml
Acetaldehyde-2	VB	11.25	836.454	363.290	31.3742	1	31.3742	ug/ml
Nitrobenzene	VB	12.51	147.568	63.6662	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.16	733.829	317.726	34.8095	1	34.8095	ug/ml
Acrolein-1	VV	13.36	640.730	294.351	46.5865	1	46.5865	ug/ml
Propionaldehyde-2	VB	13.44	484.500	207.527	22.9825	1	22.9825	ug/ml
Acrolein-2	BB	13.88	192.998	85.7424	14.0326	1	14.0326	ug/ml

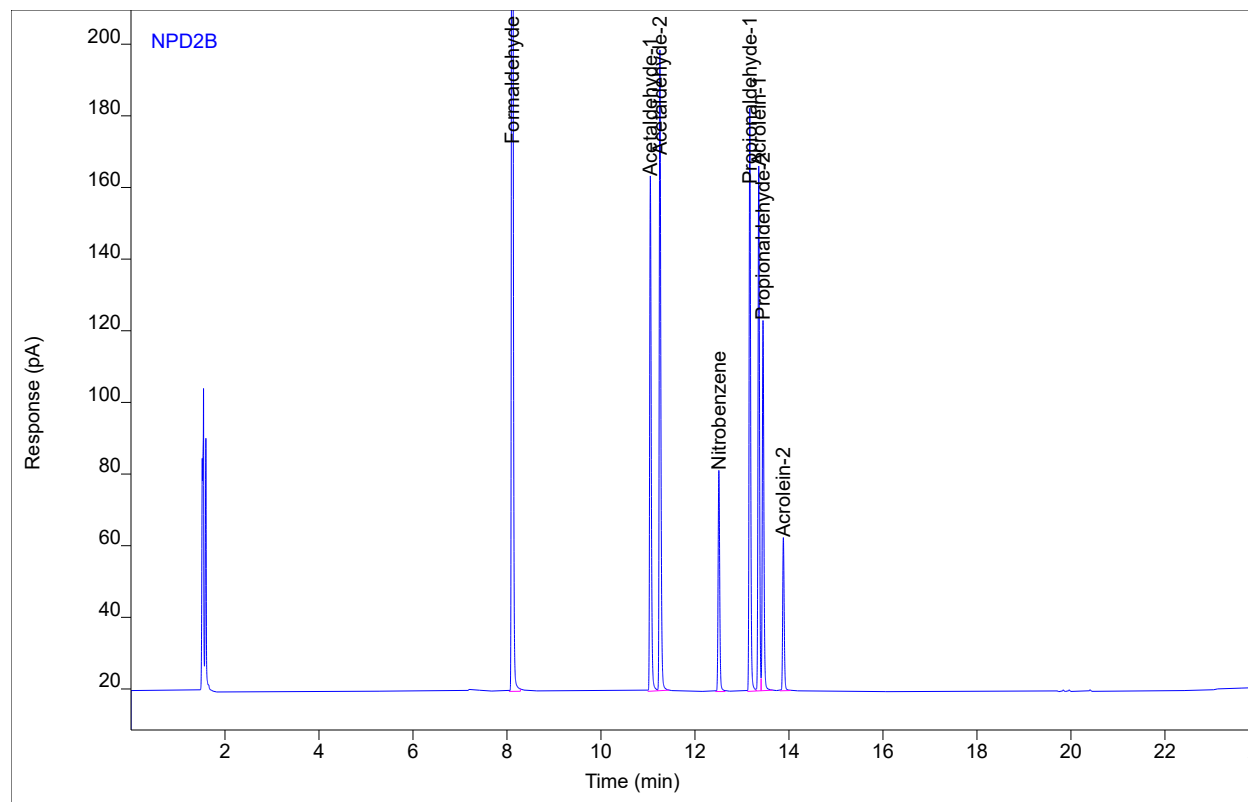


# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #5  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 028B0401.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 11:20 AM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type  
 Vial Number Vial 28  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



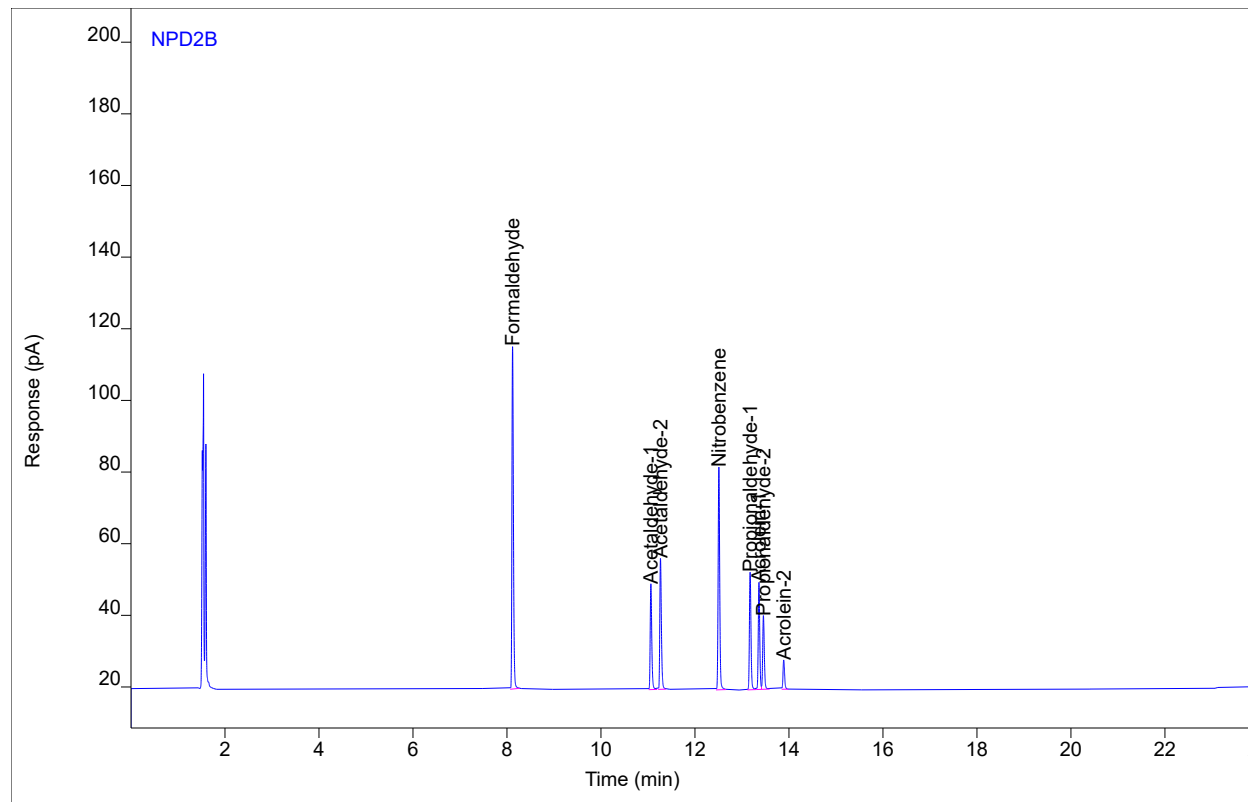
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				28.5145	1	28.5145	
Acrolein	Group				30.6056	1	30.6056	
Propionaldehyde	Group				29.1823	1	29.1823	
Formaldehyde	BV	8.11	1042.54	477.407	29.9097	1	29.9097	ug/ml
Acetaldehyde-1	VV	11.05	333.118	143.865	12.6147	1	12.6147	ug/ml
Acetaldehyde-2	VB	11.25	419.868	178.935	15.8998	1	15.8998	ug/ml
Nitrobenzene	VB	12.51	146.165	61.9394	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.17	368.060	162.822	17.6267	1	17.6267	ug/ml
Acrolein-1	VV	13.36	320.677	146.582	23.5397	1	23.5397	ug/ml
Propionaldehyde-2	VB	13.45	241.290	103.539	11.5556	1	11.5556	ug/ml
Acrolein-2	BB	13.88	96.2577	42.9174	7.06593	1	7.06593	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #3  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 029B0501.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 11:49 AM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type  
 Vial Number  
 Injection Volume  
 Injection  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



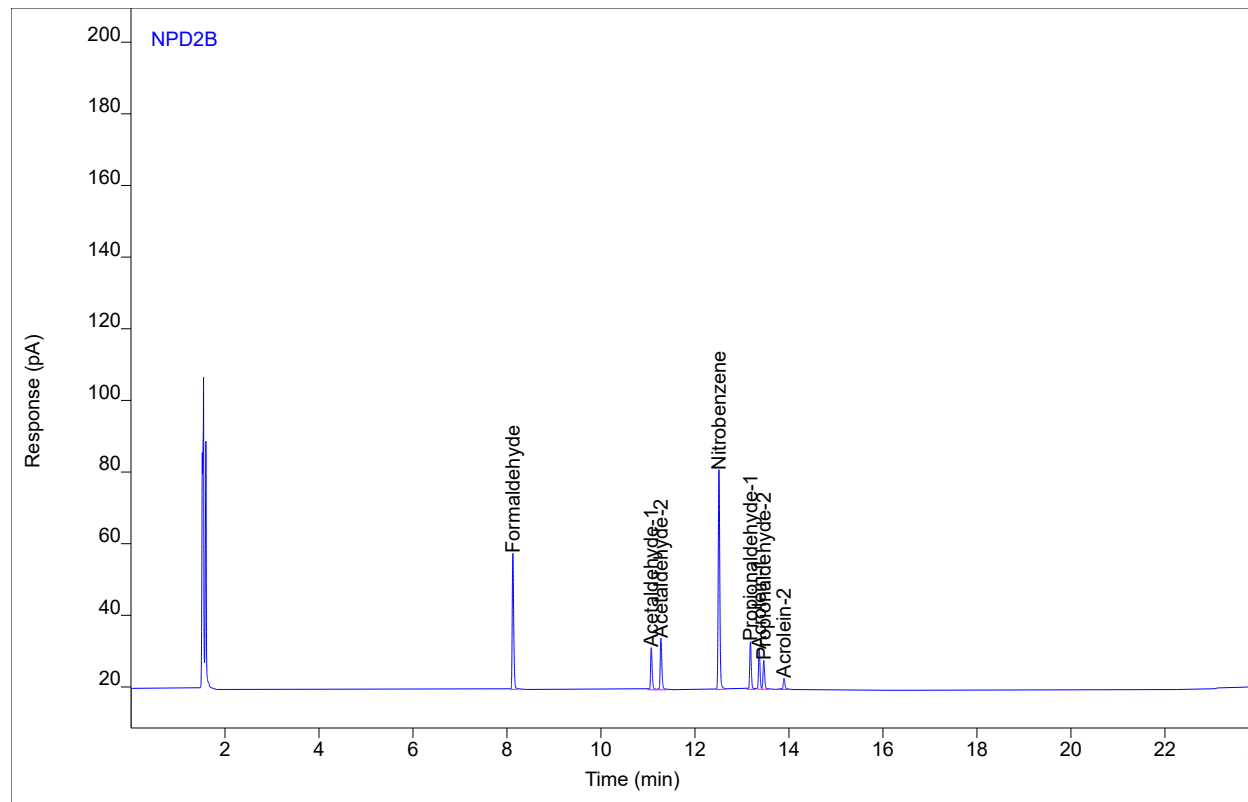
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				5.88198	1	5.88198	
Acrolein	Group				6.27687	1	6.27687	
Propionaldehyde	Group				6.08718	1	6.08718	
Formaldehyde	VB	8.12	210.040	95.7618	6.11192	1	6.11192	ug/ml
Acetaldehyde-1	VV	11.06	68.1446	29.5525	2.61738	1	2.61738	ug/ml
Acetaldehyde-2	VV	11.27	84.9952	36.6892	3.26460	1	3.26460	ug/ml
Nitrobenzene	VB	12.51	144.107	62.1817	100.000	1	100.000	ug/ml
Propionaldehyde-1	VB	13.17	76.3509	32.8412	3.70871	1	3.70871	ug/ml
Acrolein-1	BV	13.36	65.1458	29.8954	4.85039	1	4.85039	ug/ml
Propionaldehyde-2	VB	13.46	48.9652	20.5938	2.37846	1	2.37846	ug/ml
Acrolein-2	BB	13.89	19.1592	8.25773	1.42649	1	1.42649	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #2  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 030B0601.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 12:18 PM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type  
 Vial Number Vial 30  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



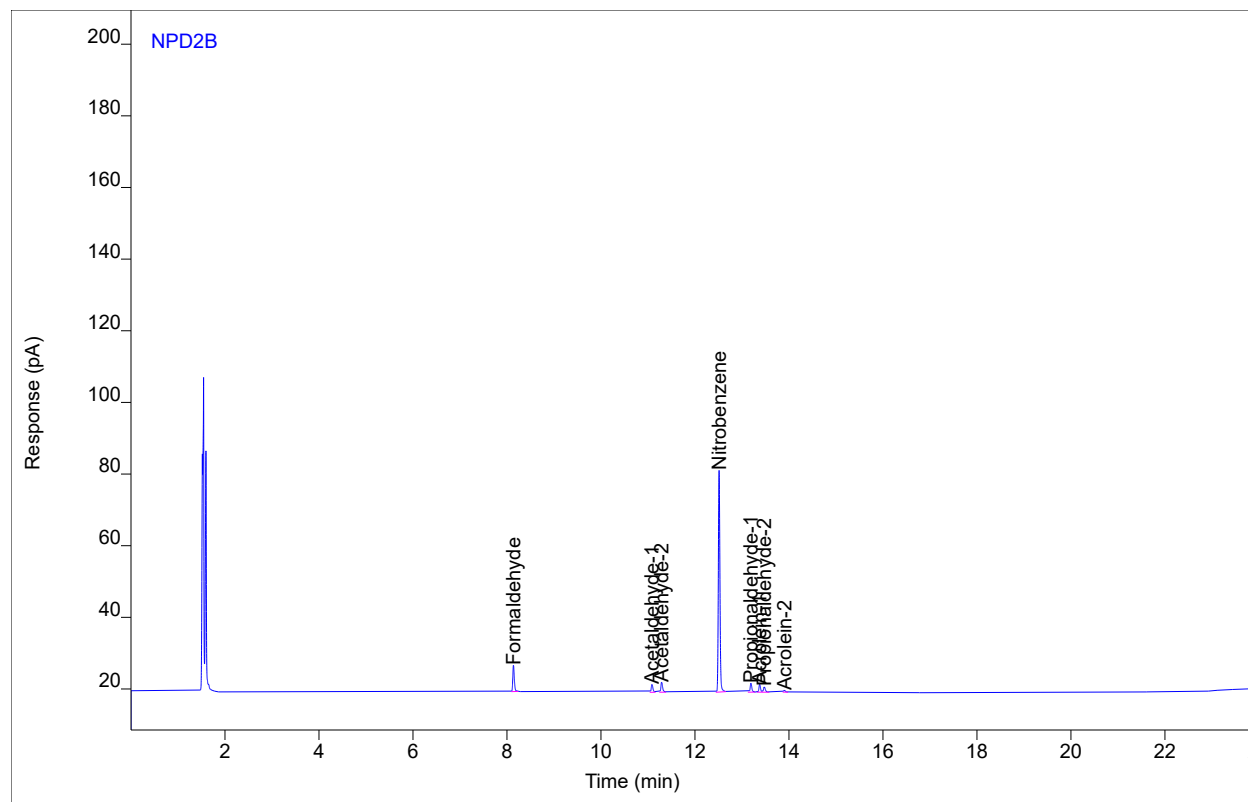
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				2.42658	1	2.42658	
Acrolein	Group				2.51419	1	2.51419	
Propionaldehyde	Group				2.40823	1	2.40823	
Formaldehyde	VV	8.13	83.1432	38.0845	2.42823	1	2.42823	ug/ml
Acetaldehyde-1	BB	11.07	27.9911	11.9303	1.07905	1	1.07905	ug/ml
Acetaldehyde-2	VV	11.27	34.9556	14.5657	1.34753	1	1.34753	ug/ml
Nitrobenzene	VB	12.51	143.582	61.3882	100.000	1	100.000	ug/ml
Propionaldehyde-1	BB	13.18	30.0795	13.4257	1.46645	1	1.46645	ug/ml
Acrolein-1	BV	13.37	25.5723	11.3739	1.91094	1	1.91094	ug/ml
Propionaldehyde-2	VB	13.46	19.3177	8.10659	0.94178	1	0.94178	ug/ml
Acrolein-2	BB	13.89	8.07276	3.27842	0.60325	1	0.60325	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1919 #1  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 031B0701.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 12:47 PM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type  
 Vial Number  
 Injection Volume  
 Injection  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



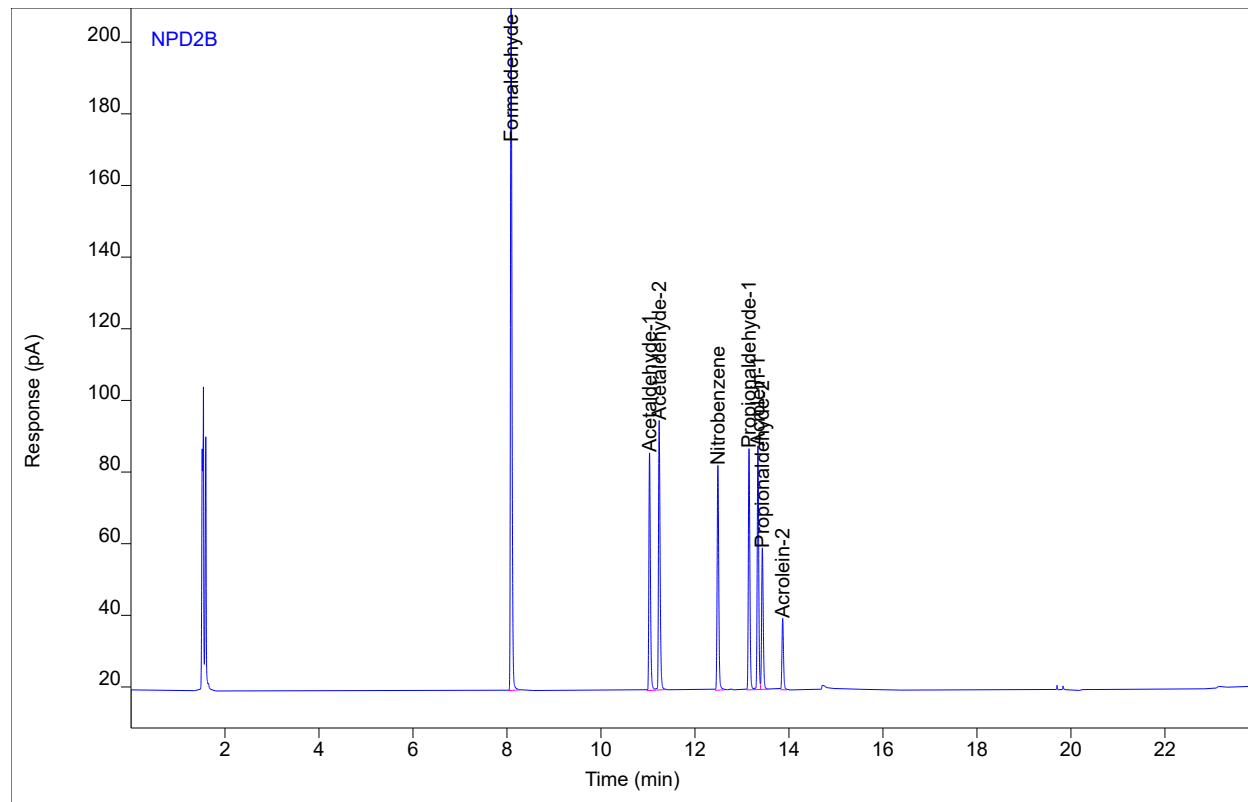
Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				0.49449	1	0.49449	
Acrolein	Group				0.48650	1	0.48650	
Propionaldehyde	Group				0.49875	1	0.49875	
Formaldehyde	VB	8.14	16.3632	7.37617	0.47352	1	0.47352	ug/ml
Acetaldehyde-1	VV	11.09	5.61247	2.30031	0.21438	1	0.21438	ug/ml
Acetaldehyde-2	VV	11.29	7.33343	2.92859	0.28011	1	0.28011	ug/ml
Nitrobenzene	VB	12.51	144.909	62.0119	100.000	1	100.000	ug/ml
Propionaldehyde-1	VB	13.19	6.02810	2.53665	0.29119	1	0.29119	ug/ml
Acrolein-1	BV	13.38	5.12206	2.19135	0.37925	1	0.37925	ug/ml
Propionaldehyde-2	VB	13.48	4.29678	1.65644	0.20756	1	0.20756	ug/ml
Acrolein-2	BB	13.91	1.44849	0.60144	0.10725	1	0.10725	ug/ml

# Chromatogram Report

# Enthalpy Analytical

Sample Name gcstds1949 #3ss  
 Sequence Name LOLITA0458 ver.5  
 Inj Data File 032B0801.D  
 File Location GC/2023/Lolita/Quarter 2  
 Injection Date 6/22/2023 2:12 PM  
 File Modified 6/26/2023 2:04 PM  
 Instrument Lolita  
 Operator Daniel Clayton

Sample Type Control  
 Vial Number Vial 32  
 Injection Volume 1  
 Injection 1 of 1  
 Acquisition Method LOLITA0349X.M  
 Analysis Method LOLITA0458\_NPD.M  
 Method Modified 6/26/2023 12:20 PM  
 Printed 6/26/2023 3:49 PM



Compound	Type	RT	Area	Height	Amount	DF	SampAmt	Unit
Acetaldehyde	Group				12.2762	1	12.2762	
Acrolein	Group				14.2343	1	14.2343	
Propionaldehyde	Group				11.6063	1	11.6063	
Formaldehyde	VB	8.09	436.333	200.067	12.3338	1	12.3338	ug/ml
Acetaldehyde-1	VV	11.03	152.029	66.4511	5.67234	1	5.67234	ug/ml
Acetaldehyde-2	VV	11.24	176.995	75.4092	6.60386	1	6.60386	ug/ml
Nitrobenzene	BV	12.49	148.349	62.8746	100.000	1	100.000	ug/ml
Propionaldehyde-1	BV	13.15	151.982	67.4759	7.17138	1	7.17138	ug/ml
Acrolein-1	VV	13.34	151.234	68.0700	10.9381	1	10.9381	ug/ml
Propionaldehyde-2	VB	13.43	93.9878	39.5166	4.43487	1	4.43487	ug/ml
Acrolein-2	BV	13.87	45.5746	20.0123	3.29620	1	3.29620	ug/ml

**This Is The Last Page  
Of This Report.**



**APPENDIX F**

**CALIBRATION DATA**

# Advanced Industrial Resources, Inc.

## Dry Gas Meter Calibration Data

Dry Gas Meter	
Console ID:	C-004
Serial Number:	229883

Reference Meter	
Meter ID:	M5RFM1
Calibration Factor, $Y_w$ :	0.995

Date: 08/03/22                      Performed By: DJK  
 Barometric Pressure,  $P_b$  (in. Hg): 29.88                      Reviewed By: DPS

Data								
Vacuum (in. Hg)	$\Delta H$ (in. H <sub>2</sub> O)	Reference Meter Volume $V_w$ (ft <sup>3</sup> )	Dry Gas Meter Volume $V_m$ (ft <sup>3</sup> )	Temperatures (°F)			Time Elapsed $\theta$ (min.)	
				Reference Meter $t_w$	Dry Gas Meter			
					init. $t_i$	final $t_f$		avg. $t_m$
7.5	0.50	5.393	5.255	77	82.0	87.0	84.5	12.50
7.5	1.00	6.562	6.472	77	87.0	92.0	89.5	11.00
7.5	2.00	5.655	5.678	77	91.0	94.0	92.5	7.00
7.5	3.00	5.941	5.956	77	92.0	97.0	94.5	6.00
7.5	4.00	5.632	5.634	77	95.0	99.0	97.0	5.00

Calculations						
$\Delta H$ (inches H <sub>2</sub> O)	$Y_m$ Variation			$\Delta H_{@}$ Variation		
	(dimensionless)			(inches H <sub>2</sub> O)                      (dimensionless)		
0.50	1.034	0.011		1.524	-0.130	
1.00	1.030	0.006		1.580	-0.074	
2.00	1.015	-0.009		1.714	0.059	
3.00	1.017	-0.006		1.705	0.051	
4.00	1.022	-0.002		1.749	0.094	
<b>Averages:</b>	<b>1.023</b>			<b>1.655</b>		

Where:

$Y_m$  is the ratio of the reading of the reference meter to that of the dry gas meter (DGM); variance limit:  $\pm 0.02$ .

$$Y_m = \frac{Y_w V_w P_b (t_m + 460)}{V_m (P_b + \Delta H/13.6) (t_w + 460)}$$

$\Delta H_{@}$  is the orifice pressure differential (inches H<sub>2</sub>O) that corresponds to 0.75 cfm of air at 68 °F and 29.92 inches of mercury; variance limit:  $\pm 0.20$ .

$$\Delta H_{@} = \frac{0.0317 \Delta H ((t_w + 460) \theta)^2}{P_b (t_m + 460) (Y_w V_w)^2}$$



EMC Approved Alternative Method (EMC ALT-009)  
Alternative Method 5 Post-test Calibration

**Console ID:** C-004

**DGM  $Y_m$ :** 1.023

**$\Delta H_{@}$**  1.655

**Source:** Carbon Bed Outlet

**Methods:** 1, 2, 3, 4, 25A, NACSI 105.01

orifice meter calibration coefficient, in. H<sub>2</sub>O.

	1	2	3	
<b>Run #</b>	1	2	3	
<b>Test Date</b>	7/12/23	7/12/23	7/12/23	
<b>Test time</b>	144	134	143	total run time, min.
<b>V<sub>m</sub></b>	106.298	96.244	103.832	total sample volume measured by dry gas meter, dcf.
<b>T<sub>m</sub></b>	532	535	535	absolute average dry gas meter temp., BR.
<b>P<sub>b</sub></b>	30.12	30.12	30.12	barometric pressure, in. Hg.
<b><math>\Delta H_{avg}</math></b>	1.71	1.71	1.71	average orifice meter differential, in. H <sub>2</sub> O.
<b>M<sub>d-stack gas</sub></b>	28.84	28.84	28.84	dry molecular weight of stack gas, lb/lb-mole.
<b>Y<sub>qa</sub></b>	1.036	1.067	1.052	dry gas meter calibration check value, dimensionless.
<b>K</b>	0.0319	0.0319	0.0319	(29.92/528)(0.75) <sup>2</sup> (in. Hg/B/R) cfm <sup>2</sup> .
<b>M<sub>d-air</sub></b>	29	29	29	dry molecular weight of air, lb/lb-mole.
<b>Hg<sub>SG</sub></b>	13.6	13.6	13.6	specific gravity of mercury.
<b>% diff. from <math>Y_m</math></b>	-1.2%	-4.3%	-2.9%	

**Average % diff. from  $Y_m$ :** -2.8%

**Calibration check value status:** PASS

\*Post-test DGM calibration check value ( $Y_{qa}$ ) must be within  $\pm 5\%$  of the specific DGM's established  $Y_m$



EMC Approved Alternative Method (EMC ALT-009)  
Alternative Method 5 Post-test Calibration

**Console ID:** C-009

**DGM  $Y_m$ :** 1.013

**$\Delta H_{@}$**  1.554

**Source:** Carbon Bed Outlet

**Method:** 1, 2, 3, 4, 25A, NACSI 105.01

orifice meter calibration coefficient, in. H<sub>2</sub>O.

	1	2	3	
<b>Run #</b>	1	2	3	
<b>Test Date</b>	7/12/23	7/12/23	7/12/23	
<b>Test time</b>	144	134	144	total run time, min.
<b>V<sub>m</sub></b>	108.425	98.778	106.568	total sample volume measured by dry gas meter, dcf.
<b>T<sub>m</sub></b>	525	533	535	absolute average dry gas meter temp., BR.
<b>P<sub>b</sub></b>	30.12	30.12	30.12	barometric pressure, in. Hg.
<b><math>\Delta H_{avg}</math></b>	1.56	1.56	1.55	average orifice meter differential, in. H <sub>2</sub> O.
<b>M<sub>d-stack gas</sub></b>	28.84	28.84	28.84	dry molecular weight of stack gas, lb/lb-mole.
<b>Y<sub>qa</sub></b>	0.993	1.021	1.018	dry gas meter calibration check value, dimensionless.
<b>K</b>	0.0319	0.0319	0.0319	(29.92/528)(0.75) <sup>2</sup> (in. Hg/B/R) cfm <sup>2</sup> .
<b>M<sub>d-air</sub></b>	29	29	29	dry molecular weight of air, lb/lb-mole.
<b>Hg<sub>SG</sub></b>	13.6	13.6	13.6	specific gravity of mercury.
<b>% diff. from <math>Y_m</math></b>	1.9%	-0.8%	-0.5%	

**Average % diff. from  $Y_m$ :** 0.2%

**Calibration check value status:** PASS

\*Post-test DGM calibration check value ( $Y_{qa}$ ) must be within  $\pm 5\%$  of the specific DGM's established  $Y_m$



15 POINT SECONDARY REFERENCE METER CALIBRATION

Date: July 14, 2022
Customer: Advance Industrial Resource

DGM Model: S-110
DGM S/N: 356333

Reference Prover: #3050 Tape: #01131693

Pbar: 29.68 in Hg

Table with 10 columns: Flow Rate (cfm) Q, Volume (Prover ft^3 Vw, DGM ft^3 Vds), Temperature (Prover (F) tw, DGM (F) tw), Pressure (Prover (in H2O) Pw, DGM (in H2O) Pm), Time (min) Phi, Meter Coefficient Yds, Average Meter Coefficient Yds.

AVERAGE Yds 0.995

Yds = (Vw(tds + tstd) / Vds(tw + tstd)) \* (Pbar / (Pbar + Pm/13.6))

Q = 17.64 \* (Pbar / (tw + tstd)) \* (Vw / Phi)

Dry gas meter Serial Number 356333 was calibrated in accordance with the Code of Federal Regulations, Title 40, Part 60, Appendix A, Method 5 Section 16.1.1

Handwritten signature with 'Signature' label below it.

# Reference Meter Calibration



Calibration Date: July 14, 2022

Test Meter	
Model Number:	AP25
Serial Number:	1902110

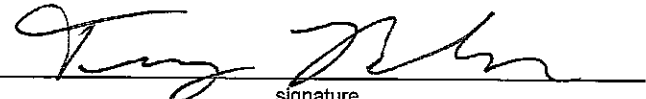
Reference Meter	
Model Number:	Shinagawa W-NK-1A
Serial Number:	538789
Yc:	1.000

Flow Rate (lpm)	Test Meter						
	Volume Initial (liters)	Volume Final (liters)	Volume (liters)	Volume (liters)	DCM Temperatures		
					Initial (°F)	Final (°F)	AVG (°F)
3.00	13,286.2	13,298.6	12.4	12.2	72.4	72.4	72.4
	13,298.6	13,310.8	12.2	12.0	72.6	72.4	72.5
	13,310.8	13,323.3	12.5	12.3	72.4	72.4	72.4
1.50	13,324.7	13,338.0	13.3	13.1	72.6	72.6	72.6
	13,338.0	13,350.7	12.7	12.5	72.6	72.6	72.6
	13,350.7	13,363.0	12.3	12.1	72.6	72.6	72.6
0.80	13,363.4	13,370.1	6.7	6.6	72.8	72.6	72.7
	13,370.1	13,376.6	6.5	6.4	72.7	72.7	72.7
	13,376.6	13,383.4	6.8	6.7	72.6	72.6	72.6
0.40	13,383.5	13,389.4	5.9	5.8	72.9	72.9	72.9
	13,389.4	13,395.3	5.9	5.8	73.1	72.9	73.0
	13,395.3	13,401.3	6.0	5.9	72.9	72.7	72.8
0.25	13,401.4	13,407.4	6.0	5.9	72.8	72.7	72.8
	13,407.4	13,413.3	5.9	5.8	72.8	72.6	72.7
	13,413.3	13,419.1	5.8	5.7	72.6	72.8	72.7

Reference Meter				
Volume Initial (liters)	Volume Final (liters)	Volume Total (liters)	Temp (°F)	Bar Pressure (in Hg)
666.163	678.364	12.201	72.8	29.77
678.364	690.565	12.201	72.8	29.77
690.565	702.776	12.211	72.7	29.77
704.321	717.518	13.197	72.8	29.77
717.518	729.910	12.392	72.9	29.77
729.910	742.182	12.272	72.8	29.77
742.566	749.155	6.599	72.9	29.77
749.155	755.737	6.582	73.0	29.77
755.737	762.318	6.581	72.9	29.77
762.432	768.360	5.928	73.1	29.77
768.360	774.297	5.937	73.3	29.74
774.297	780.245	5.948	73.2	29.77
780.319	786.195	5.876	73.0	29.74
786.195	792.079	5.884	73.0	29.74
792.079	797.961	5.882	73.0	29.74

Yc	Yc Avg	% deviation
0.983	0.986	0.3
1.000		-1.3
0.976		1.0
0.992	0.988	-0.4
0.975		1.3
0.997		-0.9
0.985	0.988	0.3
1.012		-2.4
0.967		2.1
1.004	1.000	-0.4
1.006		-0.5
0.991		1.0
0.979	0.996	1.8
0.997		0.0
1.014		-1.7

0.992

  
signature

07/15/22  
date

# Advanced Industrial Resources, Inc.

## Thermocouple Calibration Data

Thermometer ID: RT-01 ; RT-03  
 Bias: 0

Date: 07/29/23  
 Performed By: DK

Apparatus ID	Apparatus Description	Reference Temperature Reading		Indicated Temperature		Relative Variation
		°F	°R	°F	°R	
						%
P8-01	Stack Temp.	32	492	33	493	0.2
P8-01	Stack Temp.	210	670	211	671	0.1
B-01	Filter Temp.	32	492	32	492	0.0
B-01	Filter Temp.	210	670	210	670	0.0
B-01	Exit Imp. Temp.	32	492	32	492	0.0
B-01	Exit Imp. Temp.	210	670	211	671	0.1
C-009	Meter In Temp.	32	492	33	493	0.2
C-009	Meter In Temp.	210	670	210	670	0.0
C-009	Meter Out Temp.	32	492	32	492	0.0
C-009	Meter Out Temp.	210	670	211	671	0.1
B-01	Filter Exit Temp.	32	492	33	493	0.2
B-01	Filter Exit Temp.	210	670	210	670	0.0
P8-01	Probe Temp.	32	492	33	493	0.2
P8-01	Probe Temp.	210	670	211	671	0.1

### Thermocouple Calibration Procedure

#### A. References

1. Mercury-in-glass reference thermometer, calibrated against thermometric fixed points.
2. Thermometric fixed points, including ice bath and boiling water (corrected for barometric pressure)

#### B. Measurement

1. Compare field temperature sensors against the reference thermometer. Agreement must be within  $\pm 1.5\%$  of the absolute reference temperature.

# Advanced Industrial Resources, Inc.

## Thermocouple Calibration Data

Thermometer ID: RT-01 ; RT-03  
 Bias: 0

Date: 07/29/23  
 Performed By: DK

Apparatus ID	Apparatus Description	Reference Temperature Reading		Indicated Temperature		Relative Variation
		°F	°R	°F	°R	
P8-02	Stack Temp.	32	492	32	492	0.0
P8-02	Stack Temp.	210	670	212	672	0.3
B-02	Filter Temp.	32	492	32	492	0.0
B-02	Filter Temp.	210	670	210	670	0.0
B-02	Exit Imp. Temp.	32	492	33	493	0.2
B-02	Exit Imp. Temp.	210	670	212	672	0.3
C-004	Meter In Temp.	32	492	33	493	0.2
C-004	Meter In Temp.	210	670	210	670	0.0
C-004	Meter Out Temp.	32	492	33	493	0.2
C-004	Meter Out Temp.	210	670	210	670	0.0
B-02	Filter Exit Temp.	32	492	33	493	0.2
B-02	Filter Exit Temp.	210	670	210	670	0.0
P8-02	Probe Temp.	32	492	33	493	0.2
P8-02	Probe Temp.	210	670	211	671	0.1

### Thermocouple Calibration Procedure

#### A. References

1. Mercury-in-glass reference thermometer, calibrated against thermometric fixed points.
2. Thermometric fixed points, including ice bath and boiling water (corrected for barometric pressure)

#### B. Measurement

1. Compare field temperature sensors against the reference thermometer. Agreement must be within  $\pm 1.5\%$  of the absolute reference temperature.

# Advanced Industrial Resources, Inc.

## Type-S Pitot Tube Assembly Inspection Data Sheet

Date: 3/31/2023

Pitot Tube Assembly: OR-P8-01      Caliper ID: CL-OR

Performed by: DK

Pitot tube assembly level?  yes       no

Pitot tube openings damaged?  yes (explain below)       no

$\alpha_1 =$  2  $^{\circ} (<10^{\circ})$        $\beta_1 =$  0  $^{\circ} (<5^{\circ})$

$\alpha_2 =$  1  $^{\circ} (<10^{\circ})$        $\beta_2 =$  0  $^{\circ} (<5^{\circ})$

$\gamma =$  2  $^{\circ}$        $\theta =$  0  $^{\circ}$        $A =$  0.9 in.

$z = A \sin \gamma =$  0.0314 in.       $<1/8$  in. (0.125 in.)

$w = A \sin \theta =$  0.0000 in.       $<1/32$  in. (0.03125 in.)

$P_A =$  0.450 in.       $P_B =$  0.450 in.

$D_t =$  0.375 in.       $P / D_t =$  1.2 (1.05  $\leq$  and  $\leq$  1.50)

$P_a = P_b = P$

$X =$  1.20 ( $>0.75$  in.)      (Dist. between pitot and nozzle)

$Y =$  3.90 ( $>3.0$  in.)      (Dist. from nozzle union to pitot tube openings)

$Z =$  1.20 ( $>0.75$  in.)      (Dist. between pitot and stack thermocouple)

Does the pitot tube assembly meet the Method 2 requirements?  yes

no (explain below)

If the Method 2 requirements are met then a coefficient of **0.84** is assigned to the pitot tube assembly being inspected.



# Advanced Industrial Resources, Inc.

## Type-S Pitot Tube Assembly Inspection Data Sheet

Date: 5/26/2023

Pitot Tube Assembly: OR-P8-02      Caliper ID: CL-OR

Performed by: DK

Pitot tube assembly level?  yes       no

Pitot tube openings damaged?  yes (explain below)       no

$\alpha_1 =$ 0 $^\circ (<10^\circ)$        $\beta_1 =$ 0 $^\circ (<5^\circ)$

$\alpha_2 =$ 0 $^\circ (<10^\circ)$        $\beta_2 =$ 0 $^\circ (<5^\circ)$

$\gamma =$ 0 $^\circ$        $\theta =$ 0 $^\circ$        $A =$ 0.9 in.

$z = A \sin \gamma =$ 0.0000 in.      <1/8 in. (0.125 in.)

$w = A \sin \theta =$ 0.0000 in.      <1/32 in. (0.03125 in.)

$P_A =$ 0.450 in.       $P_B =$ 0.450 in.

$D_t =$ 0.375 in.       $P / D_t =$ 1.2 (1.05  $\leq$  and  $\leq$  1.50)  
 $P_a = P_b = P$

$X =$ 1.00 (>0.75 in.)      (Dist. between pitot and nozzle)  
 $Y =$ 4.00 (>3.0 in.)      (Dist. from nozzle union to pitot tube openings)  
 $Z =$ 1.00 (>0.75 in.)      (Dist. between pitot and stack thermocouple)

Does the pitot tube assembly meet the Method 2 requirements?  yes  
 no (explain below)

If the Method 2 requirements are met then a coefficient of **0.84** is assigned to the pitot tube assembly being inspected.





	<u>Analyte/Gas</u>	<u>Concentration</u>	<u>CC No.</u>
Upscale Cal Gas Info:	O2	20.00	EB0156143
Check Gas Informaiton:	O2	10.96	CC714931

MFC 5000 ccm Evaluation						
	Dilution Conc.	Cal Gas ccm	Dil Gas ccm	Cal Gas	Check Gas	Total Flow
	10.0	3490.76	3509.24	20.00	10.96	7000
	5.0	1745.38	5254.62			
	Dilution Level No.1		Dilution Level No.2		Check Gas	
Low Tolerance	9.774		4.887		10.741	
Evaluation No.1	9.996	PASS	4.937	PASS	10.932	PASS
Evaluation No.2	9.979	PASS	5.017	PASS	10.958	PASS
Evaluation No.3	9.947	PASS	5.013	PASS	10.952	PASS
High Tolerance	10.173		5.087		11.179	
	Dil Level No.1 Avg		Dil Level No.2 Avg		Check Gas Avg	
	9.974		4.989		10.947	
Evaluation No.1 (% diff Mean)	0.22%	PASS	1.04%	PASS	0.14%	PASS
Evaluation No.2 (% diff Mean)	0.05%	PASS	0.56%	PASS	0.10%	PASS
Evaluation No.3 (% diff Mean)	0.27%	PASS	0.48%	PASS	0.04%	PASS

Raw Data

Time	Time	O2 %
7/11/23	12:29	0.009
7/11/23	12:30	0.002
7/11/23	12:31	0.078
7/11/23	12:32	10.31
7/11/23	12:33	20.00
7/11/23	12:34	19.93
7/11/23	12:35	15.83
7/11/23	12:36	10.956
7/11/23	12:37	10.914
7/11/23	12:38	10.057
7/11/23	12:39	9.929
7/11/23	12:40	9.996
7/11/23	12:41	7.365
7/11/23	12:42	4.943
7/11/23	12:43	4.937
7/11/23	12:44	8.445
7/11/23	12:45	10.996
7/11/23	12:46	10.932
7/11/23	12:47	10.540
7/11/23	12:48	9.987
7/11/23	12:49	9.979
7/11/23	12:50	7.039
7/11/23	12:51	4.951
7/11/23	12:52	5.017
7/11/23	12:53	7.842
7/11/23	12:54	10.913
7/11/23	12:55	10.958
7/11/23	12:56	10.368
7/11/23	12:57	9.950
7/11/23	12:58	9.947
7/11/23	12:59	7.177
7/11/23	13:00	5.003
7/11/23	13:01	5.013
7/11/23	13:02	7.813
7/11/23	13:03	11.005
7/11/23	13:04	10.952

Carbon Bed I/O

Calibration Error Test at Run 1

Operator: Dan Kirk

Date	7/11/2023		
Analyte	O2		O2
Units	%		
Zero Ref Cyl	0.0		
Zero Avg	0.078	Times	12:31
Zero Error%	0.4%		
Zero CALERR PASS?	PASS		
Mid Ref Cyl	10.96		
Mid Avg	10.91	Times	12:37
Mid Error%	-0.2%		
Mid CALERR PASS?	PASS		
High Ref Cyl	20.00		
High Avg	19.93	Times	12:34
High Error%	-0.3%		
High CALERR PASS?	PASS		

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI80E15A0007	Reference Number: 122-402105348-1
Cylinder Number: CC714931	Cylinder Volume: 150.4 CF
Laboratory: 124 - Durham (SAP) - NC	Cylinder Pressure: 2015 PSIG
PGVP Number: B22021	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: May 04, 2021

**Expiration Date: May 04, 2029**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	9.000 %	8.914 %	G1	+/- 0.8% NIST Traceable	05/04/2021
OXYGEN	11.00 %	10.96 %	G1	+/- 0.4% NIST Traceable	05/04/2021
NITROGEN	Balance				

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060638	CC414571	13.359 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	May 14, 2025
NTRM	10010616	K014963	9.967 % OXYGEN/NITROGEN	+/- 0.3%	Apr 19, 2022

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VA-5001 CO2 BF89GV17	Nondispersive Infrared (NDIR)	Apr 29, 2021
Siemens Oxymat 61 M3299 O2	Paramagnetic	Apr 28, 2021

Triad Data Available Upon Request



\_\_\_\_\_  
Signature on file  
Approved for Release

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI62E15A1071	Reference Number: 153-402506671-1
Cylinder Number: EB0156143	Cylinder Volume: 141.0 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72022	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Aug 08, 2022

**Expiration Date: Aug 08, 2030**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	18.00 %	17.92 %	G1	+/- 0.8% NIST Traceable	08/08/2022
OXYGEN	20.00 %	20.00 %	G1	+/- 0.5% NIST Traceable	08/08/2022
NITROGEN	Balance				

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060802	CC415397	24.04 % CARBON DIOXIDE/NITROGEN	0.6%	Dec 11, 2025
NTRM	09061434	CC282492	22.53 % OXYGEN/NITROGEN	0.4%	May 13, 2025

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Jul 20, 2022
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (Mason)	Jul 20, 2022

Triad Data Available Upon Request



\_\_\_\_\_  
Signature on file  
Approved for Release

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA PROTOCOL STANDARD

Part Number: E02NI99E15A0932	Reference Number: 153-402614773-1
Cylinder Number: EB0158879	Cylinder Volume: 144.0 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72022	Valve Outlet: 350
Gas Code: PPN,BALN	Certification Date: Dec 16, 2022

**Expiration Date: Dec 16, 2030**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

### ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
PROPANE	500.0 PPM	501.8 PPM	G1	+/- 0.7% NIST Traceable	12/16/2022
NITROGEN	Balance				

### CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	12010923	ND46382	487 PPM PROPANE/AIR	0.6%	Apr 24, 2024

### ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet iS50 AUP2110269 C3H8 MC3H8	FTIR	Dec 14, 2022

Triad Data Available Upon Request



Signature on file

Approved for Release

# coastal instruments

MASS FLOW CONTROLLER SPECIALISTS

707 Enterprise Dr • Post Office Box 699 • Burgaw, North Carolina 28425 • (910) 259-4485

<http://www.mfchelp.com>

## Certificate Of Calibration

The following device has been calibrated in accordance with ANSI Z540-1-1994 and ISO/IEC-17025:2017 using instruments traceable to the National Institute of Standards and Technology

Certificate #: NC00060727

**ADVANCED INDUSTRIAL RESOURCES**  
3407 Novis Pointe  
Acworth GA 30101  
USA

STP Conditions: 25.0 °C @ 760 mmHg  
Calibration Temperature 22.2° C ± 3° C  
He pre-ship leak rate 1 x 10<sup>-9</sup>

Model: HASTINGS HFC-212  
Serial Number: 0127751001  
Range: 1000 sccm  
Gas: AIR  
Inlet Pressure: 30 PSIG  
Outlet Pressure: ATM  
Positioning: HBD  
Calibration Gas: N2, N2 CF = 0.998  
Calibration Date: 9/13/2021  
Issue Date: 09/14/2021

**Initial Inspection**

- No visible contamination

**Services**

- Purged sensor with methyl alcohol and N2
- Cleaned IAW Document 003 (rev 08/15/16), "Cleaning"
- Calibrated and response tested at full scale flow IAW Document 005 (rev 09/06/16), "MFC Calibration"
- Assembled with Viton seals

**Parts Replaced**

- No parts required

**Comments**

- We appreciate your business!
- 10% = 98.36 30% = 297.72
- 50% = 497.61 70% = 697.48
- 90% = 899.77
- The referenced DUT meets the Coastal Instruments internal quality specification for tolerance

As Found

Volt	%	Calc. Flow (sccm)	F.S. Dev.
		no data taken	

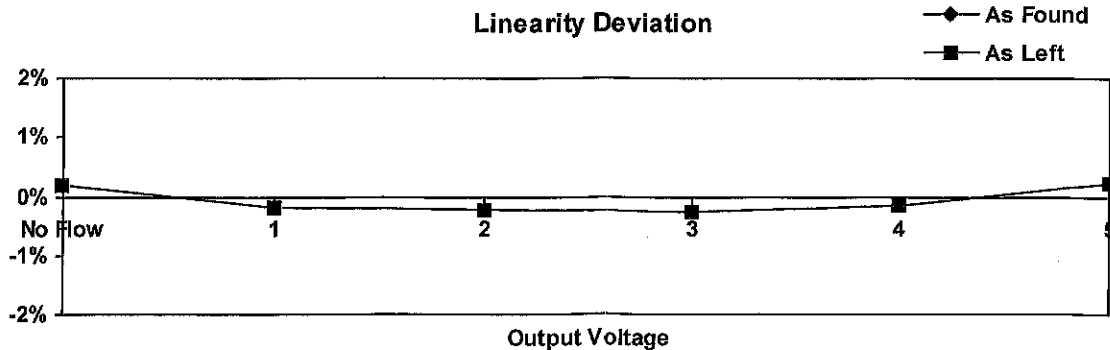
As Left

Volt	%	Calc. Flow (sccm)	F.S. Dev.
0.009	0	No Flow	0.18%
1.00	20	198.09	-0.19%
2.00	40	397.66	-0.23%
3.00	60	597.52	-0.25%
4.00	80	798.57	-0.14%
5.00	100	1002.2	0.22%

Checked for accuracy by: Brad Darby, Quality

*Brad Darby*

% F.S. Dev = (Calculated - Target) / Full Scale \* 100



### Calibration And Repair Of All Mass Flow Brands And Models

This report not to be reproduced, except in full, without written authorization by Coastal Instruments, Inc.  
The statement of conformity contained herein applies only to the calibration of flow of gas, and the gas flow data represented.



### Certificate Of Calibration

The following device has been calibrated in accordance with ANSI Z540-1-1994 and ISO/IEC-17025:2017 using instruments traceable to the National Institute of Standards and Technology

**ADVANCED INDUSTRIAL RESOURCES**  
 3407 Novis Pointe  
 Acworth GA 30101  
 USA

STP Conditions: 25.0 °C @ 760 mmHg  
 Calibration Temperature Room Temperature  
 He pre-ship leak rate 0 x 10<sup>-6</sup>

Model: HASTINGS HFC-212  
 Serial Number: 3161400002  
 Range: 5000 sccm  
 Gas: N2  
 Inlet Pressure: 30 PSIG  
 Outlet Pressure: ATM  
 Positioning: HBD  
 Calibration Gas: N2, N2 CF = 1  
 Calibration Date: 9/10/2021  
 Issue Date: 09/13/2021

**Initial Inspection**

- No visible contamination

**Services**

- Purged sensor with methyl alcohol and N2
- Cleaned IAW Document 003 (rev 08/15/16), "Cleaning"
- Calibrated and response tested at full scale flow IAW Document 005 (rev 09/06/16), "MFC Calibration"

**Parts Replaced**

- No parts required

**Comments**

- We appreciate your business!
- 10% = 503.05 30% = 1522.1
- 50% = 2523.9 70% = 3514.2
- 90% = 4502.1
- The referenced DUT meets the Coastal Instruments internal quality specification for tolerance

As Found

Volt	%	Calc. Flow (sccm)	F.S. Dev.
		no data taken	

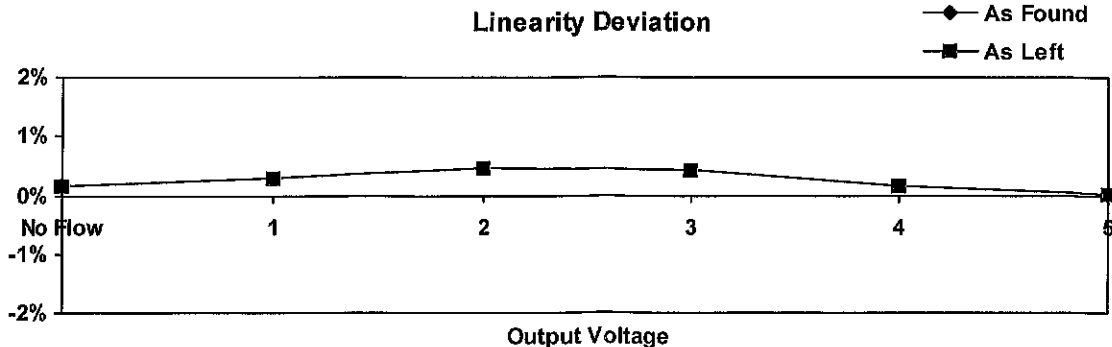
As Left

Volt	%	Calc. Flow (sccm)	F.S. Dev.
0.008	0	No Flow	0.16%
1.00	20	1014.0	0.28%
2.00	40	2023.6	0.47%
3.00	60	3020.8	0.42%
4.00	80	4006.8	0.14%
5.00	100	5000.8	0.02%

Checked for accuracy by: Brad Darby, Quality

*Brad Darby*

% F.S. Dev = (Calculated - Target) / Full Scale \* 100



### Calibration And Repair Of All Mass Flow Brands And Models

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 The statement of conformity contained herein applies only to the calibration of flow of gas, and the gas flow data represented.

## Certificate Of Calibration

The following device has been calibrated in accordance with ANSI Z540-1-1994 and ISO/IEC-17025:2017 using instruments traceable to the National Institute of Standards and Technology

**ADVANCED INDUSTRIAL RESOURCES**  
3407 Novis Pointe  
Acworth GA 30101  
USA

STP Conditions: 25.0 °C @ 760 mmHg  
Calibration Temperature 22.2° C ± 3° C  
He pre-ship leak rate 1 x 10<sup>-9</sup>

Model: HASTINGS HFC-212  
Serial Number: 3053000003  
Range: 10000 sccm  
Gas: AIR  
Inlet Pressure: 30 PSIG  
Outlet Pressure: ATM  
Positioning: HBD  
Calibration Gas: N2, N2 CF = 0.998  
Calibration Date: 9/9/2021  
Issue Date: 09/10/2021

**Initial Inspection**

- No visible contamination

**Services**

- Purged sensor with methyl alcohol and N2
- Cleaned IAW Document 003 (rev 08/15/16), "Cleaning"
- Calibrated and response tested at full scale flow IAW Document 005 (rev 09/06/16), "MFC Calibration"
- Assembled with Viton seals

**Parts Replaced**

- No parts required

**Comments**

- We appreciate your business!
- 10% = 971.89 / 30% = 2950.3
- 50% = 4928.6 / 70% = 6934.9
- 90% = 9030.4
- The referenced DUT meets the Coastal Instruments internal quality specification for tolerance

Checked for accuracy by: Brad Darby, Quality

*Brad Darby*

**As Found**

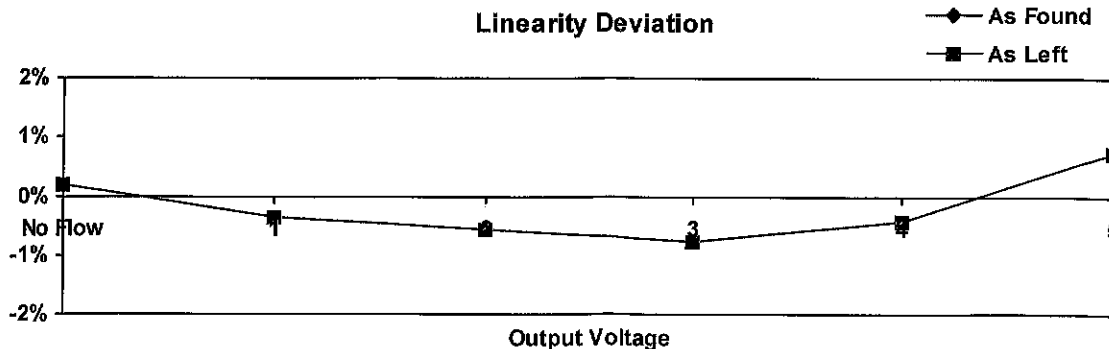
Volt	%	Calc. Flow (sccm)	F.S. Dev.
		no data taken	

**As Left**

Volt	%	Calc. Flow (sccm)	F.S. Dev.
0.009	0	No Flow	0.18%
1.00	20	1965.0	-0.35%
2.00	40	3942.3	-0.58%
3.00	60	5922.8	-0.77%
4.00	80	7955.6	-0.44%
5.00	100	10072	0.72%

% F.S. Dev = (Calculated - Target) / Full Scale \* 100

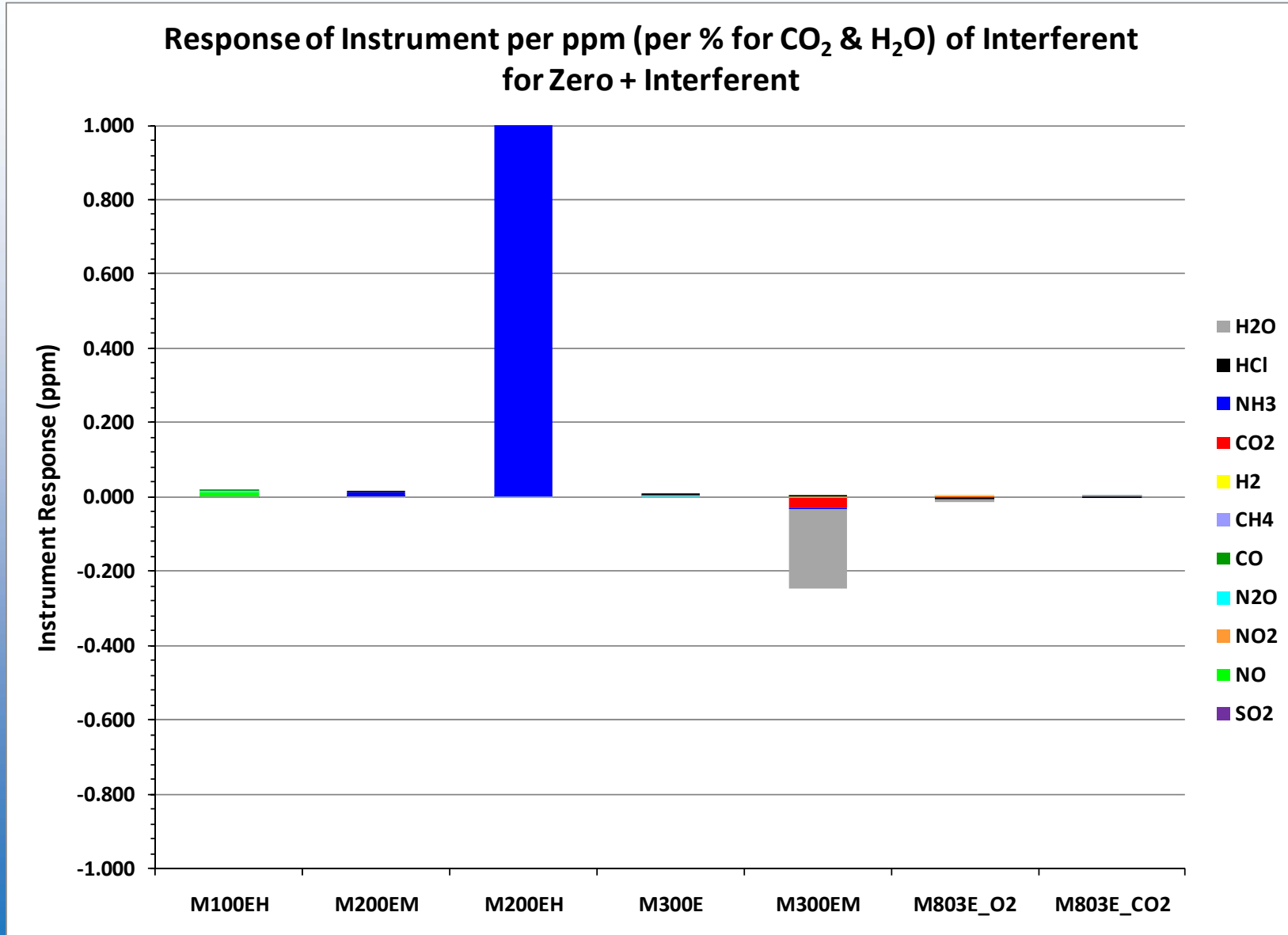
**Linearity Deviation**



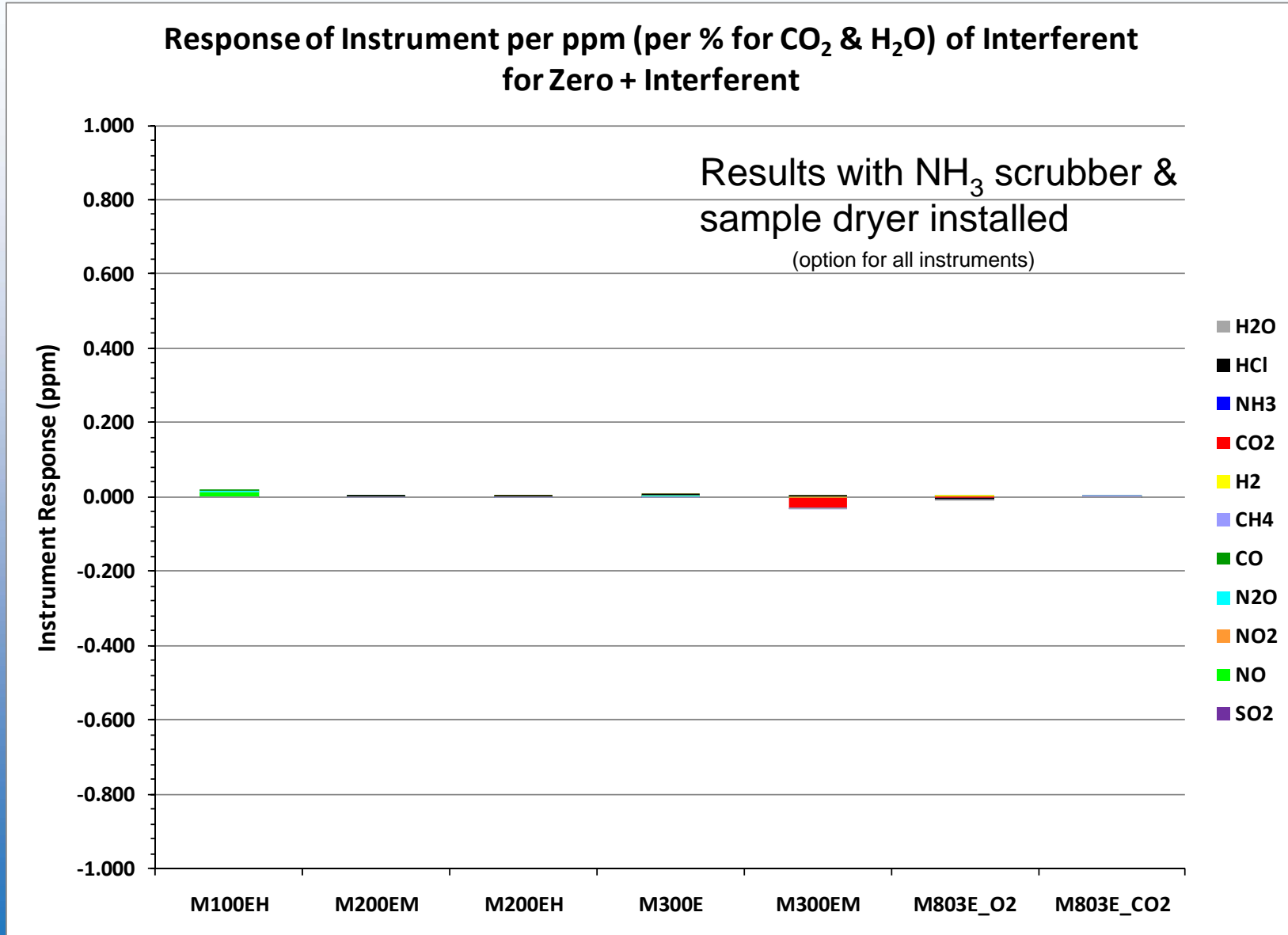
### Calibration And Repair Of All Mass Flow Brands And Models

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The statement of conformity contained herein applies only to the calibration of flow of gas, and the gas flow data represented.

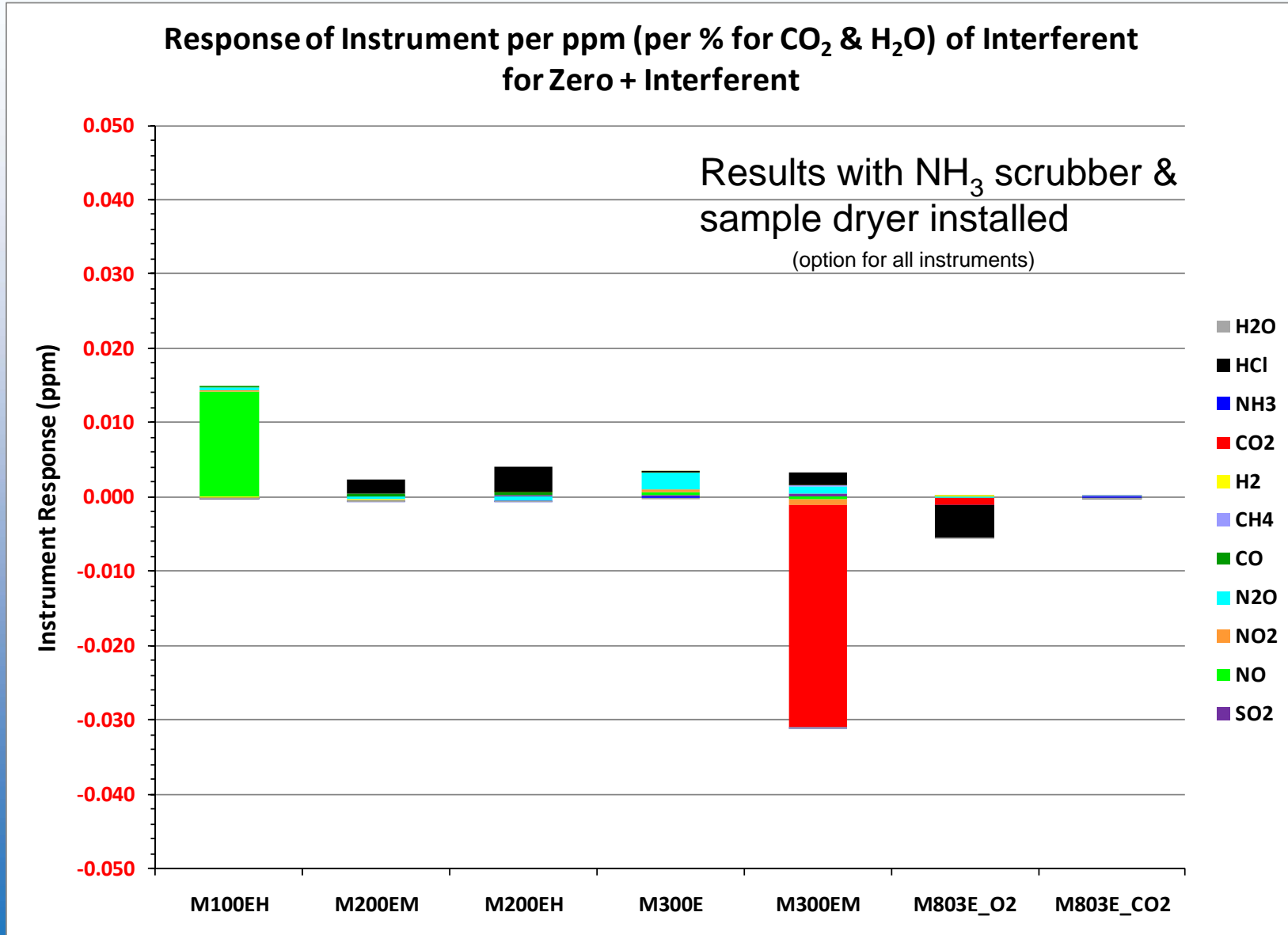
# Zero + Interferent: Instrument Response / ppm



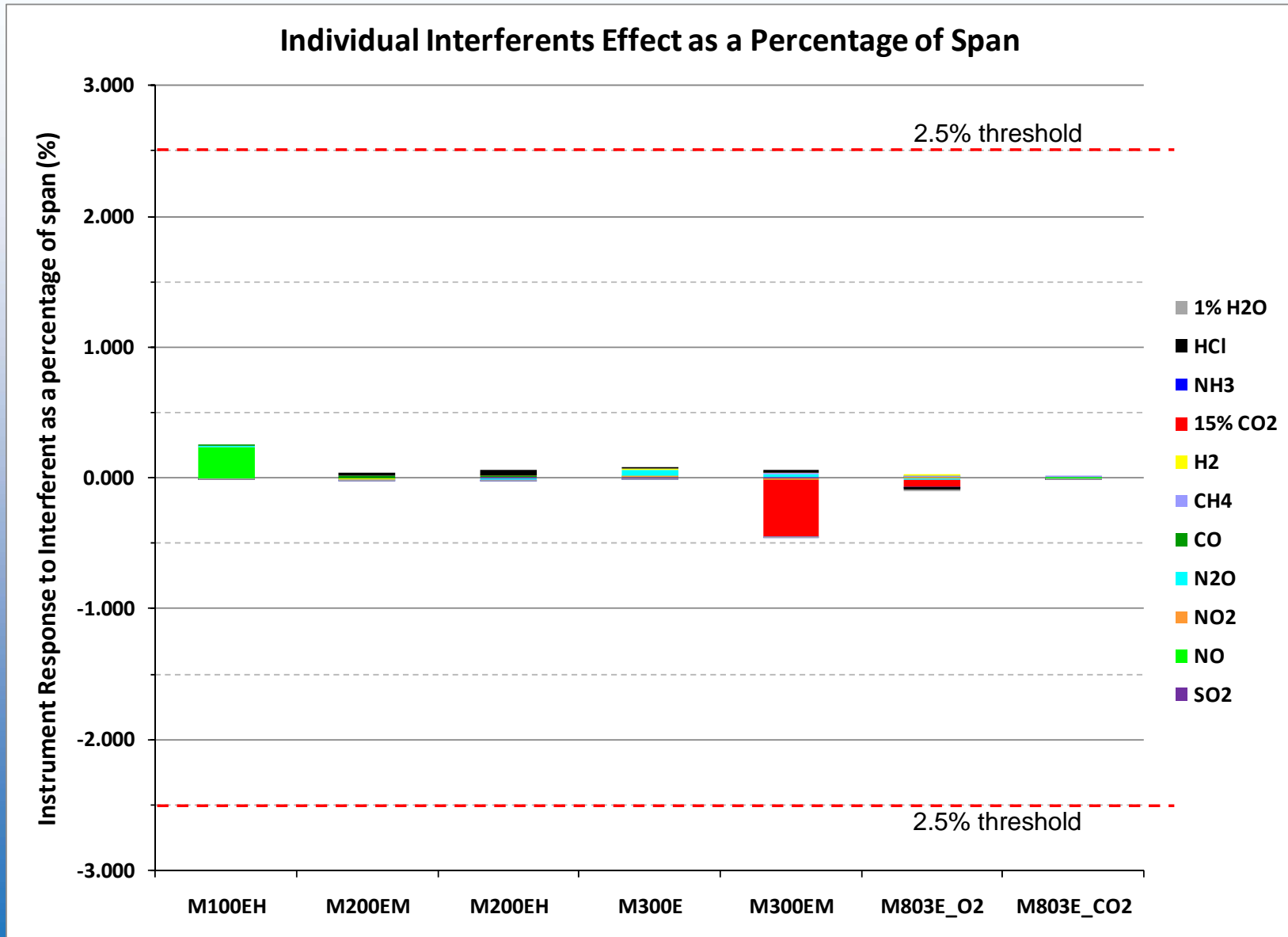
# Zero + Interferent: Instrument Response / ppm



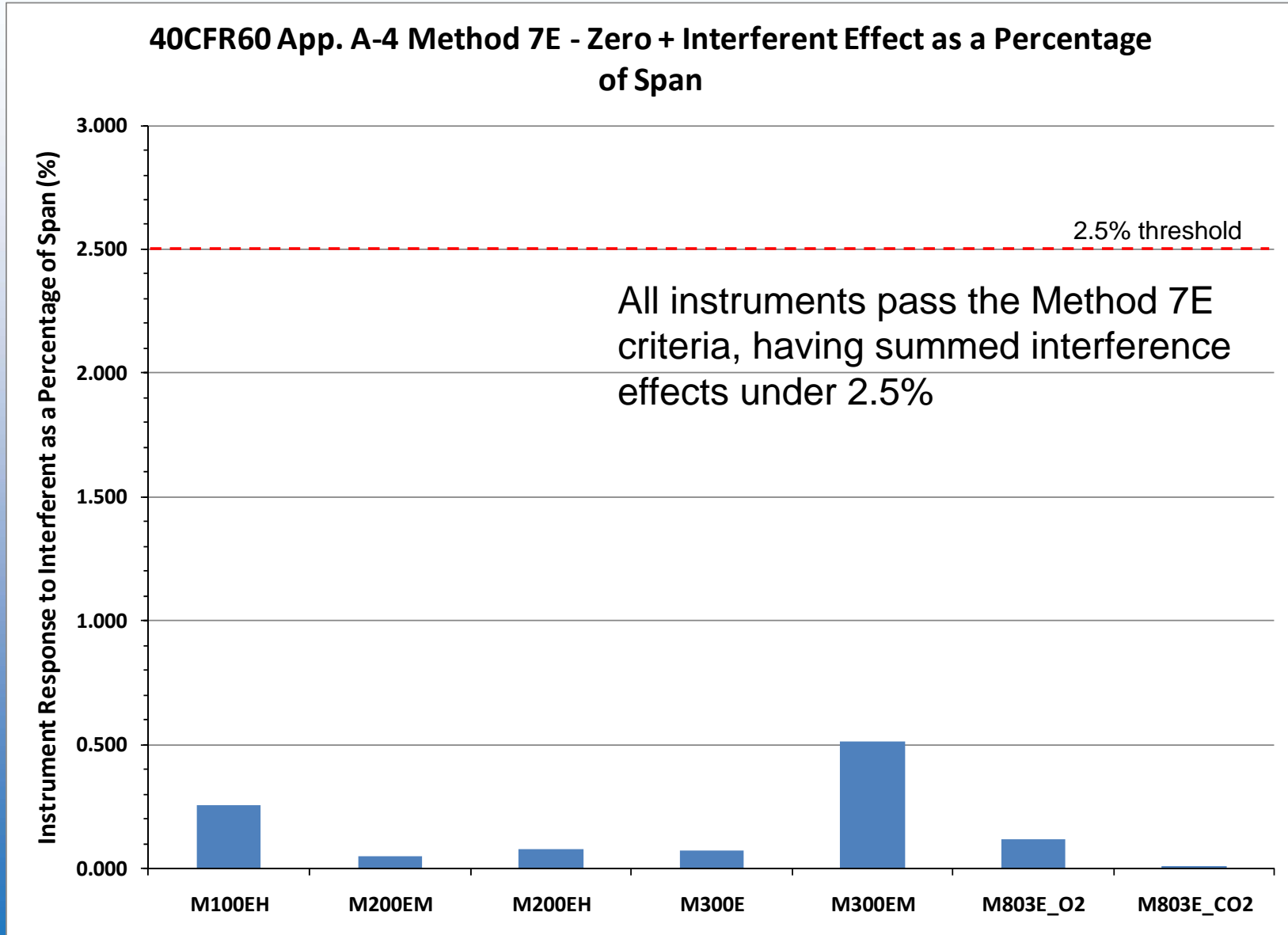
# Zero + Interferent: Instrument Response / ppm



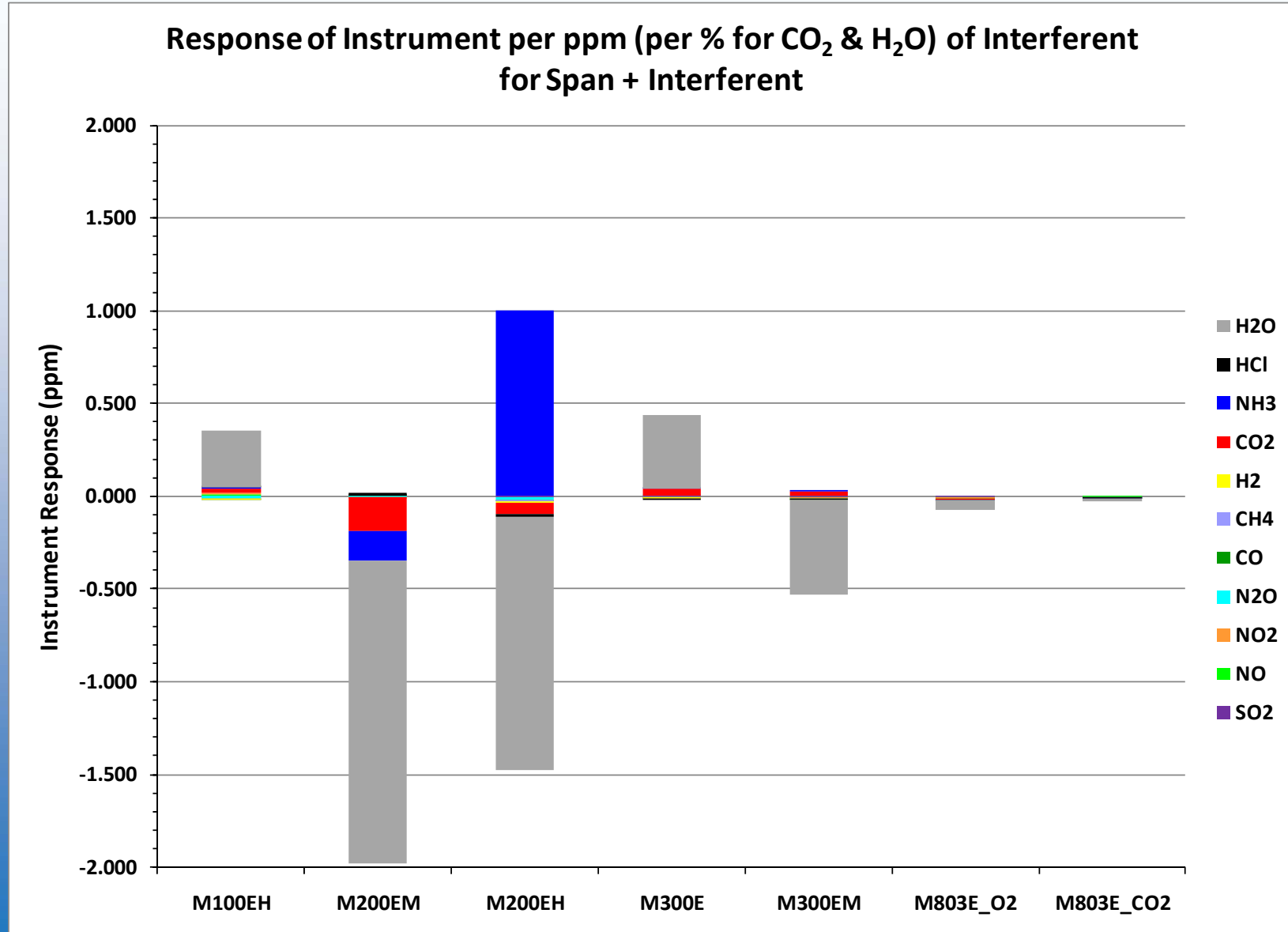
# Zero + Interferent: 40CFR60 App. 4-A Method 7E



# Zero + Interferent: 40CFR60 App. 4-A Method 7E

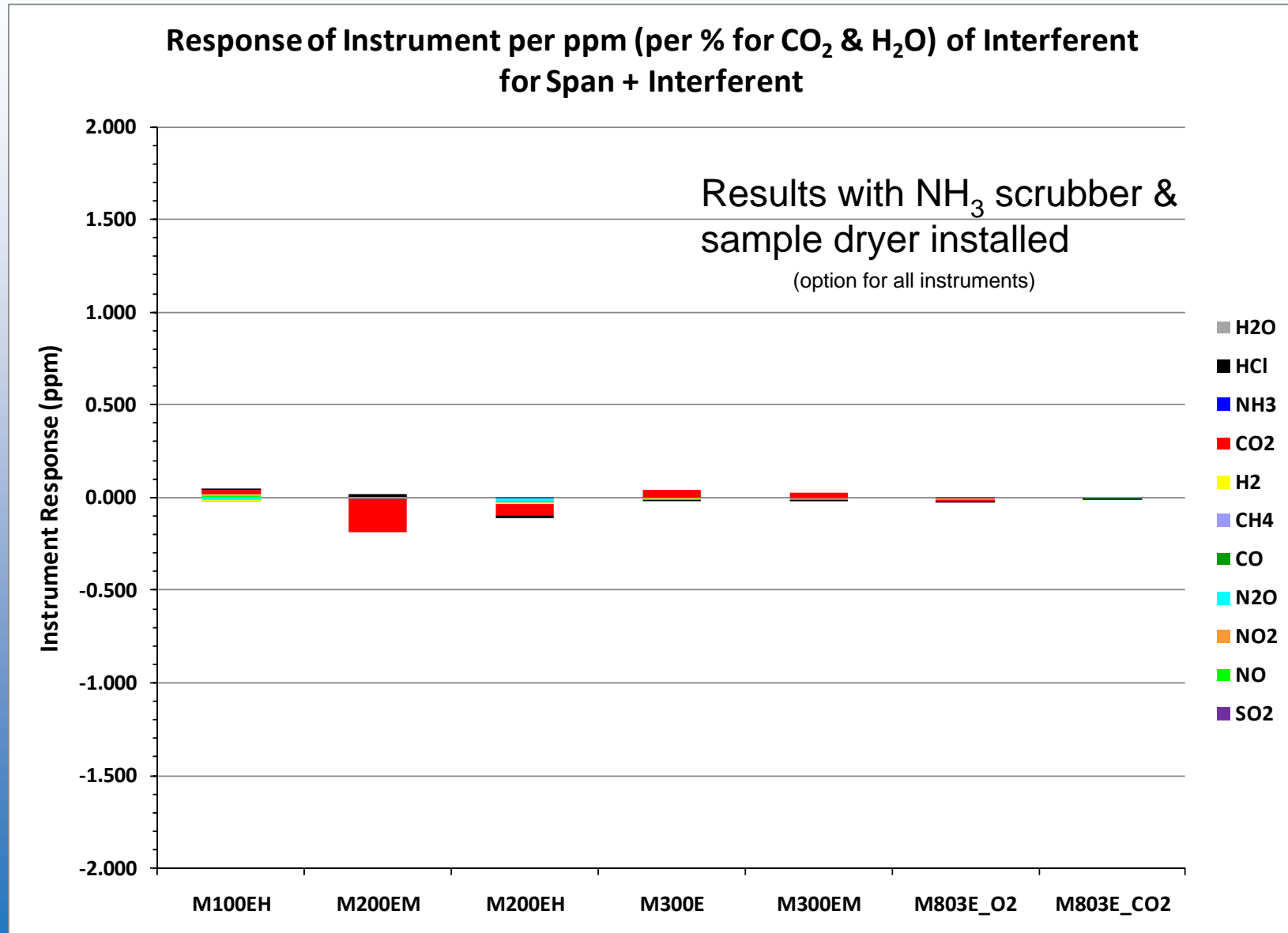


# Span + Interferent: Instrument Response / ppm

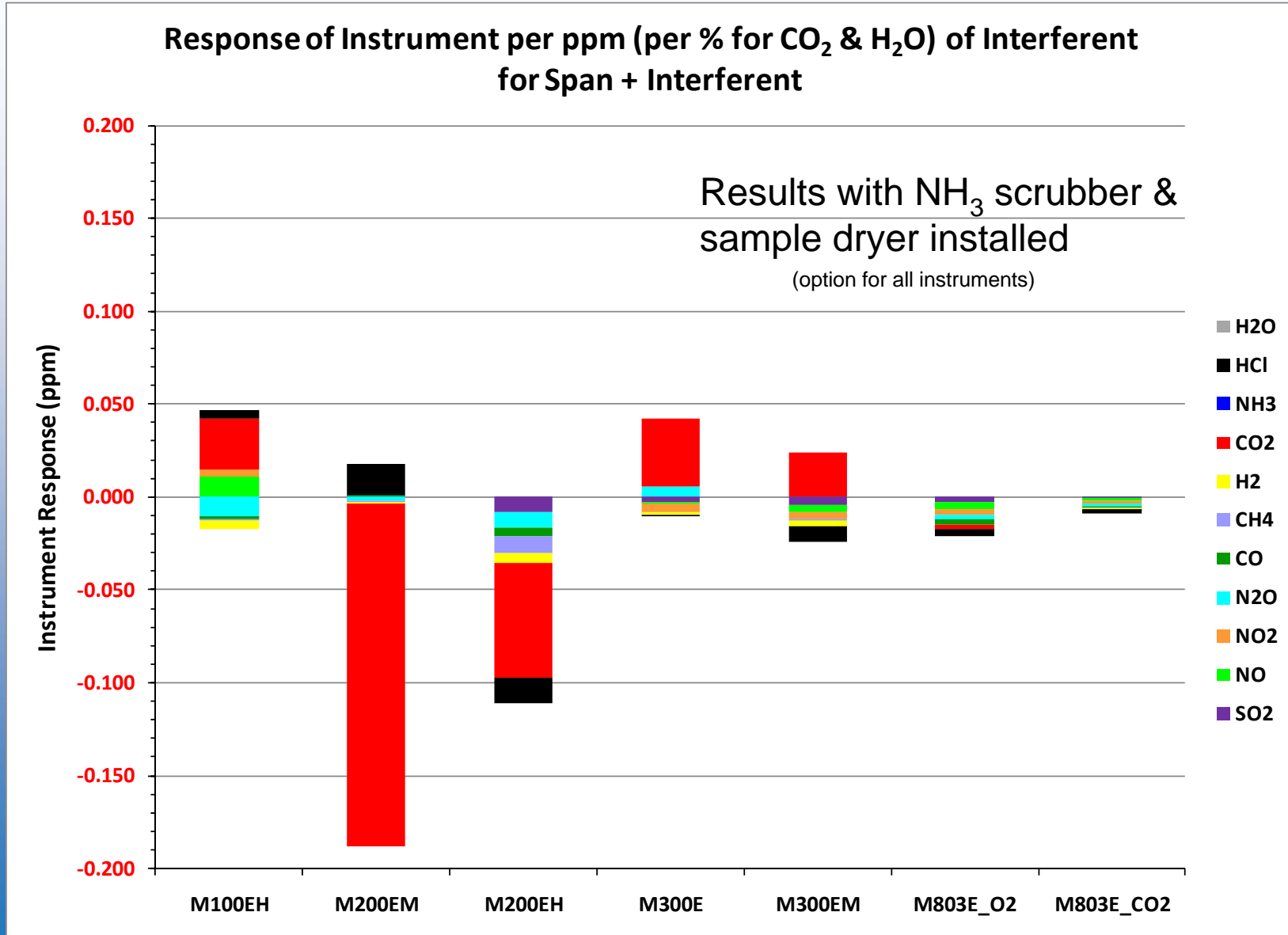




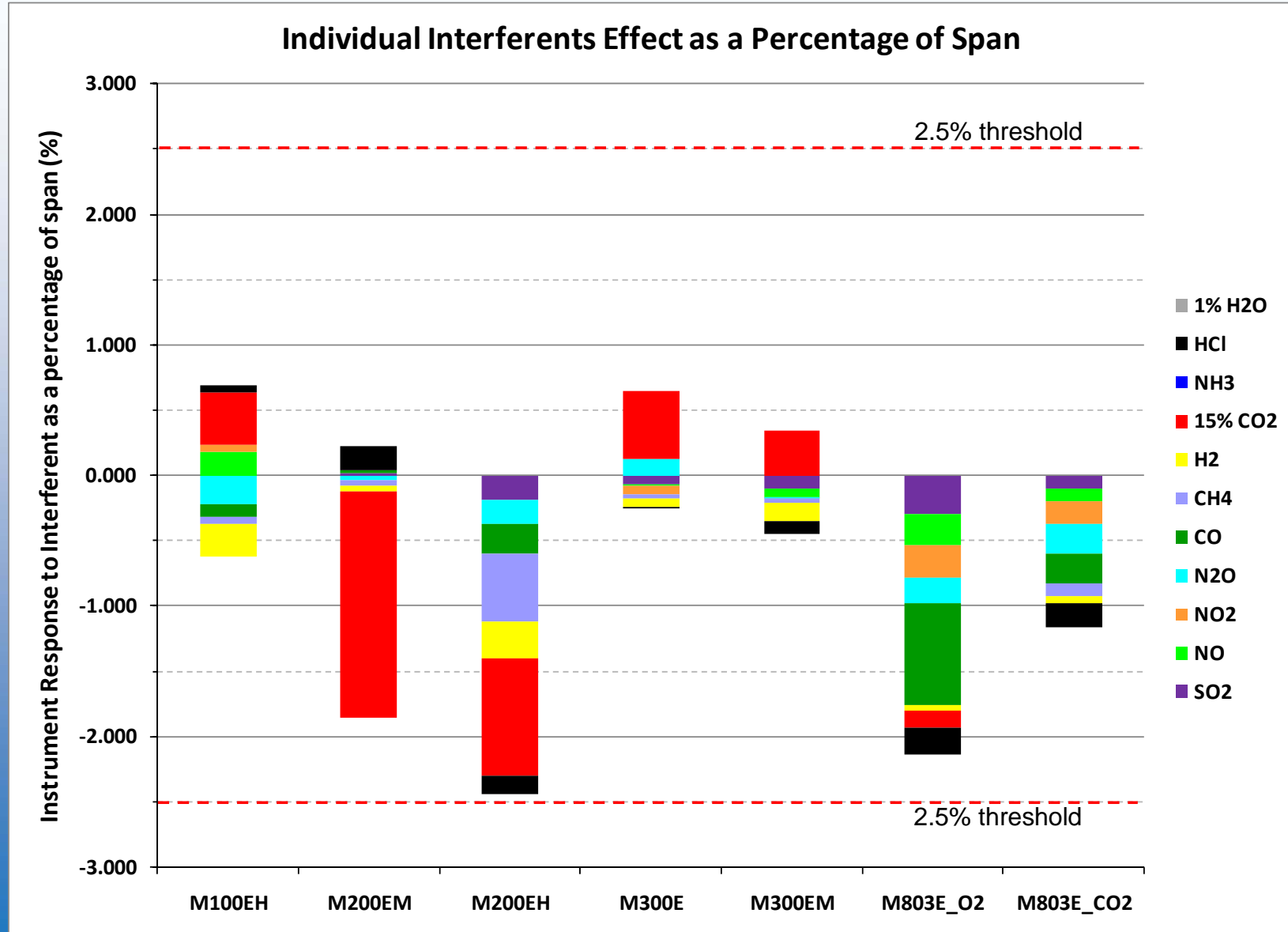
# Span + Interferent: Instrument Response / ppm



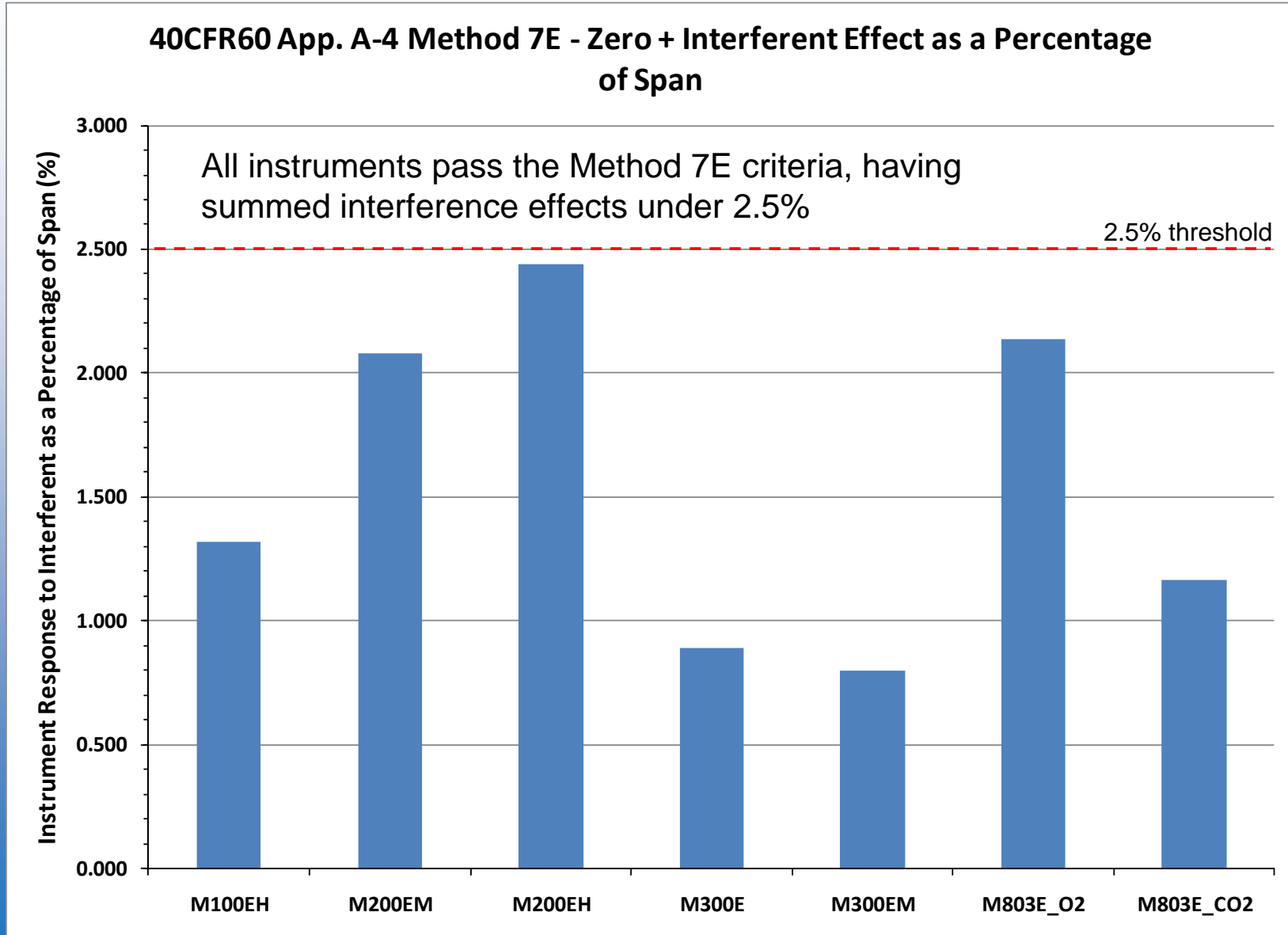
# Span + Interferent: Instrument Response / ppm



# Span + Interferent: 40CFR60 App. 4-A Method 7E



# Span + Interferent: 40CFR60 App. 4-A Method 7E



# Conclusions

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- 40CFR60 App. A-4 Method 7E interference testing
  - Relatively straightforward to perform
  - Huge investment in the time & resources involved to ensure quality experimental setup, execution, and data analysis
- Interference test results
  - Show that the Teledyne – API instruments common to RATA and CEMS applications meet the interference effect criteria defined by 40CFR60 App. A-4 Method 7E
- For the Zero + Interferent tests
  - The instruments perform well within the criteria
    - Shows that the primary effect of interferences is not due to the interferent gas producing a signal on its own

# Conclusions

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- For the Span + Interferent tests

- Some of the instruments (M100EH, M300E, M300EM, M803E(CO<sub>2</sub>)), perform well within the criteria
- The NO<sub>x</sub> instruments (especially the M200EH) are close to the threshold
  - It should be noted that this is for all interferent gasses combined at their max (worst case scenerio)
- Shows why RATA analyzers need to be calibrated under the same conditions as the CEMS instruments for proper comparison

- Future Directions

- Further investigate the cause of specific interferences and how to reduce their effect

# Acknowledgements

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- Teledyne – API Engineering & Sales
  - Pat King
  - Robin Becker
  - David Neuschuler
  - Kirk Lovewell
  - Jeff Franks
  - Bill Taylor
  - Martin Abbott

**APPENDIX G**

**PROCESS OPERATION DATA**



## Juno Stack Tests: Carbon Adsorber Beds Monthly Performance & Emission Factor Verification - July 2023 - Operations Logsheet

Date last activated carbon media replacement:

6/2/2023

Number of batches processed since last Activated Carbon Media (ACM) replacement at start of test:

112

(as of 7/12/2023 8:30 AM - start time of 1st test batch)

Test Batch #	# Batches since Last ACM Replacement	Date (MM/DD/YY)	Batch Size						Production Rate (tons/batch)	Batch Step Times (HR:MIN AM/PM)				Comments
			# Bales			Weight (lb)				BATCH START TIME	JC Door Closing at Start of Cook	JC Door Opening at End of Cook	BATCH END TIME	
#	#	(MM/DD/YY)	OCC	MSW	Total	OCC	MSW	Total	(tons/batch)	Start JC Loading	Start of Cook	End of Cook	JC Discharge Complete	
1	113	7/12/2023	0	18	18	0	39,800	39,800	19.9	8:48am	9:00am	10:30am	11:14am	
2	114	7/12/2023	0	18	18	0	42,300	42,300	21.2	12:10pm	12:24pm	1:50pm	2:34pm	
3	115	7/12/2023	0	18	18	0	42,080	42,080	21.0	3:30pm	3:46pm	5:18pm	5:57pm	

## Juno Stack Test Parameters

Monthly - July 2023

7/12/23 8:48  
7/12/23 17:58  
1m

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 08:48:00	13.0	124.7	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:49:00	13.0	124.5	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:50:00	13.0	124.3	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:51:00	13.0	124.1	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:52:00	13.0	124.0	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:53:00	13.0	123.7	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:54:00	13.0	123.5	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:55:00	13.0	123.3	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:56:00	13.0	123.1	3.0	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:57:00	13.0	122.9	3.1	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:58:00	13.0	122.6	3.1	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 08:59:00	13.0	122.3	3.1	17.1	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:00:00	12.0	122.1	3.5	17.9	76.2	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:01:00	7.8	121.8	4.0	33.2	94.7	24.6	9.7	9.7	50	1	1	0.0
12-Jul-23 09:02:00	3.9	121.4	3.7	53.3	95.0	23.8	9.7	9.8	50	1	1	0.0
12-Jul-23 09:03:00	3.0	121.2	3.3	65.0	35.1	20.8	9.7	9.7	50	1	1	0.0
12-Jul-23 09:04:00	4.1	121.8	3.3	59.3	0.0	20.2	9.7	9.7	50	1	0	0.0
12-Jul-23 09:05:00	6.1	133.4	3.3	46.0	0.0	20.0	9.7	9.7	50	1	0	0.0
12-Jul-23 09:06:00	10.8	161.0	3.3	32.5	0.0	20.0	9.7	9.7	50	1	0	0.0
12-Jul-23 09:07:00	18.8	191.3	3.3	20.9	0.0	21.8	9.7	9.7	50	1	0	0.0
12-Jul-23 09:08:00	28.4	219.0	3.2	17.0	0.0	24.2	9.7	9.7	50	1	0	0.0
12-Jul-23 09:09:00	38.0	242.0	3.2	16.8	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:10:00	47.2	259.8	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:11:00	56.7	274.0	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:12:00	65.7	285.9	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:13:00	70.3	295.3	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:14:00	69.0	297.8	3.1	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:15:00	67.7	297.4	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:16:00	65.3	296.8	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:17:00	62.2	295.0	3.2	16.9	0.0	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:18:00	59.8	292.2	3.2	16.9	-0.1	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:19:00	58.1	289.6	3.2	16.9	-0.1	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:20:00	56.8	287.3	3.3	16.9	-0.1	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:21:00	55.3	285.0	3.3	16.9	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:22:00	54.3	282.9	3.3	16.9	-0.1	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:23:00	53.5	281.0	3.3	16.9	-0.1	24.3	9.7	9.7	50	1	0	0.0
12-Jul-23 09:24:00	52.7	279.3	3.3	16.9	0.0	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:25:00	52.0	277.9	3.3	16.9	0.0	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:26:00	51.5	276.6	3.3	16.9	-0.2	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:27:00	51.0	275.6	3.3	16.9	-0.8	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:28:00	50.6	274.7	3.3	16.9	-0.4	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:29:00	50.1	273.8	3.2	16.9	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:30:00	49.8	273.1	3.2	16.9	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:31:00	49.4	272.3	3.3	16.9	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:32:00	49.2	271.6	3.3	16.9	-0.1	24.3	9.6	9.7	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 09:33:00	49.1	270.9	3.4	16.9	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:34:00	49.4	270.3	3.4	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:35:00	49.7	270.2	3.4	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:36:00	50.0	270.6	3.4	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:37:00	50.7	271.1	3.4	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:38:00	51.6	273.0	3.3	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:39:00	52.4	275.0	3.3	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:40:00	52.9	277.0	3.3	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:41:00	52.5	277.7	3.3	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:42:00	52.2	277.1	3.3	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:43:00	51.7	276.0	3.3	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:44:00	51.2	274.6	3.3	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:45:00	50.8	273.3	3.2	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:46:00	50.5	272.1	3.3	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:47:00	50.3	271.1	3.3	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:48:00	50.4	270.4	3.4	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:49:00	50.9	270.2	3.4	17.0	-0.1	24.3	9.6	9.7	50	1	0	0.0
12-Jul-23 09:50:00	51.5	270.6	3.4	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:51:00	52.1	271.3	3.4	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:52:00	52.8	273.3	3.5	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:53:00	53.4	275.3	3.5	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:54:00	53.9	276.7	3.5	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:55:00	53.5	276.6	3.5	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:56:00	53.0	276.1	3.5	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:57:00	52.7	275.2	3.5	17.0	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:58:00	52.4	274.2	3.5	17.1	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 09:59:00	52.1	273.0	3.5	17.1	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:00:00	52.1	272.1	3.5	17.1	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:01:00	52.3	271.4	3.5	17.1	-0.1	24.2	9.6	9.6	50	1	0	0.0
12-Jul-23 10:02:00	52.5	270.9	3.6	17.1	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:03:00	52.6	270.5	3.6	17.1	-0.1	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:04:00	52.8	270.4	3.6	17.1	-0.1	24.2	9.6	9.6	50	1	0	0.0
12-Jul-23 10:05:00	53.1	270.6	3.6	17.1	0.0	24.2	9.6	9.6	50	1	0	0.0
12-Jul-23 10:06:00	53.5	271.3	3.5	17.1	0.0	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:07:00	53.9	272.5	3.5	17.1	0.0	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:08:00	54.4	274.2	3.5	17.1	0.0	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:09:00	54.8	275.5	3.6	17.1	0.0	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:10:00	54.8	275.7	3.6	17.1	0.0	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:11:00	54.4	275.2	3.6	17.1	0.0	24.2	9.6	9.6	50	1	0	0.0
12-Jul-23 10:12:00	53.9	274.6	3.6	17.1	0.0	24.3	9.6	9.6	50	1	0	0.0
12-Jul-23 10:13:00	53.2	273.9	3.6	17.1	50.6	24.3	9.6	9.6	50	1	0	14.0
12-Jul-23 10:14:00	45.9	272.4	3.9	27.6	98.2	24.5	9.6	9.6	50	1	0	38.0
12-Jul-23 10:15:00	35.1	267.3	4.0	49.6	99.0	24.4	9.6	9.6	50	1	0	62.0
12-Jul-23 10:16:00	26.2	259.0	3.7	64.5	99.7	21.2	9.6	9.6	50	1	0	86.0
12-Jul-23 10:17:00	20.3	252.0	3.7	72.9	89.6	20.4	9.6	9.6	50	1	0	100.0
12-Jul-23 10:18:00	16.3	247.5	3.7	78.8	86.3	20.5	9.6	9.6	50	1	0	100.0
12-Jul-23 10:19:00	13.3	245.7	3.6	83.9	86.5	20.6	9.6	9.6	50	1	0	100.0
12-Jul-23 10:20:00	11.2	244.1	3.5	88.8	86.6	20.7	9.6	9.6	50	1	0	100.0
12-Jul-23 10:21:00	9.6	242.6	3.5	93.8	87.2	20.8	9.6	9.6	50	1	0	100.0
12-Jul-23 10:22:00	8.3	241.0	3.4	98.6	99.4	20.9	9.6	9.6	50	1	0	100.0
12-Jul-23 10:23:00	7.3	239.4	3.4	99.9	98.9	21.0	9.6	9.6	50	1	0	100.0
12-Jul-23 10:24:00	6.4	237.8	3.5	100.1	98.3	21.0	9.6	9.6	50	1	0	100.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 10:25:00	6.3	236.7	3.5	100.0	98.6	21.1	9.6	9.6	50	1	0	66.7
12-Jul-23 10:26:00	7.3	235.7	3.4	100.0	13.8	21.0	9.6	9.6	50	1	0	0.0
12-Jul-23 10:27:00	11.2	234.7	3.4	97.8	0.1	20.9	9.6	9.6	50	1	0	0.0
12-Jul-23 10:28:00	13.8	233.9	3.4	85.2	0.0	20.7	9.6	9.6	50	1	0	0.0
12-Jul-23 10:29:00	14.0	233.1	3.4	71.1	0.0	20.4	9.6	9.6	50	1	0	0.0
12-Jul-23 10:30:00	14.0	232.3	3.4	57.1	0.0	20.2	9.6	9.6	50	1	0	0.0
12-Jul-23 10:31:00	14.0	231.4	3.4	43.3	0.0	20.0	9.5	9.6	50	1	0	0.0
12-Jul-23 10:32:00	14.0	230.6	3.4	30.0	0.0	20.1	9.4	9.4	50	1	0	0.0
12-Jul-23 10:33:00	14.0	229.7	3.5	19.5	0.0	22.4	9.4	9.5	50	1	0	0.0
12-Jul-23 10:34:00	13.9	228.8	3.5	16.8	-0.3	24.2	9.4	9.5	50	1	0	0.0
12-Jul-23 10:35:00	13.9	227.9	3.5	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 10:36:00	13.9	227.1	3.6	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 10:37:00	13.9	226.3	3.5	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 10:38:00	13.9	225.6	3.5	16.8	0.0	24.3	9.4	9.5	50	1	0	0.0
12-Jul-23 10:39:00	13.9	224.9	3.5	16.8	-0.2	24.2	9.4	9.5	50	1	0	0.0
12-Jul-23 10:40:00	13.9	224.2	3.6	16.8	-0.1	24.2	9.4	9.5	50	1	0	0.0
12-Jul-23 10:41:00	13.9	223.5	3.7	16.8	-0.1	24.3	9.4	9.5	50	1	0	0.0
12-Jul-23 10:42:00	13.9	222.8	3.6	16.8	-0.2	24.2	9.4	9.5	50	1	0	0.0
12-Jul-23 10:43:00	13.9	222.1	3.6	16.8	-0.2	24.3	9.4	9.5	50	1	0	0.0
12-Jul-23 10:44:00	13.9	221.3	3.6	16.8	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:45:00	13.9	220.6	3.7	16.8	-0.6	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 10:46:00	13.8	219.8	3.6	16.8	-0.5	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:47:00	13.8	219.0	3.7	16.8	-0.4	24.2	9.4	9.5	50	1	0	0.0
12-Jul-23 10:48:00	13.8	218.3	3.7	16.8	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:49:00	13.8	217.6	3.7	16.8	-0.5	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:50:00	13.8	216.9	3.7	16.8	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:51:00	13.8	216.3	3.7	16.8	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:52:00	13.8	215.6	3.7	16.8	-0.2	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:53:00	13.8	215.0	3.8	16.8	-0.3	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:54:00	13.8	214.3	3.8	16.8	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 10:55:00	13.8	213.7	3.7	16.8	-0.4	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 10:56:00	13.8	213.0	3.7	16.8	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 10:57:00	13.7	212.3	3.7	16.8	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 10:58:00	13.7	211.7	3.8	16.8	0.0	24.3	9.4	9.5	50	1	0	0.0
12-Jul-23 10:59:00	13.7	211.1	3.8	16.9	-0.8	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:00:00	13.7	210.5	3.7	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:01:00	13.7	209.9	3.7	16.9	-0.5	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:02:00	13.7	209.3	3.7	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:03:00	13.7	208.7	3.7	16.9	-0.3	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:04:00	13.7	208.1	3.7	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:05:00	13.7	207.5	3.7	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:06:00	13.7	207.0	3.6	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:07:00	13.7	206.4	3.6	16.9	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:08:00	13.7	205.8	3.6	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:09:00	13.6	205.3	3.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:10:00	13.6	204.7	3.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:11:00	13.6	204.2	3.7	16.9	-0.8	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:12:00	13.6	203.7	3.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:13:00	13.6	203.1	3.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:14:00	13.6	202.6	3.8	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:15:00	13.6	202.1	3.8	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:16:00	13.6	201.5	3.9	16.9	-0.7	24.2	9.4	9.5	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 11:17:00	13.6	201.0	4.0	16.9	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 11:18:00	13.6	200.5	4.1	16.9	-0.7	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 11:19:00	13.6	200.0	4.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:20:00	13.6	199.4	4.1	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:21:00	13.5	198.9	4.1	16.9	-0.7	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:22:00	13.5	198.4	4.1	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:23:00	13.5	198.0	4.0	16.9	-0.7	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:24:00	13.5	197.5	4.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:25:00	13.5	197.0	4.0	16.9	-0.7	24.2	9.5	9.4	50	1	0	0.0
12-Jul-23 11:26:00	13.5	196.5	4.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:27:00	13.5	196.1	3.9	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:28:00	13.5	195.6	4.0	16.9	-0.7	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:29:00	13.5	195.2	4.1	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:30:00	13.5	194.7	4.0	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:31:00	13.5	194.2	4.0	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:32:00	13.4	193.8	4.1	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:33:00	13.4	193.3	4.1	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:34:00	13.4	192.9	4.0	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:35:00	13.4	192.4	4.1	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:36:00	13.4	192.1	4.1	16.9	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:37:00	13.4	191.6	4.1	16.9	-0.2	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:38:00	13.4	191.2	4.1	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:39:00	13.4	190.8	4.1	16.9	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:40:00	13.4	190.4	4.1	16.9	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:41:00	13.4	190.0	4.1	16.9	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:42:00	13.4	189.6	4.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:43:00	13.4	189.2	4.1	16.9	-0.8	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:44:00	13.3	188.8	4.1	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:45:00	13.3	188.4	4.2	17.0	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:46:00	13.3	188.1	4.3	17.0	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:47:00	13.3	187.7	4.3	17.0	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:48:00	13.3	187.3	4.2	17.0	-0.8	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:49:00	13.3	186.9	4.2	17.0	-0.7	24.3	9.4	9.5	50	1	0	0.0
12-Jul-23 11:50:00	13.3	186.5	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:51:00	13.3	186.2	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:52:00	13.3	185.8	4.2	17.0	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:53:00	13.3	185.5	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:54:00	13.3	185.1	4.2	17.0	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:55:00	13.3	184.8	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:56:00	13.2	184.4	4.2	17.0	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 11:57:00	13.2	184.1	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:58:00	13.2	183.8	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 11:59:00	13.2	183.4	4.2	17.0	-0.1	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:00:00	13.2	183.1	4.3	17.0	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 12:01:00	13.2	182.8	4.4	17.0	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 12:02:00	13.2	182.4	4.3	17.0	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:03:00	13.2	182.1	4.3	17.0	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:04:00	13.2	181.8	4.3	17.0	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:05:00	13.2	181.5	4.4	17.0	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 12:06:00	13.2	181.2	4.5	17.0	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:07:00	13.1	180.8	4.5	17.0	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 12:08:00	13.1	180.5	4.4	17.0	0.0	24.3	9.4	9.4	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 12:09:00	13.1	180.2	4.4	17.0	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 12:10:00	13.1	179.9	4.5	17.1	0.0	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 12:11:00	13.1	179.6	4.5	17.1	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:12:00	13.1	179.3	4.6	17.1	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:13:00	13.1	179.0	4.6	17.1	0.0	24.3	9.5	9.4	50	1	0	0.0
12-Jul-23 12:14:00	13.1	178.6	4.6	17.1	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:15:00	13.1	178.2	4.6	17.1	0.0	24.3	9.4	9.4	50	1	0	0.0
12-Jul-23 12:16:00	13.1	177.9	4.6	17.1	0.0	24.2	9.5	9.4	50	1	0	0.0
12-Jul-23 12:17:00	13.1	177.4	4.6	17.1	0.0	24.2	9.5	9.4	50	1	0	0.0
12-Jul-23 12:18:00	13.1	177.0	4.6	17.1	0.0	24.3	9.5	9.4	50	1	0	0.0
12-Jul-23 12:19:00	13.0	176.5	4.7	17.1	0.0	24.3	9.5	9.4	50	1	0	0.0
12-Jul-23 12:20:00	13.0	176.0	4.6	17.1	0.0	24.2	9.5	9.4	50	1	0	0.0
12-Jul-23 12:21:00	13.0	175.5	4.6	17.1	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:22:00	13.0	175.0	4.4	17.1	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:23:00	13.0	174.4	4.5	17.1	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:24:00	12.6	173.9	4.8	17.1	52.6	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:25:00	8.8	173.3	5.5	28.2	92.1	24.5	9.5	9.5	50	1	1	0.0
12-Jul-23 12:26:00	4.8	172.6	5.2	48.5	93.9	24.5	9.5	9.5	50	1	1	0.0
12-Jul-23 12:27:00	3.4	172.0	4.8	62.8	56.4	21.3	9.5	9.5	50	1	1	0.0
12-Jul-23 12:28:00	4.4	171.4	4.5	61.4	-0.8	20.1	9.5	9.5	50	1	0	0.0
12-Jul-23 12:29:00	6.5	171.4	4.5	48.1	-0.8	19.9	9.5	9.5	50	1	0	0.0
12-Jul-23 12:30:00	11.0	177.2	4.5	34.4	-0.3	19.8	9.5	9.5	50	1	0	0.0
12-Jul-23 12:31:00	19.1	197.1	4.4	22.2	0.0	21.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:32:00	28.7	221.9	4.4	17.0	0.0	24.1	9.5	9.5	50	1	0	0.0
12-Jul-23 12:33:00	39.7	244.0	4.4	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:34:00	51.1	263.5	4.3	16.7	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:35:00	61.7	279.1	4.4	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:36:00	68.6	291.5	4.4	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:37:00	67.6	296.6	4.4	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:38:00	66.3	296.5	4.4	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:39:00	63.6	295.8	4.3	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:40:00	59.6	293.5	4.3	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:41:00	56.2	289.9	4.2	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:42:00	53.9	286.2	4.2	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:43:00	52.2	283.6	4.2	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:44:00	51.1	281.2	4.2	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:45:00	50.2	279.1	4.3	16.8	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:46:00	49.3	277.5	4.4	16.8	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:47:00	48.5	276.0	4.4	16.9	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:48:00	47.9	274.7	4.5	16.9	0.0	24.3	9.5	9.5	50	1	0	0.0
12-Jul-23 12:49:00	47.2	273.5	4.5	16.9	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:50:00	46.6	272.4	4.6	16.9	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:51:00	46.1	271.4	4.6	16.9	-0.2	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:52:00	46.3	270.5	4.6	16.9	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:53:00	46.6	269.8	4.6	16.9	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:54:00	46.8	269.3	4.5	16.9	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:55:00	47.5	270.1	4.4	16.9	-0.5	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:56:00	49.0	271.9	4.4	16.9	-0.3	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:57:00	50.3	273.9	4.5	16.9	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:58:00	50.9	275.9	4.5	16.9	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 12:59:00	50.6	277.4	4.4	16.9	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:00:00	50.4	277.7	4.4	16.9	-0.8	24.2	9.5	9.5	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 13:01:00	50.1	277.1	4.5	16.9	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:02:00	49.8	276.2	4.4	16.9	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:03:00	49.3	274.6	4.4	17.0	-0.3	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:04:00	49.1	273.0	4.4	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:05:00	49.3	271.7	4.4	17.0	-0.3	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:06:00	49.6	270.8	4.4	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:07:00	49.8	270.3	4.3	17.0	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:08:00	50.2	271.5	4.3	17.0	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:09:00	50.7	272.5	4.4	17.0	-0.7	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:10:00	51.3	273.8	4.4	17.0	-0.6	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:11:00	51.9	275.2	4.4	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:12:00	51.8	276.3	4.4	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:13:00	51.7	276.8	4.4	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:14:00	51.5	276.3	4.5	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:15:00	51.3	275.5	4.4	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:16:00	51.1	274.4	4.3	17.0	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:17:00	51.1	273.2	4.3	17.0	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:18:00	51.3	272.3	4.3	17.0	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:19:00	51.5	271.5	4.3	17.0	0.0	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:20:00	51.6	271.1	4.3	17.0	-0.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:21:00	51.8	271.3	4.3	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:22:00	52.0	271.6	4.2	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:23:00	52.4	271.8	4.2	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:24:00	52.7	272.3	4.2	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:25:00	53.0	273.4	4.2	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:26:00	52.9	274.5	4.3	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:27:00	52.8	275.6	4.3	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:28:00	52.7	275.4	4.4	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:29:00	52.6	274.6	4.4	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:30:00	52.5	273.9	4.3	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:31:00	52.4	273.3	4.4	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:32:00	52.4	272.6	4.4	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:33:00	52.3	271.9	4.5	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:34:00	52.2	271.4	4.5	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:35:00	52.1	270.9	4.5	17.0	-0.8	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 13:36:00	51.7	270.5	4.5	17.1	53.4	24.2	9.5	9.5	50	1	0	14.0
12-Jul-23 13:37:00	44.7	269.7	4.9	28.0	95.7	24.5	9.5	9.5	50	1	0	38.0
12-Jul-23 13:38:00	34.7	265.7	4.8	49.2	96.0	24.4	9.5	9.5	50	1	0	62.0
12-Jul-23 13:39:00	26.4	257.6	4.5	63.7	96.9	21.3	9.5	9.5	50	1	0	86.0
12-Jul-23 13:40:00	20.7	250.5	4.5	71.5	83.8	20.4	9.5	9.5	50	1	0	100.0
12-Jul-23 13:41:00	16.6	246.0	4.5	76.2	82.5	20.5	9.5	9.5	50	1	0	100.0
12-Jul-23 13:42:00	13.8	243.3	4.5	80.5	83.3	20.5	9.5	9.5	50	1	0	100.0
12-Jul-23 13:43:00	11.6	242.1	4.4	84.8	81.8	20.6	9.5	9.5	50	1	0	100.0
12-Jul-23 13:44:00	10.0	240.9	4.4	88.7	82.7	20.7	9.5	9.5	50	1	0	100.0
12-Jul-23 13:45:00	8.7	239.6	4.4	93.0	93.4	20.7	9.5	9.5	50	1	0	100.0
12-Jul-23 13:46:00	7.6	238.3	4.4	98.7	96.2	20.9	9.5	9.5	50	1	0	100.0
12-Jul-23 13:47:00	6.7	237.4	4.4	100.1	96.6	20.9	9.5	9.5	50	1	0	100.0
12-Jul-23 13:48:00	6.2	236.5	4.4	100.3	95.3	20.9	9.5	9.5	50	1	0	66.7
12-Jul-23 13:49:00	7.1	235.6	4.3	100.3	22.8	21.0	9.5	9.5	50	1	0	0.0
12-Jul-23 13:50:00	11.0	234.7	4.2	97.9	-0.6	20.8	9.5	9.5	50	1	0	0.0
12-Jul-23 13:51:00	13.8	233.9	4.2	85.4	-0.8	20.6	9.5	9.5	50	1	0	0.0
12-Jul-23 13:52:00	14.0	233.1	4.3	71.2	-0.7	20.4	9.5	9.5	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 13:53:00	14.0	232.3	4.3	57.0	-0.6	20.1	9.3	9.3	50	1	0	0.0
12-Jul-23 13:54:00	14.0	231.5	4.2	43.2	-0.8	19.9	9.4	9.4	50	1	0	0.0
12-Jul-23 13:55:00	14.0	230.6	4.3	29.8	-0.7	20.0	9.4	9.4	50	1	0	0.0
12-Jul-23 13:56:00	14.0	229.8	4.3	19.3	-0.7	22.5	9.4	9.4	50	1	0	0.0
12-Jul-23 13:57:00	13.9	229.0	4.3	16.8	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 13:58:00	13.9	228.3	4.3	16.8	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 13:59:00	13.9	227.5	4.3	16.8	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:00:00	13.9	226.7	4.3	16.8	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:01:00	13.9	225.9	4.3	16.8	-0.6	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:02:00	13.9	225.1	4.2	16.8	-0.2	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:03:00	13.9	224.4	4.3	16.8	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:04:00	13.9	223.7	4.3	16.8	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:05:00	13.9	222.9	4.3	16.8	-0.3	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:06:00	13.9	222.2	4.4	16.8	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:07:00	13.9	221.5	4.4	16.8	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:08:00	13.9	220.8	4.3	16.8	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:09:00	13.8	220.1	4.3	16.8	-0.8	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:10:00	13.8	219.4	4.3	16.8	-0.8	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:11:00	13.8	218.7	4.4	16.8	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:12:00	13.8	218.1	4.3	16.8	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:13:00	13.8	217.4	4.3	16.8	-0.8	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:14:00	13.8	216.7	4.3	16.8	-0.8	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:15:00	13.8	216.0	4.4	16.9	-0.8	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:16:00	13.8	215.3	4.4	16.9	-0.8	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:17:00	13.8	214.7	4.4	16.9	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:18:00	13.8	214.0	4.4	16.9	-0.7	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:19:00	13.8	213.4	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:20:00	13.7	212.7	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:21:00	13.7	212.0	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:22:00	13.7	211.4	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:23:00	13.7	210.8	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:24:00	13.7	210.2	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:25:00	13.7	209.5	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:26:00	13.7	208.9	4.4	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:27:00	13.7	208.3	4.3	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:28:00	13.7	207.7	4.3	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:29:00	13.7	207.1	4.2	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:30:00	13.7	206.5	4.2	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:31:00	13.7	205.9	4.2	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:32:00	13.6	205.3	4.3	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:33:00	13.6	204.8	4.3	16.9	-0.7	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:34:00	13.6	204.2	4.2	16.9	-0.6	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:35:00	13.6	203.7	4.2	16.9	-0.6	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:36:00	13.6	203.1	4.2	16.9	-0.6	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:37:00	13.6	202.6	4.2	16.9	-0.6	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:38:00	13.6	202.1	4.2	16.9	-0.6	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:39:00	13.6	201.6	4.3	16.9	-0.6	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:40:00	13.6	201.1	4.2	16.9	-0.6	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:41:00	13.6	200.6	4.2	16.9	-0.6	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:42:00	13.6	200.1	4.2	16.9	-0.1	24.2	9.3	9.3	50	1	0	0.0
12-Jul-23 14:43:00	13.6	199.6	4.2	16.9	-0.6	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:44:00	13.5	199.1	4.2	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0



	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 14:45:00	13.5	198.7	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:46:00	13.5	198.2	4.3	16.9	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:47:00	13.5	197.7	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:48:00	13.5	197.2	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:49:00	13.5	196.7	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:50:00	13.5	196.2	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:51:00	13.5	195.7	4.3	16.9	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 14:52:00	13.5	195.2	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:53:00	13.5	194.8	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:54:00	13.5	194.3	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:55:00	13.4	193.9	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:56:00	13.4	193.4	4.3	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:57:00	13.4	193.0	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:58:00	13.4	192.5	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 14:59:00	13.4	192.1	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:00:00	13.4	191.7	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:01:00	13.4	191.3	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:02:00	13.4	190.9	4.4	16.9	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:03:00	13.4	190.4	4.4	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:04:00	13.4	190.0	4.5	16.9	-0.2	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:05:00	13.4	189.6	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:06:00	13.4	189.2	4.4	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:07:00	13.3	188.8	4.5	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:08:00	13.3	188.4	4.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:09:00	13.3	188.0	4.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:10:00	13.3	187.6	4.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:11:00	13.3	187.2	4.6	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:12:00	13.3	186.8	4.7	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:13:00	13.3	186.5	4.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:14:00	13.3	186.1	4.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:15:00	13.3	185.7	4.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:16:00	13.3	185.3	4.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:17:00	13.3	185.0	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:18:00	13.2	184.6	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:19:00	13.2	184.3	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:20:00	13.2	184.0	4.8	16.9	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 15:21:00	13.2	183.6	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:22:00	13.2	183.2	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:23:00	13.2	182.9	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:24:00	13.2	182.6	4.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:25:00	13.2	182.2	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:26:00	13.2	181.9	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:27:00	13.2	181.5	4.8	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:28:00	13.2	181.2	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:29:00	13.2	180.9	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:30:00	13.1	180.6	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:31:00	13.1	180.2	5.0	16.9	-0.8	24.2	9.4	9.3	50	1	0	0.0
12-Jul-23 15:32:00	13.1	179.9	5.1	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:33:00	13.1	179.6	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:34:00	13.1	179.2	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:35:00	13.1	178.9	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:36:00	13.1	178.5	5.1	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 15:37:00	13.1	178.1	5.1	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:38:00	13.1	177.6	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:39:00	13.1	177.1	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:40:00	13.1	176.6	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:41:00	13.0	176.1	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:42:00	13.0	175.6	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:43:00	13.0	175.0	5.0	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:44:00	13.0	174.4	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:45:00	13.0	173.9	4.9	16.9	-0.8	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:46:00	13.0	173.3	4.9	16.9	-0.1	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:47:00	11.4	172.7	5.5	19.3	93.1	24.2	9.5	9.5	50	1	0	0.0
12-Jul-23 15:48:00	7.1	172.0	5.7	37.4	96.4	24.6	9.5	9.5	50	1	1	0.0
12-Jul-23 15:49:00	3.7	171.3	5.4	56.8	96.7	23.1	9.4	9.5	50	1	1	0.0
12-Jul-23 15:50:00	3.8	170.6	5.0	65.7	15.9	20.4	9.4	9.5	50	1	1	0.0
12-Jul-23 15:51:00	5.2	170.2	5.0	57.0	-0.7	20.1	9.4	9.4	50	1	0	0.0
12-Jul-23 15:52:00	8.1	171.5	4.9	43.5	-0.7	19.9	9.4	9.4	50	1	0	0.0
12-Jul-23 15:53:00	14.3	184.7	5.0	30.2	-0.7	20.0	9.4	9.4	50	1	0	0.0
12-Jul-23 15:54:00	23.0	208.2	5.0	19.4	-0.7	22.3	9.4	9.4	50	1	0	0.0
12-Jul-23 15:55:00	32.9	231.7	5.0	16.9	-0.7	24.1	9.4	9.5	50	1	0	0.0
12-Jul-23 15:56:00	42.1	251.6	5.1	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:57:00	51.7	267.2	5.1	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 15:58:00	61.6	280.3	5.1	16.9	-0.7	24.2	9.4	9.5	50	1	0	0.0
12-Jul-23 15:59:00	68.2	291.6	5.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:00:00	66.0	295.7	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:01:00	64.4	295.1	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:02:00	62.5	294.1	5.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:03:00	60.2	292.5	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:04:00	58.1	290.3	5.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:05:00	56.5	288.0	5.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:06:00	55.5	285.9	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:07:00	54.5	283.7	5.1	16.9	-0.7	24.1	9.4	9.5	50	1	0	0.0
12-Jul-23 16:08:00	53.7	281.7	5.1	16.9	-0.7	24.1	9.4	9.5	50	1	0	0.0
12-Jul-23 16:09:00	52.9	280.1	5.1	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:10:00	52.4	278.7	5.1	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:11:00	52.1	277.5	5.0	16.9	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:12:00	51.3	276.5	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:13:00	50.9	275.7	4.9	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:14:00	50.4	274.8	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:15:00	50.1	274.1	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:16:00	49.7	273.4	5.0	16.9	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:17:00	49.3	272.8	5.0	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:18:00	49.1	272.1	5.1	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:19:00	49.2	271.4	5.1	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:20:00	49.4	270.8	5.1	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:21:00	49.6	270.3	5.1	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:22:00	49.8	270.2	5.1	17.0	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:23:00	50.2	270.8	5.1	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:24:00	51.1	272.0	5.1	17.0	-0.7	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:25:00	52.0	274.3	5.1	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:26:00	52.8	276.5	5.2	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:27:00	52.6	277.8	5.2	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:28:00	52.2	277.5	5.2	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 16:29:00	51.8	276.9	5.2	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:30:00	51.4	275.7	5.3	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:31:00	51.1	274.3	5.3	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:32:00	51.2	273.0	5.3	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:33:00	51.3	272.0	5.4	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:34:00	51.5	271.3	5.4	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:35:00	51.6	270.7	5.4	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:36:00	51.7	270.3	5.4	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:37:00	51.9	270.4	5.4	17.0	-0.7	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:38:00	52.2	271.7	5.3	17.0	-0.2	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:39:00	52.9	273.4	5.2	17.0	-0.1	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:40:00	53.4	275.3	5.3	17.0	-0.4	24.2	9.4	9.4	50	1	0	0.0
12-Jul-23 16:41:00	53.8	276.7	5.4	17.0	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:42:00	53.6	276.6	5.3	17.0	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:43:00	53.1	276.1	5.4	17.0	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:44:00	52.8	275.2	5.4	17.0	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:45:00	52.5	274.2	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:46:00	52.3	273.2	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:47:00	52.1	272.5	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:48:00	52.2	271.9	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:49:00	52.4	271.5	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:50:00	52.6	271.1	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:51:00	52.9	271.2	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:52:00	53.1	271.5	5.4	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:53:00	53.5	271.8	5.3	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:54:00	53.9	272.4	5.2	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:55:00	54.2	273.8	5.2	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:56:00	54.5	274.8	5.4	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:57:00	54.8	274.7	5.4	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:58:00	54.6	274.5	5.4	17.1	-0.8	24.1	9.4	9.4	50	1	0	0.0
12-Jul-23 16:59:00	53.6	274.2	5.3	17.1	50.4	24.1	9.4	9.4	50	1	0	14.0
12-Jul-23 17:00:00	46.3	273.0	5.8	28.0	97.4	24.4	9.4	9.5	50	1	0	38.0
12-Jul-23 17:01:00	35.7	267.8	5.9	49.5	98.5	24.2	9.4	9.5	50	1	0	62.0
12-Jul-23 17:02:00	26.8	259.8	5.6	63.9	87.3	21.1	9.4	9.5	50	1	0	86.0
12-Jul-23 17:03:00	20.8	252.8	5.5	70.1	84.2	20.3	9.4	9.4	50	1	0	100.0
12-Jul-23 17:04:00	16.6	248.3	5.5	74.9	85.4	20.4	9.4	9.4	50	1	0	100.0
12-Jul-23 17:05:00	13.7	246.2	5.4	79.6	83.6	20.5	9.4	9.4	50	1	0	100.0
12-Jul-23 17:06:00	11.5	244.7	5.3	84.1	85.2	20.6	9.4	9.4	50	1	0	100.0
12-Jul-23 17:07:00	9.8	243.2	5.3	88.8	84.6	20.6	9.4	9.4	50	1	0	100.0
12-Jul-23 17:08:00	8.5	241.7	5.3	93.3	90.5	20.7	9.4	9.4	50	1	0	100.0
12-Jul-23 17:09:00	7.4	240.1	5.3	98.6	98.4	20.8	9.4	9.4	50	1	0	100.0
12-Jul-23 17:10:00	6.5	238.6	5.3	100.2	97.2	20.9	9.4	9.4	50	1	0	100.0
12-Jul-23 17:11:00	6.2	237.6	5.2	100.3	98.2	20.9	9.4	9.4	50	1	0	66.7
12-Jul-23 17:12:00	7.1	236.6	5.1	100.2	23.6	20.9	9.4	9.4	50	1	0	0.0
12-Jul-23 17:13:00	10.7	235.6	5.2	98.2	-0.8	20.8	9.4	9.4	50	1	0	0.0
12-Jul-23 17:14:00	13.7	234.8	5.2	85.9	-0.8	20.6	9.4	9.4	50	1	0	0.0
12-Jul-23 17:15:00	14.0	234.0	5.2	71.9	-0.8	20.3	9.4	9.4	50	1	0	0.0
12-Jul-23 17:16:00	14.0	233.2	5.2	57.7	-0.8	20.1	9.4	9.4	50	1	0	0.0
12-Jul-23 17:17:00	13.9	232.4	5.2	44.0	-0.8	19.8	9.2	9.2	50	1	0	0.0
12-Jul-23 17:18:00	13.9	231.5	5.2	30.6	-0.8	20.0	9.3	9.3	50	1	0	0.0
12-Jul-23 17:19:00	13.9	230.6	5.2	19.7	-0.8	22.2	9.2	9.2	50	1	0	0.0
12-Jul-23 17:20:00	13.9	229.8	5.3	16.9	-0.8	24.1	9.2	9.3	50	1	0	0.0

	Pressure	Temperature, Max	Scrubber dP	Scrubber Liquid Blowdown	Scrubber Liquid Recirculation Flow	Mill Water Flow	Cabon Asdsorption Filter dP	Cabon Asdsorption Filter dP	Inlet Damper to Blower	Blower to Carbon Bed Status	Pre-Vac Ejector Supply Valve Position	Post-Vac After Condenser Vent Pressure Control Valve
	psi	F	inH2O	Scrubber Sump Level Control % Open	gpm	gpm	inH2O	inH2O	%	0 or 1	0 or 1	%
12-Jul-23 17:21:00	13.9	229.1	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:22:00	13.9	228.4	5.2	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:23:00	13.8	227.8	5.2	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:24:00	13.8	227.1	5.1	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:25:00	13.8	226.4	5.0	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:26:00	13.8	225.7	5.1	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:27:00	13.8	225.1	5.0	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:28:00	13.8	224.4	5.0	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:29:00	13.7	223.7	5.1	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:30:00	13.7	223.0	5.2	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:31:00	13.7	222.2	5.2	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:32:00	13.7	221.5	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:33:00	13.7	220.8	5.2	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:34:00	13.7	220.0	5.3	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:35:00	13.6	219.2	5.2	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:36:00	13.6	218.4	5.2	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:37:00	13.6	217.7	5.2	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:38:00	13.6	216.9	5.2	16.8	-0.8	24.1	9.2	9.3	50	1	0	0.0
12-Jul-23 17:39:00	13.6	216.2	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:40:00	13.5	215.4	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:41:00	13.5	214.7	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:42:00	13.5	214.1	5.4	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:43:00	13.5	213.4	5.4	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:44:00	13.5	212.8	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:45:00	13.5	212.2	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:46:00	13.4	211.6	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:47:00	13.4	210.9	5.3	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:48:00	13.4	210.3	5.5	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:49:00	13.4	209.8	5.5	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:50:00	13.4	209.2	5.5	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:51:00	13.4	208.6	5.5	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:52:00	13.3	208.1	5.4	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:53:00	13.3	207.5	5.4	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:54:00	13.3	206.9	5.5	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:55:00	13.3	206.4	5.4	16.8	-0.8	24.1	9.2	9.2	50	1	0	0.0
12-Jul-23 17:56:00	13.3	205.9	5.4	16.8	-0.8	24.1	9.3	9.3	50	1	0	0.0
12-Jul-23 17:57:00	13.3	205.3	5.3	16.8	-0.8	24.1	9.3	9.3	50	1	0	0.0

**APPENDIX H**

**SOURCE TEST PLAN AND APPROVAL**



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*Advanced Industrial Resources, Inc.  
Environmental Engineering  
800-224-5007  
www.airtest1.com*

May 1<sup>st</sup>, 2023

Ms. Suzanne Blackburn  
Oregon Department of Environmental Quality  
Western Region (Salem Office)  
4026 Fairview Industrial Drive Southeast  
Salem, Oregon 97302

Regarding: Source Test Plan for EU 144 – Advanced Material Recycling System (aka Juno<sup>®</sup>)  
Georgia-Pacific Toledo LLC  
Permit No. 21-00005-TV-01

Dear Ms. Blackburn:

Please accept for review the Source Test Plan (STP) that accompanies this cover letter. The STP describes the protocols for conducting the permit required 30-batch cycle VOC control efficiency determination monitoring, the 12 consecutive monthly VOC control efficiency monitoring periods, and the once per permit term required VOC and HAPs emission factor verification (EFV) performance test on the Advanced Material Recycling System (AMRS) (aka Juno<sup>®</sup>) EU-144 operated at the Georgia-Pacific Toledo LLC facility located in Toledo, Oregon.

This testing is being conducted to in accordance to the applicable permit operating conditions in the Oregon Department of Environmental Quality Title V Permit No. 21-00005-TV-01. Advanced Industrial Resources, Inc (AIR) personnel will perform all elements of the test program. The 30-Batch Cycle test is scheduled for the weeks of **June 5, 2023 and June 12, 2023**, as detailed in Section 11.3 of this protocol. The EFV test is scheduled for the week of **July 10, 2023**. The 12 consecutive monthly VOC control efficiency test schedule begins the week of June 12, 2023, and the test schedule is also presented in Section 11.3.

The facility is located at the following address:

Georgia-Pacific Toledo LLC  
1400 SE Butler Bridge Road  
Toledo, Oregon 97391

If there are any questions, please do not hesitate to contact us at (800) 224-5007.

Sincerely,  
Advanced Industrial Resources

Ross Winne  
Technical Director

Derek Stephens  
Vice President

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## APPENDICES

- Appendix A Sample Outline of the Final Test Report
- Appendix B Sample Calculations and Nomenclature

## 1.0 INTRODUCTION

Georgia-Pacific Toledo operates a pulp and paper facility located at 1400 SE Butler Bridge Road, Toledo, Oregon 97391. This document represents the protocol for completing the permit required 30-batch cycle VOC control efficiency monitoring tests, 12 consecutive monthly VOC control efficiency monitoring tests, and the once per permit term VOC and HAPs emission factor verification (EFV) performance test on the Advanced Material Recycling System (AMRS; aka Juno<sup>®</sup>) (EU-144) stack exhaust all in accordance with the facility's Oregon Department of Environmental Quality (ODEQ) issued air quality permit (Permit No. 21-0005-TV).

This Source Test Plan (STP) describes the methods and procedures to be used in conducting the subject emissions monitoring and testing. The protocol was developed using approved United States Environmental Protection Agency (EPA) test methods and in accordance with the requirements of 40 *CFR* Part 60, Appendix A, ODEQ testing guidance, and the facility's Title V permit. This STP is being submitted to DEQ to meet conditions 77.a., 77.b.ii., and 99.a. in the facility's permit.

Advanced Industrial Resources, Inc. (*AIR*) has been contracted by Georgia-Pacific Toledo LLC to perform the aforementioned test programs. *AIR* will conduct all field sampling work while the HAPs samples collected via NCASI 105.01 will be performed by Enthalpy Labs of Durham, North Carolina. The office headquarters of *AIR* are located at 3407 Novis Pointe NW, Acworth, Georgia, but all correspondence should be directed to P.O. Box 846, Marietta, Georgia 30061. If there are any questions or comments concerning this Site-Specific Test Protocol, please contact Mr. Ross Winne ([rwinne@airtest1.com](mailto:rwinne@airtest1.com)) of *AIR* at 800-224-5007. Mr. Scott Austin ([Scott.Austin2@gapac.com](mailto:Scott.Austin2@gapac.com)) will represent Georgia-Pacific Toledo LLC and can be contacted at 541-336-8318.

### Test Team Personnel

Team Leaders: Dan Kirk (primary)

Field Technician: (others TBD)

Lab Technician: Russell Barton

The following statements are required by ODEQ to be included in the Source Test Plan:

- Sampling replicate(s) will not be accepted if separated by a time duration of twenty-four (24) hours or more, unless prior authorization is granted by DEQ.
- All compliance source tests must be performed while the emission unit(s) are operating at normal maximum operating rates. As this is the initial performance test for the AMRS, Permit Condition 99.c. states the operating rate is to be at least 90% of design capacity of the unit. Rates not in agreement with those stipulated in the Title V Permit can result in rejection of the test data. Imposed process limitations could also result from operating at atypical rates during the compliance demonstration.
- The DEQ must be notified of any changes in the source test plan and/or the specified methods prior to testing. Significant changes not acknowledged by the DEQ could be the basis for invalidating a test run and potentially the entire testing program. Documentation of any deviations must include an evaluation of the impact of the deviation on the test data.
- Method-specific quality assurance/quality control (QA/QC) procedures must be performed to ensure that the data is valid for determining source compliance. Documentation of the procedures and results shall be presented in the source test report for review. Omission of this critical information will result in rejection of the data, requiring a retest.
- Only regular operating staff may adjust the combustion system or production process and emission control parameters during the source performance tests and within two (2) hours prior to the tests. Any operating adjustments made during the source performance tests, which are a result of consultation during the tests with source testing personnel, equipment vendors or consultants, may render the source performance test invalid.
- Source test reports must be submitted to DEQ within thirty (30) days of the test dates, unless another deadline has been stipulated, either by permit condition, or by DEQ written approval. (Condition 99.e of the Title V Permit stipulates 60 days)

## 2.0 SOURCE DESCRIPTION

Georgia-Pacific Toledo operates a pulp and paper facility located at 1400 SE Butler Bridge Road, Toledo, Oregon 97391. The facility produces containerboard products from “brown stock”. The facility is comprised of all normal paper industry processes except for the pulp bleaching processes.

The AMRS (EU-144) is operated in a new processing building constructed near the existing #4 boiler and extracts usable cellulose fiber from mixed solid waste streams that include food, paper, plastics, glass, and metals. OCC rejects can be added to the solid waste stream as it enters the process.

All of the raw materials, including OCC rejects, will be collected, baled, and wrapped at an off-site solid waste collection facility. The sealed, plastic wrapped bales will be delivered by truck to the Toledo mill where the raw material will be unloaded and stored outside of the processing building.

The municipal solid waste streams will be staged at predesignated third-party operated transfer stations that are licensed to handle municipal solid waste from commercial and residential sources. The transfer stations have mechanisms in place for both prevention, detection, and removal of hazardous wastes, used oils, asbestos-containing materials, and any other inappropriate solid waste streams. Thus, the AMRS process will not receive or accept hazardous wastes, asbestos-containing materials, or other inappropriate solid waste streams. The DEQ Solid Waste Division approved the Operations Plan for the facility on 10/26/18.

At the mill site, the raw material will be fed into a rotating autoclave which is a steam-pressurized vessel with an internal rotating drum that processes and breaks down the raw materials during the two-hour batch cycle. The system utilizes a proprietary process that sanitizes the feedstock and separates paper fiber from the other commodities inherent in the feedstock stream. Although elevated, the maximum temperature of 270 degrees Fahrenheit in the autoclave is not high enough to decompose wood so the wood fibers in the raw materials or OCC rejects will leave the autoclave as fiber in a slurry form. The design capacity of the AMRS is 50,000 lbs/batch of feedstock.

The fiber recovered from the AMRS will be sent to the existing OCC plant in slurry form and will be further cleaned and refined along with the regular OCC feedstock. The fiber recovered through the AMRS will replace a portion of the OCC wastepaper that is currently brought to and processed in the OCC plant.

Any metals and other residual materials that are not recovered as fiber during the AMRS process will be collected, sorted, and sent to off-site recycling facilities or to an off-site industrial landfill. Any effluent arising from the process will be treated in the company's existing wastewater treatment system.

The overall process emissions are controlled first by packed bed tower scrubber followed by a carbon bed and then vented out of a single stack. The carbon bed also controls the building exhaust. The scrubber operating parameters pressure drop ("W.G.) and scrubber liquid rate (gpm), as well as the carbon absorption filters' pressure drop, will be recorded during each test run for the AMRS.

### 3.0 TEST PROGRAM SUMMARY

*AIR* will be conducting a series of VOC removal efficiency monitoring tests as well as an emission factor verification (EFV) performance test to confirm source emissions are as expected from the initial unit's permit application and as established in the facility's permit under the plant site emission limits (PSEL). Testing shall be conducted in accordance with applicable methodologies and test protocols established in 40 CFR 60 Appendix A, ODEQ emissions testing guidance, and the applicable permit conditions established within the facility's Title V permit.

#### 30-consecutive batch cycle monitoring

As previously described, continuous VOC emissions monitoring shall be conducted over 30-consecutive batch cycles. This testing is to be started within one week of carbon media replacement and will consist of continuously monitoring the unit's common carbon bed absorption system inlet duct and stack exhaust, simultaneously, via EPA Method 25A, in accordance with Permit condition 77.a. As described in Permit condition 77.a, the inlet and outlet volumetric flow rates and moisture contents will be assumed to be the same and therefore the VOC removal efficiency of the carbon bed system will be assessed on a concentration basis only. The VOC emissions will be quantified as total hydrocarbon (THC) on a propane calibration basis. It is further noted that EPA Method 25A quantifies the emissions of THC/VOC on a 'wet' basis and that typically the 'wet' concentrations would be converted to a dry basis for reporting purposes. However, since the inlet and outlet moisture contents will be assumed to be the same, and no EPA Methods 1-4 testing is required, no moisture corrections will be applied for this 30-batch cycle monitoring period and thus the VOC removal efficiency will be assessed using 'wet' emission concentrations only (ppmvw).

#### 12-consecutive monthly batch cycle tests

Additionally, as required in Permit condition 77.b, monthly monitoring of the carbon absorption filter system's VOC removal efficiency shall be conducted. These monitoring periods shall consist of quantifying the VOC loading to the carbon absorption system as well as the VOC emissions from the unit's stack exhaust over at least a single batch cycle (the start of one batch to the start of the next batch) once per month. The unit's VOC control efficiency will be based on mass rate emissions (lb/hr) and therefore volumetric flow rate, molecular weight, moisture, and VOC emissions, measured as total hydrocarbons (THC) on a propane calibration basis, shall be

conducted at the inlet and/or outlet sampling locations in accordance EPA Methods 1, 2, 3, 3A (outlet only), 4, and 25A.

#### Emission Factor Verification testing

Finally, as required in Permit condition 93, the once per permit term emission factor verification (EFV) performance test will be conducted to assess the unit's emissions against the applicable PSEL established in the facility's Title V Permit condition 92.a where the annual emission factor for VOCs (as Carbon) is 0.246 pounds per ton of municipal solid waste (lbs/ton MSW). This testing shall consist of quantifying the emissions of VOC (measured as THC on propane calibration basis, converted to as Carbon basis) and HAPs (methanol, formaldehyde, phenol, acetaldehyde, acrolein, and propionaldehyde) at the stack exhaust during three (3) separate batch cycles or as otherwise deemed appropriate. The sampling will be conducted via EPA Methods 1, 2, 3, 3A, 4, 25A, and NCASI 105.01. It is noted that based upon measurements made prior to this EFV test mobilization a determination will be made as to whether the mini-impinger and isokinetic versions of NCASI 105.01 will be utilized. As per the methodology, if the gas stream is saturated with moisture droplets, (i.e. above theoretical moisture carrying capacity) then the isokinetic version must be used. Specific test methods are described in further detail in Section 5.0 of this Test Protocol.

All testing will be conducted while the applicable processes are operating at a target rate of 90% or greater of the designed capacity of 50,000 lbs/batch. During testing, the process will run exclusively on municipal solid waste (MSW) feedstock. GP Toledo will ensure that all essential process monitoring equipment is operating properly and recording data throughout the test period to provide process operating rates necessary to determine process weight-based emission rates, as applicable. At a minimum, the facility will monitor and record during each test run for AMRS EU-144, the scrubber operating parameters pressure drop ("H<sub>2</sub>O) and scrubber liquid rate (gpm), damper position, as well as the carbon absorption filters' pressure drop, and the operating rate. The number of batches processed since the last carbon media replacement will be recorded during the 12-consecutive monthly batch cycle tests. This information will be included in the Final Test Report submitted.

#### 4.0 SAMPLING LOCATIONS

The AMRS EU-144 carbon filter stack exhaust is circular and has an internal diameter of 39.0 inches and the sampling ports are located 120” upstream (3.1 equivalent diameters) from the stack exhaust (upstream disturbance), and 240” downstream (6.2 equivalent diameters) from the exhaust fan (downstream disturbance). The exhaust stack is equipped with a minimum of two sampling ports oriented 90 degrees to one another on a parallel plane oriented perpendicular to the exhaust gas flow direction. A maximum of sixteen (16) sampling points (eight traverse points in each of the two cross-sections) will be used for USEPA Methods 2, 3, and 4 sampling, in accordance with USEPA Method 1 requirements. Should it be determined that the mini-impinger version of NCASI 105.01 can be used, the centroid of the sampling location will be used to collect the samples. However, if it is determined that the large impinger isokinetic version is required, then sampling will be conducted from a total of 24 total traverse points (12 in each cross-section).

The AMRS EU-144 carbon filter inlet duct sampling location is circular and has an internal diameter of 39.0 inches and the sampling ports are located at least 0.5 equivalent diameters upstream from the stack exhaust (upstream disturbance), and at least 2.0 diameters downstream from the exhaust fan (downstream disturbance). These measurements will be verified by the test team. The inlet duct is equipped with a minimum of two sampling ports oriented 90 degrees to one another on a parallel plane oriented perpendicular to the exhaust gas flow direction. A maximum of twenty-four (24) sampling points (twelve traverse points in each of the two cross-sections) will be used for USEPA Methods 2, 3, and 4 sampling, in accordance with USEPA Method 1 requirements, as applicable.

Where applicable and in accordance with EPA Method 3A Section 8.1 and Method 25A Section 8.2, the centroidal region of the sampling locations shall be used for O<sub>2</sub>/CO<sub>2</sub> and VOC emission concentration measurements.



## 5.0 SAMPLING AND ANALYSIS

Source emissions sampling will be conducted at the sampling locations listed in Section 4.0, as applicable, of this Test Protocol in accordance with 40 *CFR* Part 60 Appendix A. Specifically:

- EPA Method 1 will be used for the qualification of the location of sampling ports and for the determination of the number and positions of stack traverse points, as applicable to sample traverses for Method 2.
- EPA Method 2 will be employed for the determination of the stack gas velocity and volumetric flow rate during stack sampling using the Type “S” Pitot tube.
- EPA Method 3 and 3A will be used for the determination of molecular weight and oxygen and carbon dioxide concentration determinations.
- EPA Method 4 will be used for the direct determination of moisture content with 3 batch-length test runs of about 120-150 minutes each. ODEQ Method 4 (ODEQ4) will be used as the 2<sup>nd</sup> method for determining the moisture content of the stack gas. Specifically, ODEQ4 Equations 4.4-1 and 4.4-2 will be used to calculate the theoretical maximum moisture content of the stack gas. The lower of these two values (actual vs. theoretical) will be used for calculating dry standard volumetric flow rates (dscfm) and correcting total hydrocarbon (THC) emission concentrations to a dry basis when applicable.
- EPA Method 25A will be used for the determination of volatile organic compounds (VOCs), measured as total hydrocarbons (THC) on a propane calibration basis and corrected to an as Carbon basis when applicable.
- NCASI Method 105.01 will be used to quantify the HAPS emissions including methanol, formaldehyde, phenol, acetaldehyde, acrolein, and propionaldehyde. To ensure QA/QC, a 2<sup>nd</sup> identical sample train operated as duplicate and spiked test runs will utilized, as required by the method. Unless otherwise directed, the sample run will be conducted from batch-length durations.
- EPA Method 205 may be used for the verification of calibration gas accuracy when utilizing a gas mixing (dilution) system.

The procedure detailed in Section 11.4 of EPA Method 1 shall be used to verify the absence of cyclonic flow. Data for the verification of the absence of cyclonic flow will be included in the final report.

As applicable, samples will be recovered on site in a controlled environment and stored at the appropriate temperature in polypropylene or glass storage containers, as applicable to the method. The liquid level will be marked to verify no liquid was lost during transport. All samples will be stored upright in a closed sample box until final laboratory analysis. In order to limit the chain of custody, only essential *AIR* personnel are permitted access to these samples. All samples will be analyzed within fifteen (15) days of the completion of the field testing.

Sample analysis of the gaseous parameters will be performed on site by *AIR* during the test program. Any deviations from the Source Test Plan will be thoroughly discussed with ODEQ for approval and described in the final report.

## 6.0 DATA QUALITY OBJECTIVES

The data quality objectives (DQOs) process is generally a seven-step iterative planning approach to ensure development of sampling designs for data collection activities that support decision making. The seven steps are as follows: (1) defining the problem; (2) stating decisions and alternative actions; (3) identifying inputs into the decision; (4) defining the study boundaries; (5) defining statistical parameters, specifying action levels, and developing action logic; (6) specifying acceptable error limits; and (7) selecting resource-effective sampling and analysis plan to meet the performance criteria. The first five steps are primarily focused on identifying qualitative criteria such as the type of data needed and defining how the data will be used. The sixth step defines quantitative criteria, and the seventh step is used to develop a data collection design. In regards to emissions sampling, these steps have already been identified for typical monitoring parameters.

Monitoring methods presented in 40 *CFR* Part 60 Appendix A indicate the following regarding DQOs: Adherence to the requirements of this method will enhance the quality of the data obtained from air pollutant sampling methods. At a minimum, each method provides the following types of information: summary of method; equipment and supplies; reagents and standards; sample collection, preservation, storage, and transportation; quality control; calibration and standardization; analytical procedures, data analysis and calculations; and alternative procedures. These test methods have been designed and tested according to DQOs for emissions testing and analysis. These test methods have been specified and will be followed in accordance with this Site-Specific Test Protocol, which will ensure that DQOs are met for this project.

## 7.0 INTERNAL QUALITY ASSURANCE PROGRAM

The quality assurance/quality control (QA/QC) measures associated with the sampling and analysis procedures given in the noted EPA reference methodologies, in Subparts A of 40 *CFR* Part 60 and 40 *CFR* Part 63, and in the *EPA QA/QC Handbook*, Volume III (EPA 600/R-94/038c) will be employed, as applicable. Such measures include, but are not limited to, the procedures detailed below.

### 7.1 SAMPLING TRAIN LEAK CHECKS

Determinations of the leakage rate of the sampling train are made before and after each sampling run using the procedure detailed in Section 8.4.2 of EPA Method 5. Before the sampling run, after the sampling train has been assembled and probe and filter box temperatures have had time enough to settle at their appropriate operating values, the probe nozzle will be plugged and the system will be evacuated to a pressure of 15 inches of Hg below ambient pressure. The volumetric leakage rate will be measured by the dry gas meter over the course of one (1) minute. If the leakage rate is less than 0.020 cfm, then the test proceeds. After the sampling run, before the train is disassembled the probe nozzle will be plugged and the system will be depressurized to a vacuum equal to or greater than the maximum value reached during the sampling run. The volumetric leakage rate will be measured by the dry gas meter over the course of one (1) minute. If the leakage rate is less than 0.020 cfm, then the test run will be considered valid. If a component change must be made during the test run, a leak check will be conducted immediately before and after the component change is made using the procedure outlined above.

The Type “S” Pitot tube assembly will also be checked for leaks before and after sampling runs using the procedure in Section 8.1 of EPA Method 2. The impact opening of the Pitot tube will be blown through until a pressure of at least 3 inches of water registers on the manometer. The impact opening will quickly be plugged and held for at least 15 seconds, during which time the manometer reading must hold. The same operation will be performed on the static pressure side of the Pitot tube, except suction will be used to obtain the pressure differential.

### 7.2 PROBE NOZZLE DIAMETER CHECKS

Probe nozzles will be calibrated before each field use by measuring the internal diameter of the nozzle entrance orifice along three different diameters. Each diameter is measured to the nearest 0.001 inch, and all measurements will be averaged. If the total variation of the three

measurements exceeds 0.004 inch, the nozzle shall be reshaped, sharpened, and recalibrated before further use.

### 7.3 PITOT TUBE FACE PLANE ALIGNMENT CHECK

Before field use, each Type S Pitot tube is examined in order to verify that the face planes of the tube are properly aligned, per Method 2 of 40 *CFR* Part 60, Appendix A. The external tubing diameter and base-to-face plane distances are measured in order to verify the use of 0.84 as the baseline (isolated) pitot coefficient. At this time the entire probe assembly (i.e., the sampling probe, nozzle, thermocouple, and Pitot tube) is inspected in order to verify that its components meet the interference-free alignment specifications given in EPA Method 2. If the specifications are met, then the baseline pitot coefficient is used for the entire probe assembly.

After each field use, the face plane alignment of each Pitot tube is checked. If any damage has occurred to the tube orifices, the tube will be reshaped, realigned, and recalibrated before further use.

### 7.4 METERING SYSTEM CALIBRATION

Annually each dry gas meter (DGM) console is calibrated at five orifice settings according to Method 5 of 40 *CFR* Part 60, Appendix A. From the calibration data, calculations of the values of  $Y_m$  and  $DH_{@}$  are made, and an average of each set of values is obtained. The limit of total variation of  $Y_m$  values is  $\pm 0.02$ , and the limit for  $DH_{@}$  values is  $\pm 0.20$ .

After each field use, the calibration of the DGM console is checked by performing three calibration runs at a single intermediate orifice setting that is representative of the range used during field testing. The limit of acceptable relative variation from  $Y_m$  is 5.0%.

### 7.5 TEMPERATURE GAUGE CALIBRATION

After each field use, the temperature measuring instruments on each sampling train are calibrated against standardized mercury-in-glass reference thermometers. The limit of acceptable variation between the absolute reference temperature and the absolute indicated temperature is 1.5%.

### 7.6 BAROMETRIC PRESSURE DATA ACQUISITION

The barometric pressure at the test site is measured by contacting the National Weather Service prior to and immediately following the testing. Reported barometric pressure will be adjusted for actual elevation at the test site.

## 7.7 SAMPLE HANDLING AND CHAIN OF CUSTODY PROCEDURES

All samples are transported in a closed sample box, the security of which is the responsibility of the Field Test Director. These samples are received, checked, and numbered by the Test Director and custody records are written. The QA Director then again checks the integrity of the samples and their identifications.

For samples that require off-site analysis, the samples collected during the emissions testing program will be placed in shipping coolers with sufficient insulation to prevent breakage during shipping. All samples in a shipping container will be listed on the chain-of-custody form enclosed in the shipping container. Once the samples are securely packaged, the container will be sealed with tape and several custody seals will be placed over the top edge so that the container cannot be opened without breaking the custody seal.

## 7.8 DATA REDUCTION CHECKS

The Report Preparation Director will run an independent check (using a validated computer program) of the calculations with predetermined data before the field test. The Test Director will conduct spot checks on-site to assure that data are being recorded accurately. After the test, the Report Preparation Director will check the data input to assure that the raw data have been transferred to the computer accurately. Isokinetic sampling rates will be checked to ensure rates were  $100\% \pm 10\%$ . Volumetric flow rates, temperatures and moisture contents will be compared to test results from previous sampling events, if available, to identify potential inconsistencies in test data.

## 7.9 GAS ANALYZER CALIBRATION

**7.9.1 Calibration Gas Concentration Verification** Calibration gases that are analyzed following the Environmental Protection Agency Traceability Protocol No. 1 will be used. Certification from the gas manufacturer that Protocol No. 1 was followed will be obtained.

**7.9.2 Measurement System Preparation** *AIR* will assemble each measurement system by following the manufacturer's written instructions for preparing and preconditioning each gas analyzer and, as applicable, the other system components. *AIR* will make all necessary adjustments to calibrate the analyzers and the data recorders.

**7.9.3 Analyzer Calibration Error Test** *AIR* will conduct the analyzer calibration error check by introducing calibration gases to the measurement system upstream of each gas analyzer. After the measurement system has been prepared for use and immediately prior to starting the test run, *AIR* will introduce the zero and high-level (80-90% of applicable span value) calibration gases to calibrate the analyzer to establish calibration curve. Then, sequentially, the low- and mid-range gases will be introduced into the analyzer and their responses recorded to determine the differences between the measurement system responses and the predicted responses. These differences must be less than 5% of the respective calibration gas values. If not, the measurement system is not acceptable and must be repaired or replaced prior to testing. During this check, *AIR* will make no adjustments to the system except those necessary to achieve the correct calibration gas flow rate at the analyzer.

**7.9.4 Drift Determinations** At the end of each test run or whenever adjustments are necessary for the measurement system, *AIR* will reintroduce the zero and mid-level calibration gases, one at a time, to the measurement system at the calibration valve assembly. No adjustments are to be made to the measurement system until both the zero and calibration drift checks are made. If the respective drift values exceed  $\pm 3\%$  of the span, the test run is invalidated and the system must be repaired or replaced and the calibration error test described in the above section must be repeated before successive tests can be conducted.

**7.9.5 Analyzer Calibration Error and Drift Check Specifications** Analyzer calibration error shall be less than  $\pm 5$  percent of the calibration gas value. Zero and calibration drifts shall be less than  $\pm 3$  percent of the span value.

## 7.10 INSTRUMENT RESPONSE TIME

After the analyzer has been initially calibrated and the Calibration Error Test has been completed, *AIR* will introduce the zero calibration gas into the measurement system at the calibration valve assembly. When the system response has stabilized, the high-level calibration gas will be quickly introduced at the calibration valve assembly. The time will be recorded for

the system response output to stabilize at a value that is 95 percent of the certified calibration gas value. *AIR* will then switch back to the zero calibration gas and allow the system response to return to zero. The above procedure will be repeated three (3) times and the response times will be averaged and will be considered the system response time.



## **8.0 EXTERNAL QUALITY ASSURANCE PROGRAM**

### **8.1 AUDIT SAMPLE PROCEDURES**

There are currently no audit samples available for this testing program.

### **8.2 SITE-SPECIFIC TEST PLAN EVALUATION**

In submitting this Source Test Plan in advance of testing, Oregon DEQ personnel have been afforded the opportunity to review and comment upon the test and quality assurance procedures to be used in conducting this Source Test Plan.

### **8.3 ON-SITE TEST EVALUATION**

In submitting the schedule in Section 11.3 of this Source Test Plan, ODEQ personnel have been afforded the opportunity for on-site evaluation of all test procedures. *AIR* will provide all regulatory personnel complete access to all activities during the execution of this Source Test Plan to ensure transparency of the process.

## **9.0 REPORTING AND DATA REDUCTION REQUIREMENTS**

Upon completion of field testing activities, *AIR* will reduce the collected data and prepare a Final Test Report.

Appendix A of this Site-Specific Test Protocol includes an example outline of the Final Test Report and a brief explanation of points. The report will summarize in tabular form the results of all tests and will include all data sheets and calculations necessary to confirm whether the various emission limits were achieved. Appendix B includes example calculations and the related nomenclature for the data reduction. The Final Test Report will be submitted to ODEQ within 60 days completing the field testing portion of the program in accordance with Oregon Title-V Operating Permit #21-0005-TV-01, Condition 77.a. and 99.e.

## 10.0 PLANT ENTRY AND SAFETY

### 10.1 SAFETY RESPONSIBILITIES

The Test Director is responsible for ensuring compliance with plant entry, health, and safety requirements. The Facility Contact has the authority to impose or waive facility restrictions.

### 10.2 SAFETY PROGRAM

*AIR* has a comprehensive health and safety program that satisfies Federal OSHA requirements. The basic elements include: (1) written policies and procedures, (2) routine training of employees and supervisors, (3) medical monitoring, (4) use of personal protection equipment, (5) hazard communication, (6) pre-mobilization meetings with GP Toledo personnel, and (7) routine surveillance of the on-going test work.

### 10.3 SAFETY REQUIREMENTS

During the pretest inspection, *AIR* will ensure all sampling locations on the inlet ducts and exhaust stacks are easily accessible by scaffolding, hydraulic lift or permanent platform. There is little risk of exposure to harmful amounts of toxic materials at the sampling locations. However, test personnel will be instructed to minimize their exposure to exhaust gases.

All test personnel will adhere to the following standard safety and precautionary measures as follows:

- Confine selves to test area only.
- Wear hard hats at all times on-site, except inside the equipment resource vehicle
- Wear steel-toed shoes or boots, protective shatter-resistant glasses or goggles, and hearing protection as appropriate at the test site
- Know the locations of readily available first aid equipment and fire extinguishers
- Be familiar with Emergency Response Procedures at the facility, including evacuation signals and procedures.

## 11.0 PERSONNEL RESPONSIBILITIES AND TEST SCHEDULE

### 11.1 TEST SITE ORGANIZATION

The key tasks and task leaders are:

Facility Contact:	Jen Wagner
Program Director:	Scott Wilson
Test Director:	Dan Kirk
Technical Director:	Ross Winne
VP/QA Director:	Derek Stephens
Report Preparation Director:	Steven Haigh
Operations/Safety Director:	John Hendry

### 11.2 TEST PREPARATIONS

11.2.1 Construction of Special Sampling and Analytical Equipment. There are no equipment modifications or special analytical equipment required for this site.

11.2.2 Modifications to Facility. No modifications are necessary to the facility in order to accommodate this testing.

11.2.3 Services Provided by Facility. *AIR* will be providing all services to GP Toledo.

11.2.4 Access to Sampling Sites. During a pretest inspection, *AIR* will ensure the sampling location is easily accessible by scaffolding, hydraulic lift or permanent platform. GP Toledo will be notified of any inadequacies and these will be addressed prior to conducting the tests.

### 11.3 TEST PERSONNEL RESPONSIBILITIES AND SCHEDULE

*AIR* personnel will arrive at the plant about 1.5 hours before the start of the first test run on each of the days scheduled for sampling. Pre-test activities on these days will include the following:

The Test Director, QA Director and other *AIR* personnel will:

- Meet with the Facility Contact to review the daily test objectives

- Prepare and set-up (including leak checks) the sampling trains and analyzers
- Calibrate instrumental analyzers
- Verify communication links between team members/leaders/plant personnel

The Facility Contact will:

- Verify that the proper and adequate feed materials specified in this Plan for the various emission sources are available and that the facility will be capable of operating under the specified feed rate conditions for the entire test duration.
- Verify that all process monitors and recording devices are operating properly

*AIR* personnel will travel to the site, establish test team/facility operator communications and set up equipment at the sampling location test locations at least several hours prior to the beginning of the test program. The compliance test program is scheduled to take place as follows:

Week of 6/5/23

- Method 25A for VOC concentration @ inlet/outlet of Carbon Beds – 30 batch cycles

Week of 6/12/23

- Method 25A for VOC concentration @ inlet/outlet of Carbon Beds - 30 batch cycles (continuation)
- Method 25A for VOC concentration @ inlet/outlet of Carbon Beds & Methods 1-4 inlet or outlet for air flow (1<sup>st</sup> of series of 12 monthly tests)

Week of 7/10/23

- Second monthly test - Method 25A for VOC concentration @ inlet/outlet of Carbon Beds & Methods 1-4 inlet or outlet for air flow
- Emission Verification Test – Stack exhaust – Methods 1-4, 25A, 105.01 – 3 batch cycles

Monthly tests 3-12 for Method 25A for VOC concentration @ inlet/outlet of Carbon Beds & Methods 1-4 inlet or outlet for air flow to be conducted during 1<sup>st</sup> week of month, except for January 2024. Monthly tests may need to be reschedule depending on Toledo Mill and/or AMRS Plant operational availability.

**APPENDIX A**

**EXAMPLE OUTLINE OF THE  
FINAL TEST REPORT**

## **EXAMPLE OUTLINE OF THE FINAL TEST REPORT**

### **1.0 Introduction**

- Summary of Test Program
- Key Personnel

### **2.0 Plant, Process, and Sampling Location Descriptions**

- Process and Operation Descriptions
- Sampling Locations

### **3.0 Summary and Discussion of Test Results**

- Objectives
- Field Test Changes and Problems
- Presentation of Test Results
- Process Monitoring

### **4.0 Sampling and Analytical Procedures**

### **5.0 Quality Assurance Activities**

- Internal Quality Assurance (equipment, methodology, etc.)
- External Quality Assurance (SSTP and on-site evaluation)

### **6.0 Data Quality Objectives**

## **Appendices**

Appendix A	Test Results
Appendix B	Field Data Reduction
Appendix C	Example Calculations and Nomenclature
Appendix D	Raw Field Data
Appendix E	Laboratory Analytical Reports
Appendix F	Facility Process Monitoring Data

**APPENDIX B**

**EXAMPLE CALCULATIONS  
AND NOMENCLATURE**



## EXAMPLE CALCULATIONS

$$A_n = D_n^2 \pi / 4$$

$$A_s = D_s^2 \pi / 4$$

$$B_{ws} = V_{w(std)} / (V_{m(std)} + V_{w(std)})$$

$$c_{PM} = (m_{PM} / V_{m(std)}) (35.31466 \text{ ft}^3/\text{m}^3)$$

$$c'_{PM} = (m_{PM} / V_{m(std)}) (0.015432 \text{ gr/mg})$$

$$E_{PM} = (m_{PM} / V_{m(std)}) Q_{sd} (60 \text{ min/hr}) (2.2046 \times 10^{-6} \text{ lb./mg})$$

$$E'_{PM} = E_{PM} / P$$

$$I = 100 T_s (K_3 M_{lc} + Y_m V_m P_m / T_m) / (60 \theta v_s P_s A_n)$$

$$\text{where } K_3 = 0.002668 (\text{in. Hg ft}^3) / (\text{mL } ^\circ\text{R})$$

$$K_I = [(2.0084 \times 10^7 \Delta H_{@}) A_n (1 - B_{ws})]^2 (M_d / M_s) (T_m / T_s) (P_s / P_m)$$

$$M_d = 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2) + 0.28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_s = M_d (1 - B_{ws}) + M_w B_{ws}$$

$$P_m = P_{bar} + \Delta H / 13.6$$

$$P_s = P_{bar} + p_g / 13.6$$

$$Q_a = (60 \text{ s/min}) v_s A_s$$

$$Q_{sd} = (60 \text{ s/min}) (1 - B_{ws}) v_s A_s (T_{std} / T_s) (P_s / P_{std})$$

$$T_m = t_m + 460^\circ$$

$$T_s = t_s + 460^\circ$$

$$V_{m(std)} = 17.636 V_m Y_m P_m / T_m$$

$$V_{w(std)} = M_{lc} 0.04716$$

$$v_s = K_p C_p [\Delta p]^{1/2} [T_s / (P_s M_s)]^{1/2}$$

## NOMENCLATURE

Symbol	Units	Description
$A_n$	ft <sup>2</sup>	Area of the nozzle
$A_s$	ft <sup>2</sup>	Area of the stack
$B_{ws}$	dimensionless	Volume proportion of water in the stack gas stream
$C_p$	dimensionless	Type S pitot tube coefficient
$c_{PM}$	mg/dscm	Concentration of PM in dry stack gas, standardized
' $c_{PM}$	gr./dscf	Concentration of PM in dry stack gas, standardized
$D_n$	inches	Internal diameter of the nozzle at the entrance orifice
$D_s$	inches	Internal diameter of the stack at sampling location
$DH$	inches H <sub>2</sub> O	Average pressure differential across the meter orifice
$DH@$	inches H <sub>2</sub> O	Orifice pressure differential that corresponds to 0.75 cfm of air at 68 °F and 29.92 inches of Hg
$D_p$	inches H <sub>2</sub> O	Velocity head of stack gas
$E_{PM}$	lb./hour	Emission rate of PM, time basis
' $E_{PM}$	kg/Mg	Emission rate of PM, production basis
$I$	percent	Isokinetic sampling ratio expressed as percentage
$K_i$	dimensionless	K-factor, ratio of DH to DP, ideal
$K_p$	ft[(lb/lb-mol)(in. Hg)] <sup>1/2</sup>	Type S pitot tube constant,
	s[(°R)(in. H <sub>2</sub> O)] <sup>1/2</sup>	= 85.49
$L_p$	cfm	Measured post-test leakage rate of the sampling train
$M_d$	lb./lb.-mole	Molecular weight of gas at the DGM

Symbol	Units	Description
$M_s$	lb./lb.-mole	Molecular weight of gas at the stack
$M_w$	lb./lb.-mole	Molecular weight of water,
		= 18.0
$m_{PM}$	mg	Mass of PM in the sample
$n$	dimensionless	Number of data points
$P_{bar}$	inches Hg	Barometric pressure at measurement site
$P_{input}$	tons/hour	Process dry mass input rate
$p_g$	inches H <sub>2</sub> O	Gauge (static) pressure of stack gas
$P_m$	inches Hg	Absolute pressure of meter gases
$P_s$	inches Hg	Absolute pressure of stack gases
$P_{std}$	inches Hg	Standard absolute pressure
		= 29.92
$Q_a$	cfm	Volumetric flow rate of actual stack gas
$Q_{sd}$	dscfm	Volumetric flow rate of dry stack gas, standardized
$R$	(in. Hg)(ft <sup>3</sup> )	Ideal gas constant,
	(lb-mole)(°R)	= 21.85
$r_w$	lb/mL	Density of water,
		= 0.002201
$r_a$	g/mL	Density of acetone,
		= 0.7899
$S_d$	dimensionless	Standard deviation
$T_m$	°R	Absolute temperature of dry gas meter
$T_s$	°R	Absolute temperature of stack gas
$T_{std}$	°R	Standard absolute temperature,
		= 528
$t_m$	°F	Temperature of DGM
$t_s$	°F	Temperature of stack gas
$q$	minutes	Total sampling time

<b>Symbol</b>	<b>Units</b>	<b>Description</b>
<b>M<sub>lc</sub></b>	g	Total mass of liquid collected
<b>V<sub>m</sub></b>	dcf	Volume of gas sample as measured by the DGM
<b>V<sub>m(std)</sub></b>	dscf	Volume of gas sample as measured by the DGM, standardized
<b>V<sub>w(std)</sub></b>	scf	Volume of water vapor in the gas sample, standardized
<b>v<sub>s</sub></b>	ft./sec	Velocity of stack gas
<b>Y<sub>m</sub></b>	dimensionless	DGM calibration coefficient
<b>Y<sub>c</sub></b>	dimensionless	DGM calibration check value
<b>Y<sub>w</sub></b>	dimensionless	Reference (wet) gas meter calibration coefficient
<b>% CO<sub>2</sub></b>	percent	Percent CO <sub>2</sub> by volume, dry basis
<b>% O<sub>2</sub></b>	percent	Percent O <sub>2</sub> by volume, dry basis
<b>% N<sub>2</sub></b>	percent	Percent N <sub>2</sub> by volume, dry basis



# Oregon

Tina Kotek, Governor

## Department of Environmental Quality

Western Region Salem Office

4026 Fairview Industrial Dr SE

Salem, OR 97302

(503) 378-8240

FAX (503) 373-7944

TTY 711

June 1, 2023

Jen Wagner  
Georgia-Pacific Toledo LLC  
1400 SE Butler Bridge Rd.  
Toledo, OR 97391

Ross Winne  
Advanced Industrial Resources  
PO Box 846  
Marietta, GA 30061

Georgia-Pacific Toledo LLC  
Title V Permit 21-0005-TV-01  
2023 – Advanced Material Recycling System  
Source Test Plan – Emission Factor Verification  
**REVISED**

Ms. Wagner and Mr. Winne:

The source test plan received on May 4, 2023, [and the email received on May 31, 2023](#), for source testing at the Georgia-Pacific facility located in Toledo has been reviewed. The source test plan is for source testing the emissions from the new Advanced Material Recycling System (AMRS).

DEQ understands that the following testing is proposed.

- VOC (THC as propane) emissions at the AMRS scrubber / carbon adsorption system outlet.
- Methanol, formaldehyde, phenol, acetaldehyde, acrolein and propionaldehyde emissions from the AMRS scrubber / carbon adsorption system outlet.
- The Total VOC emissions shall be determined using the Oregon DEQ IMD for Wood Products. <https://www.oregon.gov/deq/Filtered%20Library/IMDevalVOC.pdf>

The results of these tests will be used to verify emission factors. The test plan is approved with the following conditions:

### GENERAL PROCESS CONDITIONS

1. Only regular operating staff may adjust the production process and emission control parameters during the source performance tests and within two (2) hours prior to the tests. Any operating adjustments made during the source performance tests, which are a result of consultation during the tests with source testing personnel, equipment vendors or consultants, may render the source performance test invalid.
2. The DEQ must be notified of any changes in the source test plan and/or the specified methods prior to testing. Significant changes not acknowledged by the DEQ could be the basis for invalidating a test run and potentially the entire testing program. Documentation of any deviations must include an evaluation of the impact of the deviation on the test data.

3. Method-specific quality assurance/quality control (QA/QC) procedures must be performed to ensure that the data is valid for determining source compliance. This must be done whether or not DEQ representatives are on-site to observe the testing and whether or not a QA/QC requirement has been specifically acknowledged and approved by DEQ. Only method-specific requirements explicitly exempted by the EPA and/or DEQ need not be performed. Documentation of the procedures and results shall be presented in the source test report for review. Omission of this critical information will result in rejection of the data, requiring a retest.
4. It is acceptable to postpone a scheduled test or suspend a test in progress if the discontinuation is due to equipment failure beyond the facility's control, construction delays beyond the facility's control, severe meteorological conditions, and situations that would jeopardize the safety of the testing contractors and/or operators. If the test is underway, the permittee should make every effort to complete the test run. All recoverable test information (process & sample data) must be available for DEQ review.  
  
It is unacceptable to postpone or suspend a test run in progress if it is discontinued because the source is not able to comply with an emission limit, verify an existing emission factor, or comply with a control equipment performance standard. The permittee must provide DEQ written documentation explaining the reasons for the postponement or stoppage, and any data collected prior to the stoppage. DEQ will review the documentation and all available stack test data to determine if a violation occurred.
5. Unless otherwise specified in the Permit, source testing shall be performed as follows:  
**When verifying or determining an emission factor, the stack test must generate an emission factor that represents normal emissions for the operating condition tested.**
6. A test run will start when material is beginning to be added to the autoclave and ends when the next batch of material is starting to be added to the autoclave. This testing consists of at least three batch cycles. **You may need to skip a batch, in order to give AIR the time to calibrate their instruments between source test runs.**
7. **Source testing shall be performed while the AMRS is processing feedstock that is representative of normal operations.**
8. Include a copy of the running annotated 1-minute test van DAS log that starts with initial calibrations and ends at the conclusion of the test day. It should include all calibrations, stratification checks, and test runs. Include all DAS and lab book entries and lab data in the hardcopy bound and PDF test report.
9. During source testing, the following process parameters shall be determined, recorded, and documented in the source test report. The process parameters below are to be reported for each individual test run and averaged for all test runs as appropriate.
  - Scrubber pressure drop (inches of water column)
  - Scrubber liquid blowdown rate (gpm) - **Estimated**
  - Scrubber liquid recirculation flow rate (gpm)
  - Mill water flow rate (gpm)
  - Carbon Adsorption filter pressure drop (inches of water column) – Hourly Readings
  - **Exhaust air blower inlet damper measurement**, Hourly Readings
  - **Pre-Vac Ejector Supply Valve Position** (0 or 1)
  - **Post-Vac After Condenser Vent Pressure Control Valve** (percent)
  - AMRS pressure (psi) – maximum
  - AMRS temperature (F) - maximum

- Material processed – Normal Representative Conditions – OCC / MSW ratio if possible.
- Weight of material processed during each Batch Cycle.
- Number of Batches processed since the last carbon media replacement.
- Production rate (tons per batch, tons per test run)
- Start and End Time for each batch processed during the source test.

#### **EPA/ODEQ METHODS 1-4 CONDITIONS**

- 10. Using EPA Method 2, Section 8.6 is acceptable - For processes emitting essentially air, an analysis need not be conducted; use a dry molecular weight of 29.0.**
11. If you use Method 3A, the sampling system must be leak-checked before and after the testing program (before the first run and after the last run). Results of the leak check are to be documented within the test report.
12. For compliance source testing, the flow rate for the outlet stack must meet the EPA Methods 1 & 2 criteria. Clear diagrams and documentation of this must be included in the source test report.
13. The outlet stack must be checked for cyclonic flow. Documentation of this must be provided in the test report.
- 14. The outlet flow rate must be measured for the duration of each batch cycle using EPA Methods 1-4.**
15. The moisture content of the outlet stack gas must be determined by Oregon DEQ Method 4 or by EPA Method 4 for each test run. In addition, Section 12.1.7 of EPA Method 4 states “In saturated or moisture droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one using a value based upon the saturated conditions (alternate method) and one based upon the results of the impinger analysis (EPA Method 4). If this is the case, then ODEQ Method 4 (wet bulb/dry bulb) shall be used as the alternative method. At minimum, two measurements of moisture content (Bws) using ODEQ Method 4 shall be made for each run and averaged for the run. The lower of the two values of Bws as determined by EPA Method 4 and ODEQ Method 4 shall be considered correct for each run.
16. For Oregon DEQ Method 4 in saturated stacks, the wet bulb temperature equals the dry bulb temperature. Use the dry bulb temperature for both readings.

#### **EPA METHOD 25A CONDITIONS**

17. Each Method 25A sampling system must be leak-checked before and after the testing program (before the first run and after the last run). The results of each leak check must be reported in the test report.
18. The span of the analyzer used to perform EPA Method 25A should be equivalent to 1.5 to 2.5 times the expected concentration. **AIR should attempt to choose an outlet span that will keep all test run measurements on scale, without choosing an overly high span.**

**During the previous source test, the outlet concentrations were greater than 29 ppmvw as propane at some times.**

**The analyzer span should be chosen so that all FID readings are less than the span for their respective channels.**

19. The calibration gases must be Propane in Air or in Nitrogen.
20. Include a copy of the running annotated 1-minute DAS log that starts with initial calibrations and ends at the end of the test day. It should include all calibrations, stratification checks, and test runs.
21. The DAS logs and calibration data need to be labeled THC as propane, to clarify the calibration gas used.
22. Results may not be drift corrected.
23. If the calibration drift is more than 3% of the span value, the run must be repeated.
24. Moisture content of the outlet stack gas must be determined by EPA Method 4 for each test run, to correct the wet ppmv values from Method 25A.
25. VOC (THC) as propane emissions must be reported as indicated below for each individual test run and averaged for all three test runs.

Results should be on a propane or carbon basis and be shown with and without the inclusion of methanol, formaldehyde, phenol, propionaldehyde, acetaldehyde and acrolein following DEQ Guidance Document P-820-100. Hand calculations must be provided for at least one test run.

- ppmvw as propane
- ppmvd as propane
- ppmvd as carbon
- lb/hr propane basis
- lb/hr carbon basis
- lb/ton MSW

#### **NCASI METHOD A.105.01 CONDITIONS**

26. During sampling, equipment associated with isokinetic sampling will not share a test port with other sampling equipment.
27. Ensure sufficient o-benzylhydroxylamine (BHA) is available to derivatize the aldehydes collected during the test.
- 28. Since entrained water droplets are expected, be prepared for isokinetic sampling.**
29. Ensure all quality assurance procedures summarized in the method's appendix, on page A1, are followed.
30. The sampling rate must be constant during testing.
31. Collected samples must be maintained at approximately 4°C until analysis of the samples is completed.
32. Include a full lab data package in the test report.



33. Emission of methanol, formaldehyde, phenol, propionaldehyde, acetaldehyde and acrolein must be reported individually and totaled as follows for each test run and averaged for all three test runs. Complete hand calculations must be provided for at least one test run.
- ppmvd
  - lb/hr

#### **EPA METHOD 205 CONDITIONS**

34. If a gas dilution system is to be used to provide calibration gases for other source test methods, then the system shall be evaluated once during the source test in accordance with the requirements of EPA Method 205.
35. **The Method 205 evaluation must be performed using the Method 25A FID instrument using propane calibration gas.**

#### **GENERAL TESTING CONDITIONS**

36. The Certification Form (only) of the Source Test Audit Reports (STAR) shall be completed and submitted with the Source Test Report. The Certification Form can either be bound in the report or it can be submitted separately. Submittal of the method-specific STAR reports is no longer required. Copies of all of the STAR forms are available electronically.
37. Test reports are due within 60 days of completion of each testing campaign.
38. Submit a searchable electronic PDF copy of the report, in addition to the hard copy. Email limits are 20 MB per attachment. If the report is larger than that, please send a copy on a thumb drive. We no longer have a CD Drive.
39. In an attempt to conserve natural resources and to minimize storage space requirements, the test report should be printed on both sides of each page within the document. The DEQ recognizes this may not be feasible for some supporting documentation.

DEQ understands that testing is to be conducted the week of July 10, 2023. Please let me know if there are any changes to the testing schedule.

If you have any questions or concerns, please contact me at 503-508-1989.

Sincerely,



Suzanne Blackburn  
Source Test Coordinator  
Environmental Engineer  
DEQ Salem Office

cc: Mike Eisele, DEQ: AQ File

**APPENDIX I**

**S.T.A.R. FORMS**

## SOURCE TESTING AUDIT REPORT: CERTIFICATION FORM

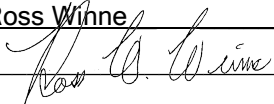
Facility: Georgia-Pacific Toledo LLC Permit #: 21-0005-TV-01 Test Date: July 12, 2023  
Emission Unit: ADVANCED MATERIAL RECYCLING SYSTEM (AMRS) (EU-144) Sampling Location: Toledo, Oregon

### SECTION 1: TESTING PROGRAM CERTIFICATION INFORMATION

ITEM OF INQUIRY	Yes	No	EXPLANATION
A. Is the purpose(s) for the testing clearly defined within the test report?	X		
B. Did testing include all pollutants specified within the Source Test Plan (STP)?	X		
C. Were all issues within the Department's response to the STP fully addressed?	X		
D. Was the source operating within $\pm 10\%$ of normal maximum capacity?	X		
E. Are all appropriate operating conditions documented?	X		
F. Were there any test interruptions?		X	
G. Were there any variances or modifications to the STP? (if Yes; reply to i & ii)		X	
i. Were the variances or modifications approved by the Department?			
ii. Does the report include an evaluation of the impact the variances or modifications had on the test data?			

### SECTION 2: SOURCE SAMPLING REPORT AUDITOR CERTIFICATION:

I hereby certify that to the best of my knowledge, the information provided within this source sampling audit report is complete and factual.

Name: Ross Winne Title: Technical Director  
Signature:  Date: September 8, 2023

### SECTION 3: PERMITTEE REPRESENTATIVE CERTIFICATION:

I hereby certify that to the best of my knowledge, the information provided within this source sampling audit report is complete and factual.

Name: \_\_\_\_\_ Title: \_\_\_\_\_  
Signature: \_\_\_\_\_ Date: \_\_\_\_\_

### SECTION 4: DEPARTMENT REPRESENTATIVE:

The Oregon Department of Environmental Quality has evaluated the Source Sampling Audit Report and has determined that the information provided is sufficient for accepting the results originating from the testing program. Although no deficiencies were exposed by the Source Sampling Audit Report, additional errors and/or inconsistencies may be detected through additional Departmental review at a later date, which may lead to a retest or an enforcement action against the permittee.

Name: \_\_\_\_\_ Title: \_\_\_\_\_  
Signature: \_\_\_\_\_ Date: \_\_\_\_\_